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Key Points:

- Maximum horizontal stress orientation varies along strike in the Hikurangi Subduction Margin upper plate
- Stress orientations reflect contemporary elastic strain accumulation processes related to subduction megathrust locking
- Stress orientations in the southern HSM are oblique to focal-mechanism stress suggesting the subduction interface is mechanically weak

Abstract

Knowledge of the contemporary in-situ stress orientations in the Earth's crust can improve our understanding of active crustal deformation, geodynamic processes, and seismicity in tectonically active regions such as the Hikurangi Subduction Margin (HSM), New Zealand. The HSM subduction interface is characterized by varying slip behavior along strike, which may be a manifestation of variation in the stress state and the mechanical strength of faults and their hanging walls, or, alternatively, these variations in seismic behavior may generate variation in the stress state in space and time. In this study, we analyze borehole image and oriented four-arm caliper logs acquired from thirteen boreholes along the HSM to present the first comprehensive stress orientation dataset within the HSM upper plate. Our results reveal a NE-SW  $S_{Hmax}$  orientation (parallel to the Hikurangi margin) within the central HSM (Hawke's Bay region) which rotates to a WNW- ESE  $S_{Hmax}$  orientation (roughly perpendicular to the Hikurangi margin) in the southern HSM. This rotation of  $S_{Hmax}$  orientation spatially correlates with along-strike variations in subduction interface slip behavior, characterized by creep and/or shallow episodic slip events in the central HSM and interseismic locking in the southern HSM. Observed borehole  $S_{Hmax}$  orientations are largely parallel to maximum contraction directions derived from geodetic surface deformation measurements, suggesting that modern stress orientations may reflect contemporary elastic strain accumulation processes related to subduction megathrust locking.

Plain Language Summary

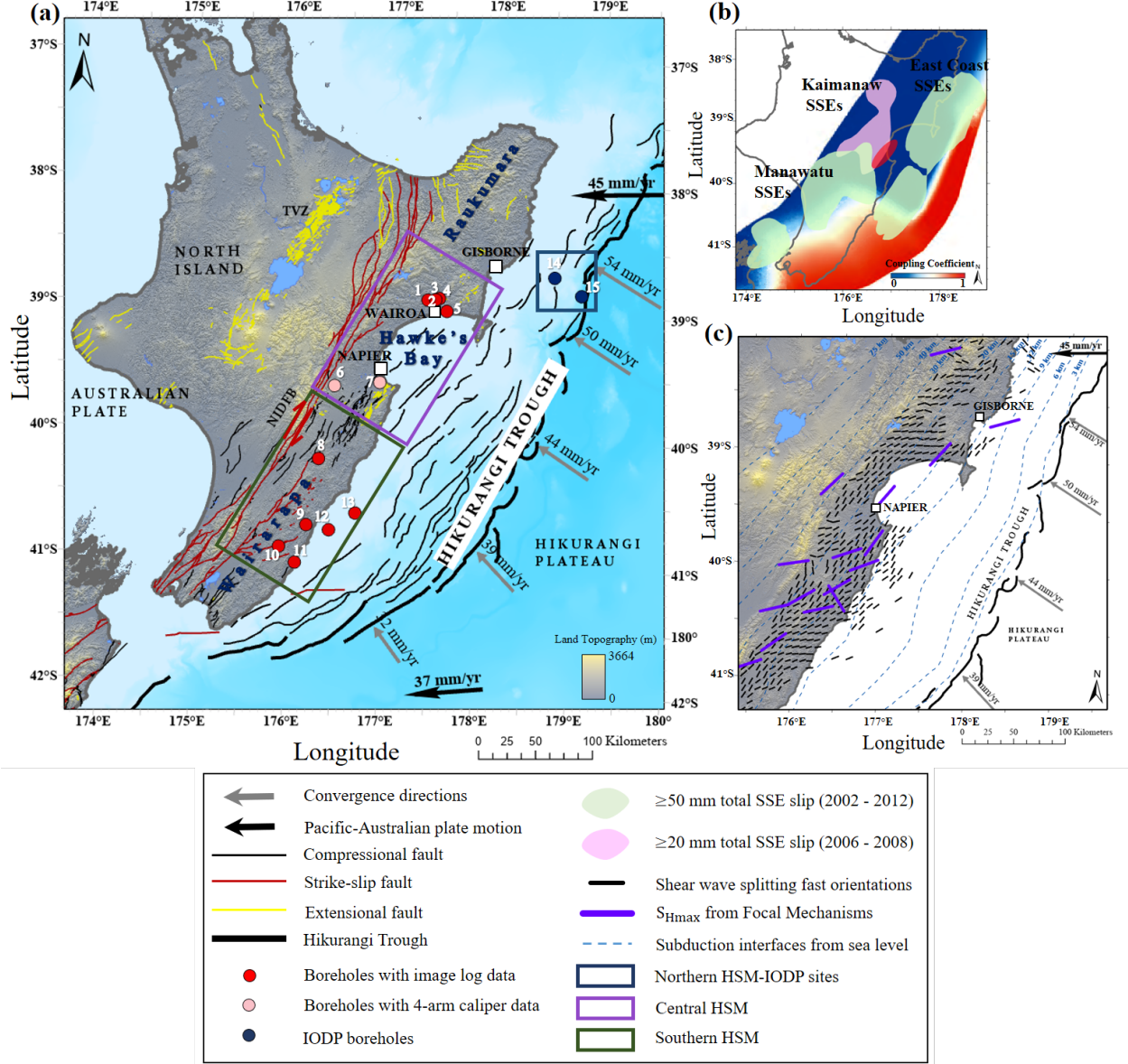
Movement along faults at tectonic plate boundaries can cause changes in the orientations of the forces, known as stress, that make them move. Such changes may help us explain how deformation at the surface occurs when these faults move, the way fluid moves along these faults, and why different types of earthquakes occur on these faults. The Hikurangi Subduction Margin, New Zealand’s largest and most hazardous plate boundary fault, shows a variety of deformation and earthquake types that occur in the over-riding plate which may be linked to stress orientation. In this study, we found that variability in the stress orientations within the upper plate of Hikurangi Subduction Margin matches areas where we see different earthquake types occurring, and observed patterns of surface deformation. We suggest that stress orientations reflect the accumulation and release of strain caused by subduction at the HSM.

## 1 Introduction

In-situ stress measurements can provide important insights into stress states at global and localized scales, the geomechanical state of earthquake-hosting faults, shear traction on faults, and processes of stress accumulation and release on plate boundary faults. Such measurements also assist with understanding how crustal stresses relate to strain observed geodetically and geologically (e.g., Zoback et al., 1987; Magee & Zoback, 1993; Townend & Zoback, 2006; Byrne et al., 2009; Chang et al., 2010; Lin et al., 2013, 2016; Brodsky et al., 2017). Earthquake occurrence and many earthquake rupture characteristics are partly dependent on the shear to normal stress ratio, which is a function of the relative magnitude of in-situ principal stresses, the orientation of the fault plane with respect to the orientation of the principal stress orientations, pore pressure, and fault plane friction coefficients (Jaeger et al., 2007; Schellart & Rawlinson, 2013; Vavryčuk, 2015). Additionally, earthquakes can redistribute stress and change both shear and normal stress on adjacent fault planes and surrounding rocks either statically (a shift in the stress state from before to after the earthquake) or dynamically (oscillating stress changes that occur with the passage of seismic waves) (Stein, 1999; Seeber & Armbruster, 2000; Hardebeck, 2004; Ma et al., 2005; Lin et al., 2007, 2016; Hardebeck & Okada, 2018).

The Hikurangi Subduction Margin (HSM), on the east coast of the North Island of New Zealand (Figure 1a), experiences strong along-strike variations in megathrust slip behaviour, ranging from deep interseismic locking (and stress accumulation) beneath the southern North Island, to episodic slow slip events (SSEs) and creep at the northern and central HSM (Figure 1b). Creep and shallow (<15 km depth) SSEs lasting for 2-3 weeks recur every 18-24 months offshore of the northern and central HSM (Wallace & Beavan 2010; Wallace, 2020; Figure 1b). Deep (>25 km), long-term (>1 year) slow slip events occur approximately every ~5 years at the southern HSM (Wallace & Beavan 2010), just down-dip of a portion of the plate interface that is strongly locked and accumulating stress likely to be released in a future great earthquake ( $M_w > 8.0$ ). Despite the recognized importance of in-situ stress states along active subduction zones in understanding strain accumulation and release, few studies have

been undertaken to directly estimate stress magnitudes in these settings (Chang et al., 2010; Huffman & Saffer, 2016; Lin et al., 2010, 2013, 2016; Malinverno et al., 2016; Brodsky et al., 2017; McNamara et al., 2021).



**Figure 1.** (a) Tectonic setting of East Coast of North Island, New Zealand. Fault traces from Barnes et al., (2010), Langridge et al., (2016), Mountjoy and Barnes (2011), and Pedley et al., (2010). Black arrows indicate the long-term motion of the Pacific relative to Australian Plate from DeMets et al., (1994)

and grey arrows show shortening rates at the Hikurangi Trough from Wallace et al. (2012). (b) Interseismic coupling based on campaign GPS velocities (1995–2008), shown in terms of coupling coefficient (Wallace et al. 2012a). Green and pink shaded regions represent the cumulative slow slips in 2002 and 2012 (Wallace et al., 2012a) and SSEs beneath the Kaimanawa ranges in 2006 and 2008 (Wallace & Eberhart-Phillips, 2013; Wallace, 2020). Area of possible locked patch between the East Coast and Kaimanaw SSEs is shaded in red. (c) Map showing  $S_{Hmax}$  orientations from focal mechanisms (Townend et al., 2012) and shear wave splitting fast orientations (Illsley-Kemp et al., 2019). Boreholes are numbered 1: Makareo-1, 2: Kauhauroa-2, 3: Waitahora-1, 4: Kauhauroa-5, 5: Tuhara-1A, 6: Kereru -1, 7: Whakatu-1, 8: Ngapaeruru-1, 9: Te Mai-2, 10: Rauni-2, 11: Orui-1A, 12: Titihaoa-1, 13: Tawatawa-1, 14: U1519A, and 15: U1518B. Abbreviations: NIDFB, North Island Dextral Fault Belt; TVZ, Taupo Volcanic Zone.

To date, several studies have been carried out to determine the contemporary in-situ stress patterns along the East Coast of the HSM. Analysis of earthquake focal mechanism solutions reveal that  $S_{Hmax}$  orientations in the crust (60 km depth) change from NE-SW (roughly margin-parallel; Figure 1c) in the northern and central Hikurangi margin to a more margin-oblique, ENE-WSW orientation, sub-parallel to Pacific/Australia relative plate motion, further south (Figure 1c). These measurements are largely from earthquakes within the subducting slab most located at depths >25 km depth (Townend et al., 2012). In contrast, the seismic anisotropy fast orientations determined from shear wave splitting methods that sample the upper ~40 km (Figure 1c) suggest a dominant  $S_{Hmax}$  orientation of NE-SW for most of the HSM forearc (generally margin-parallel), while the northern HSM forearc displays variable fast orientations, with a more dominant ENE-WSW inferred  $S_{Hmax}$  orientation (Illsley-Kemp et al., 2019). Shallow (<3km)  $S_{Hmax}$  orientations have been determined from limited analysis of borehole image logs from boreholes drilled onshore and offshore HSM (Heidbach et al., 2018; Lawrence, 2018; Griffin, 2019; Griffin et al., 2021; McNamara et al., 2021). Analysis of borehole image data from four onshore boreholes show NE-SW to ENE-WSW  $S_{Hmax}$  orientations in the central HSM (Heidbach et al., 2018; Lawrence, 2018;), and an E-W to NW-SE  $S_{Hmax}$  orientation is determined from two borehole image logs in the southern HSM (Heidbach et al., 2018; Griffin, 2019; Griffin et al., 2021). Boreholes offshore the northern HSM drilled as part of the International Ocean Discovery Program (IODP) Expeditions 372 and 375 show an E-W  $S_{Hmax}$  orientation close to the Hikurangi trench, and a NW-SE  $S_{Hmax}$  orientation in the offshore forearc (McNamara et al., 2021), indicating strong variations in stress orientations across the forearc.

In this study, we provide a detailed analysis of  $S_{Hmax}$  orientations from stress related drilling-induced borehole failures, and assess their variability within the upper plate of the HSM. We analyze six borehole image and oriented four-arm caliper logs (not previously used for stress orientation studies), and provide a re-analysis of the seven borehole image logs investigated in Heidbach et al. (2018), Lawrence (2018), Griffin (2019), and Griffin et al. (2021) with a focus on ac-

quiring higher resolution measurements (length, width, orientation) of induced borehole features. We then discuss spatial variations in contemporary  $S_{\text{Hmax}}$  orientations and their relationship to far-field stresses and long-term patterns of tectonic deformation, and their potential links to along-strike variations in subduction megathrust slip behavior.

## 2 Geological Setting

The Hikurangi Subduction Margin (HSM) lies along the Pacific-Australian plate boundary at the southern end of the Tonga-Kermadec Trench, off the east coast of the North Island, New Zealand (Figure 1a). The Hikurangi Subduction Margin accommodates westward subduction of the Hikurangi Plateau (a Cretaceous large igneous province) beneath the continental crust of North Island at the Hikurangi Trough (Davy, 1992). The Hikurangi Plateau is ~10-15 km thick and transitions to a more typical 5-7 km thick oceanic plate further north at the Kermadec Trench (Davy et al., 2008; Davy, 1992; Ghisetti et al., 2016; Mochizuki et al., 2019). The southern termination of the HSM is located somewhere beneath New Zealand’s northeastern South Island, where oblique convergence is transferred to the Marlborough Fault System and Alpine Fault in the South Island (Barnes et al., 1998; Little & Roberts, 1997).

Three major tectonic phases during the Neogene to present-day have been identified: 1) an early to middle Miocene compressional stage that resulted in extensive reverse faulting, folding, and tectonic uplift along the margin (Chanier et al., 1999; Barnes et al., 2002; Bailleul et al., 2013); 2) a mixed compressional and extensional stage from the mid-Miocene to early Pliocene resulting in widespread compressional tectonics and localized subsidence and normal faulting in the inner portion of the subduction wedge (Hawke’s Bay region) (Barnes et al., 2002); 3) a compressional stage associated with and structural inversion of listric thrust faults and folds during the Quaternary and rapid, late Quaternary uplift of the Coastal Ranges, Axial Ranges, and Raukumara Peninsula (Beanland & Haines, 1998; Nicol et al., 2002, 2007; Nicol & Beavan, 2003; Bailleul et al. 2013). Late Quaternary extensional faulting in the Raukumara Peninsula is likely the result of gravitational collapse due to rapid uplift (Berryman et al., 2009; Pettinga, 2004; Walcott, 1987).

Neogene to present tectonic deformation across the HSM is complex and includes contributions from shortening associated with subduction at the Hikurangi Trough, clockwise rotation of the East Coast forearc, strike-slip faulting along the North Island Dextral Fault Belt (NIDFB), and back-arc extension in the Taupo Volcanic Zone (TVZ) (Beanland & Haines, 1998; Wallace et al., 2004; Figure 1a). The East Coast forearc has rotated for at least the last few Myr at rate of  $3^{\circ}$ – $4^{\circ}$ /Myr relative to the Australian plate (Nicol et al. 2007). This rotation results in back-arc rifting in the central North Island’s Taupo Volcanic Zone (TVZ), transpression in the southern North Island, and creates a large along-strike change in convergence rate at the Hikurangi Trough, from 20 mm/year in the south to 60 mm/year at the northern Hikurangi Trough (Wallace et al. 2004; Figure 1a). Wallace et al. (2004) suggest that an along-strike change from



**Figure 2.** (a) Statically and dynamically normalized resistivity image log (FMI) showing borehole breakouts and natural fractures in borehole Tuhara-1A, (b) Dynamically normalized travel time and amplitude images from an acoustic image log (AFIT) acquired in Orui-1A borehole showing petal centerline fractures (PCFs), natural fractures, and a fault (observable offset of other geological features across a natural fracture). (c) Plot of an oriented four-arm caliper log (C1-C3 and C2-C4) from borehole Kereru-1. The 10% tolerance of bit size (black line) is shown as a grey shaded zone, plotted next to pad 1 azimuth and borehole orientation information showing caliper enlargement indicative of the presence of a borehole breakout.

Image log acquisition, data processing, and quality assessment is performed on all image logs, the details of which are documented in the supplemental information (Text S1 & S2).

From the borehole image logs, we identify stress-induced borehole failures, including borehole breakouts (BOs; Figure 2a & 2c), drilling-induced tensile fractures (DITFs), and petal-centerline fractures (PCFs; Figure 2b). BOs and DITFs are well-known indicators of horizontal in-situ stress orientations in vertical to semi-vertical boreholes, in which it is assumed one of the principal stresses is the vertical stress ( $S_v$ ). BOs and DITFs develop parallel to the contemporary minimum ( $S_{hmin}$ ) and maximum ( $S_{Hmax}$ ) horizontal stresses respectively (Bell, 2003; Bell & Gough, 1979; Aadnoy & Bell, 1998). In such cases, BOs and DITFs can also be used to determine  $S_{Hmax}$  orientations in boreholes deviated  $\geq 20^\circ$  as long as corrections are applied to address the impact of vertical stress ( $S_v$ ) on their development (Peška & Zoback, 1995). BOs form as enlargements of the borehole diameter on opposite sides of the borehole wall where the circumferential hoop stress, induced by non-uniform horizontal principal stress magnitudes, is large enough to exceed the rock strength (Bell & Gough, 1979; Zoback, 2007). Borehole breakouts typically appear on resistivity image logs as a pair of wide, conductive (in water-based mud) or resistive (in oil-based mud, such as OBMI tool; King et al., 2010) zones. In acoustic televiewer logs, they appear as low amplitude, out-of-focus zones (Figure 2a). In both types of logs, BOs are located  $\sim 180^\circ$  from each other around the circumference of the borehole wall. BOs often correlate with borehole enlargement and associated large caliper values as the result of the borehole failure (Figure 2c; Tingay et al., 2008). Oriented four-arm caliper data is also used to infer the presence of BOs along boreholes. To reliably distinguish BOs from other non-stress related features that affect borehole shape, such as keyseats and washouts, we apply the criteria presented by Reinecker et al., (2003).

DITFs develop on the borehole wall where there is a significant difference between the two horizontal principal stress magnitudes and the local stress concentrations around the borehole wall lead to hoop stresses that overcome the tensile strength of the rock (Brudy & Zoback, 1999; Zoback, 2007; Barton & Moos, 2010). DITFs typically appear as narrow, conductive (on resistivity image logs) or low amplitude and longer travel time (on acoustic image logs) pairs,

$\sim 180^\circ$  from each other around the circumference of the borehole wall. DITFs are generally parallel or slightly inclined to the borehole axis in vertical to semi-vertical boreholes (Barton et al., 1998; Bell, 2003; Tingay et al., 2008; Rajabi et al., 2016a, 2016b). In this study, all BOs and DITFs are reported as individual feature length and width, such that a single BO or DITF measurement does not span a number of separate individual BOs or DITFs, similar to what has been done in previously analyzed HSM image logs (Lawrence, 2018; Griffin, 2019). This is an important aspect of quantifying induced features from borehole image logs because geological properties, such as varying strength associated with variably bedded lithologies, impact the development and growth (both width and length) of borehole breakouts (Kingdon et al., 2016; Fellgett et al., 2019). It is also important to capture each induced feature individually for accurate statistical considerations of borehole stress orientations.

PCFs are induced fractures that form within the bedrock ahead of the drill bit in response to stress concentrations at the bottom of the borehole during drilling, and propagate inward towards the borehole (Li & Schmitt, 1998; Davatzes & Hickman, 2010; Wenning et al., 2017). PCFs appear as conductive (resistivity image logs) or low amplitude (acoustic image logs) partial sinusoids that merge into discontinuous borehole axial centerline fractures (Figure 2b; Kulander et al., 1990). The average of the centerline fracture orientations or dip orientation of the partial sinusoids of a PCF is parallel to the orientation of  $S_{\text{hmin}}$  (Davatzes & Hickman, 2010). In contrast to the DITFs, the centerline portions of PCFs are often less than  $180^\circ$  apart from each other around the circumference of the borehole wall.

Finally, we use the A–E World Stress Map (WSM) quality ranking system and circular statistical analysis for stress orientation indicators (Heidbach et al., 2016). The borehole locations, image log intervals,  $S_{\text{Hmax}}$  orientation mean, standard deviation, and the quality classification are based on the length-weighted method (Heidbach et al., 2016) for individual boreholes are summarized in Table 1 and Table 2.

## 4 Results

### 4.1 Central HSM (Hawke’s Bay region)

A total of 810 BOs with a combined length of 454 m are identified from borehole image logs and oriented four-arm caliper logs acquired in Kauhauroa-2, Kauhauroa-5, Makareao-1, Tuhara-1A, Kereru-1, and Whakatu-1 boreholes in the Central HSM region (Figure 3; data set 1; see Fig. 5 for the borehole locations and names). Using only BOs from boreholes with B-C quality rankings (following the WSM criteria), and so more likely to display far-field stress orientation measurements, a dominant  $157^\circ/337^\circ \pm 18^\circ$  orientation is observed, indicating a NW-SE  $S_{\text{hmin}}$  orientation, from which we infer an  $S_{\text{Hmax}}$  orientation of  $067^\circ/247^\circ$  (ENE-WSW) (Figure 3). The only exception is borehole Whakatu-1 (WSM D quality ranking), in the southeast area of the central HSM, which shows a dominant BO orientation of  $054^\circ/234^\circ \pm 13^\circ$  (NE-SW), from which we

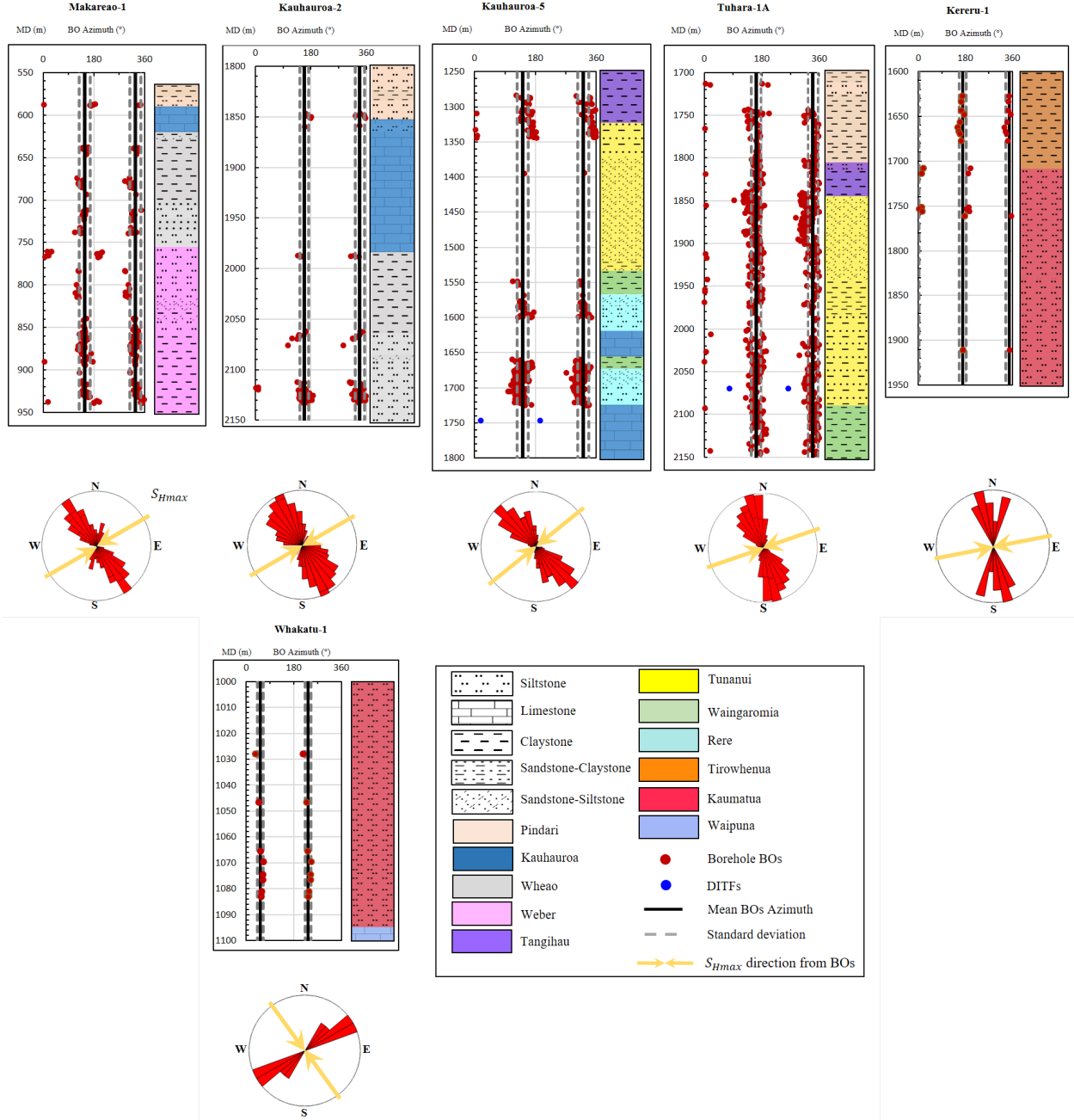


infer a NW-SE  $S_{Hmax}$  orientation ( $144^\circ/324^\circ$ ) (Table 1; Figure 3). 2 DITF pairs are observed in boreholes Kauhauroa-5 and Tuhara-1A with mean  $S_{Hmax}$  orientation of  $020^\circ/195^\circ$  (NNE-SSW) and  $079^\circ/263^\circ$  (ENE-WSW), respectively (Figure 3). No BOs, DITFs, or PCFs are observed in Waitahora-1 borehole from OBMI image logs (this image log only provided ~37% coverage of borehole wall) or from oriented four-arm caliper data.

**Table 1.** Stress Indicators From Analysis of Borehole Image Logs and Oriented Four-Arm Caliper Data in the Central HSM, New Zealand.

Borehole ID	Year	Max borehole Deviation ( $^\circ$ )	Tool name coverage (%)	Borehole image coverage interval (m MD)	Image feature type	Feature Number	Mean $S_{Hmax}$ ( $^\circ$ )	S.D.	Total length (m)	Quality
North-central HSM	Kauhauroa-2		FMI <sup>TM</sup>	-	BO	2138.5	$^\circ/249^\circ$			C
	Kauhauroa-5		FMI <sup>TM</sup>	-	BO	1750.2	$^\circ/232^\circ$ - $020^\circ/195^\circ$	3.1		B
	Makareo-1		FMI <sup>TM</sup>	-	BO	939.7	$^\circ/238^\circ$			B
	Tuhara-1A		FMI <sup>TM</sup>	-	BO	2148	$^\circ/251^\circ$ - $079^\circ/263^\circ$	0.16		B
	Tuhara-1A		FMI <sup>TM</sup>	-	DITF					D
South-central HSM	Koruru-1		-	-	BO	1920	$^\circ/259^\circ$			C
	Koruru-1		arm caliper							
	Whakatu-1		-	-	BO	1400	$^\circ/324^\circ$			D
	Whakatu-1		arm caliper							

Note.  $S_{Hmax}$  azimuth means, standard deviations (S.D.), and data quality ranking are calculated according to World Stress Map conventions (Heidbach et al., 2016).



**Figure 3.** Graph of BO azimuths (red dots), DITF azimuths (blue dots), and stratigraphy column against measured depth (m MD) for boreholes at the central HSM. Mean BO azimuths and the standard deviation for individual borehole are plotted in black and dashed grey lines respectively. Bi-directional rose

diagram of breakout orientations for each borehole is shown below BO panels.

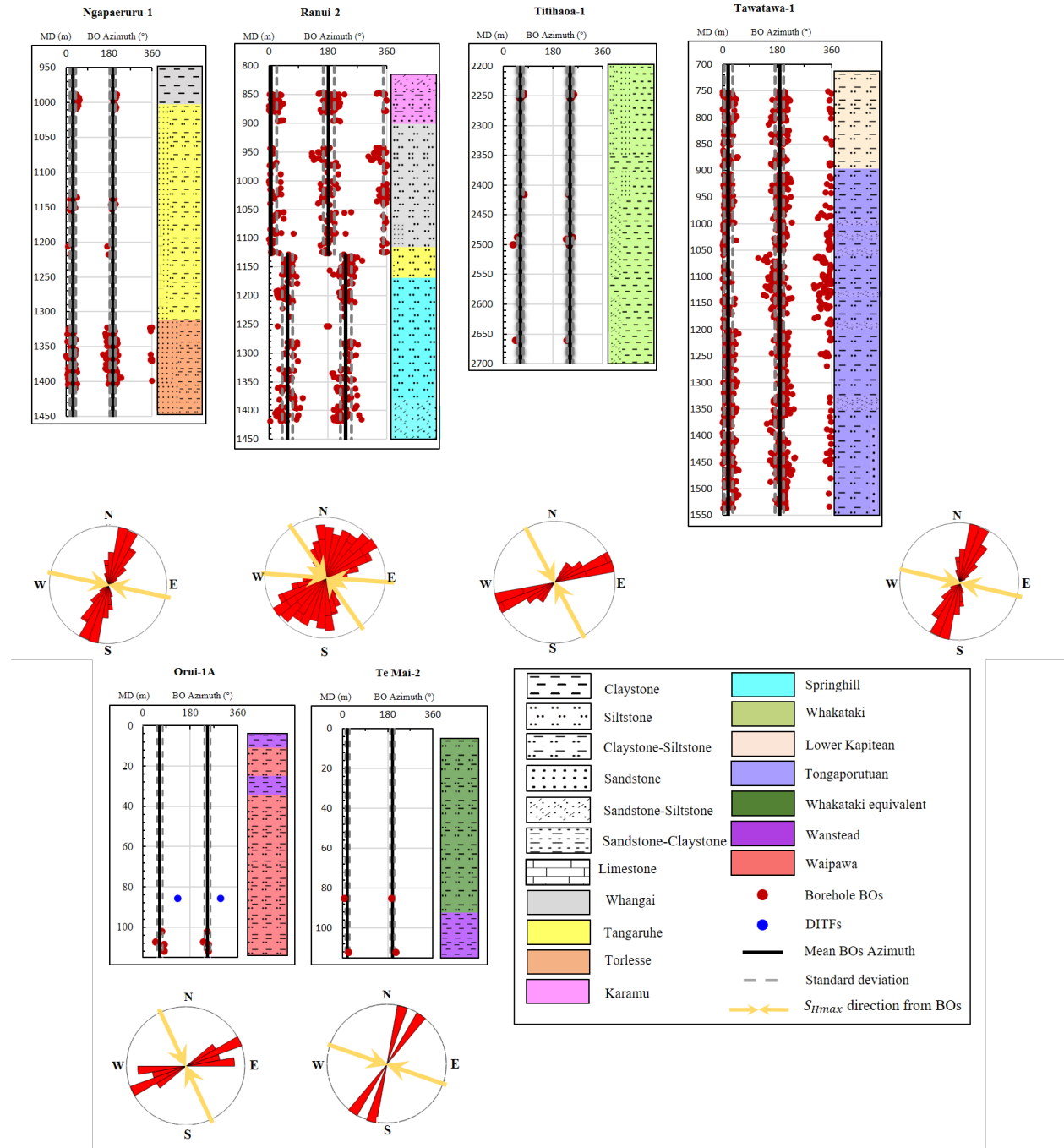
#### 4.2 Southern HSM

A total of 1517 BOs with a combined length of 520 m are identified from borehole image logs in boreholes Ngapaeruru-1, Rauni-2, Titihaoa-1, Tawatawa-1, Te Mai-2, and Orui-1A boreholes (Figure 4; data set 1). For borehole stress data with a WSM quality ranking of B-C (Ngapaeruru-1, Tawatawa-1, and Ranui-2) we observe an  $S_{\text{hmin}}$  orientation of  $016^\circ/196^\circ \pm 21^\circ$  (NNE-SSW) from which we infer an  $S_{\text{Hmax}}$  orientation of  $106^\circ/286^\circ$  (WNW- ESE) (Figure 4). BOs in boreholes Ngapaeruru-1, Tawatawa-1, Te Mai-2, and the shallow ( $<1130$  m MD) interval of Ranui-2 show a consistent WNW-ESE  $S_{\text{Hmax}}$  orientation (Figure 4), whereas BOs measured in boreholes Titihaoa-1, the deeper ( $>1130$  m MD) imaged interval of Ranui-2, and Orui-1A provide dominantly NW-SE  $S_{\text{Hmax}}$  orientations (Figure 4). Our reanalysis of BOs from borehole Ranui-2 suggest a  $51^\circ$  clockwise  $S_{\text{Hmax}}$  orientation rotation from E-W ( $094^\circ/274^\circ \pm 17^\circ$ ) in the shallower imaged depth interval (842-1130 m MD) to NW-SE ( $145^\circ/325^\circ \pm 16^\circ$ ) in the deeper imaged interval (1130-1422 m MD) (Table 2) that was first reported by Griffin (2019).

**Table 2.** *Stress Indicators From Analysis of Borehole Image Logs in the Southern HSM, New Zealand.*

Borehole ID	Year	Max bore-hole deviation (°)	Tool name	% Bore-hole surface coverage	Image in-survey (m MD)	Feature type	Number	Mean $S_{\text{Hmax}}$ (°)	S.D	Total length (m)	Quality
Southern HSM 1	Ngapaeruru-1	17.78	FMI <sup>TM</sup>	-	1417	BO	1	$^\circ/292^\circ$		49	B
	Rauni-2*	25.4	FMI <sup>TM</sup>	-	1130-1422	BO	1	$^\circ/274^\circ 16^\circ$		0.8	D
	Te Mai-2		AFIT <sup>150</sup>	-	147.5	BO	1	$^\circ/289^\circ$		0.2	C
	Orui-1A		AFIT <sup>150</sup>	-	114.5	PCF	1	$^\circ/335^\circ - 125^\circ$		0.2	D
Titihaoa-1			FMI <sup>TM</sup>	-	2741	BO	1	$^\circ/332^\circ$		0.2	D
Tawatawa-1			STAR	-	1540	BO	1	$^\circ/283^\circ$			B

Note.  $S_{Hmax}$  azimuth means, standard deviations (S.D.), and data quality ranking are calculated according to World Stress Map conventions (Heidbach et al., 2016). \*Measured stress feature orientation are not corrected for borehole deviations  $\geq 20^\circ$ .

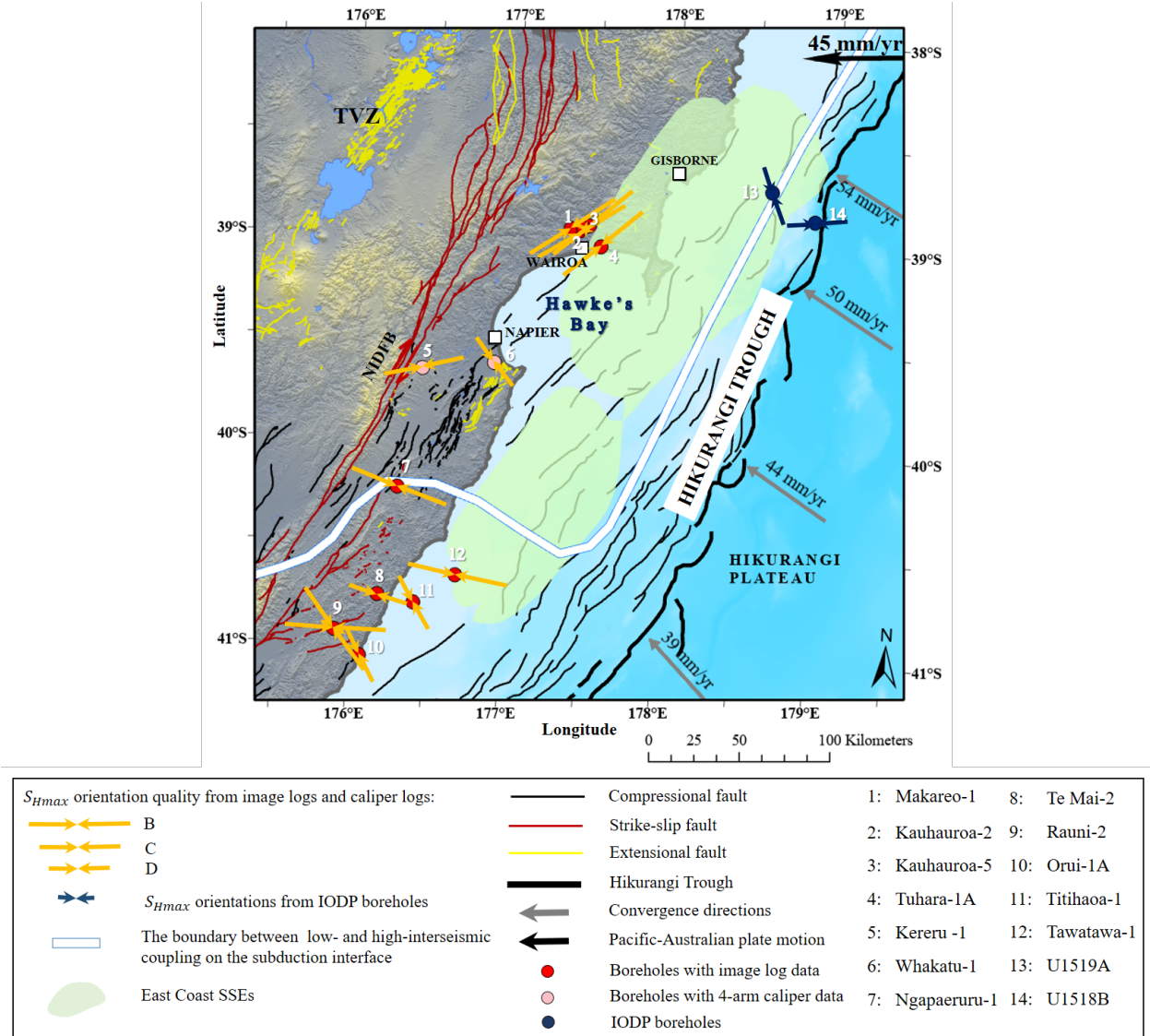


**Figure 4.** Graph of BO azimuths (red dots), DITF azimuths (blue dots), and stratigraphy column against measured depth (m MD) for boreholes at the south-

ern HSM. Mean BO azimuths and the standard deviation for individual borehole are plotted in black and dashed grey lines respectively. Bi-directional rose diagram of breakout orientations for each borehole is shown below BO panels.

## 5 Discussion

Our results show that the contemporary  $S_{Hmax}$  orientations in the upper plate of the HSM change from dominantly NE-SW, parallel to the subduction margin, within the central HSM to WNW-ESE/NW-SE within the southern HSM (Wairarapa region), roughly perpendicular to the subduction margin (Figure 5). This along-strike rotation in HSM  $S_{Hmax}$  orientations may be explained in a few ways; 1) HSM kinematics, 2) long-term tectonic deformations, and 3) lateral variations in basement topography.



**Figure 5.** Map of  $S_{Hmax}$  at the East Coast of North Island determined from borehole Breakouts in (orange arrows) and IODP borehole image analysis from McNamara et al., 2021 (blue arrows). Green shaded region represents the East Coast cumulative slow slip (Wallace et al., 2012a). Active faults (normal faults: yellow; strike slip: red; reverse fault: black) traces from Litchfield et al. (2014) and Langridge et al. (2016). The bold black line shows the Hikurangi Through. Black arrow indicate the relative convergence vector between the Pacific and Australian Plates from DeMets et al., (1994) and grey arrows show shortening rates at the Hikurangi Trough from Wallace et al. (2012). Abbreviations:

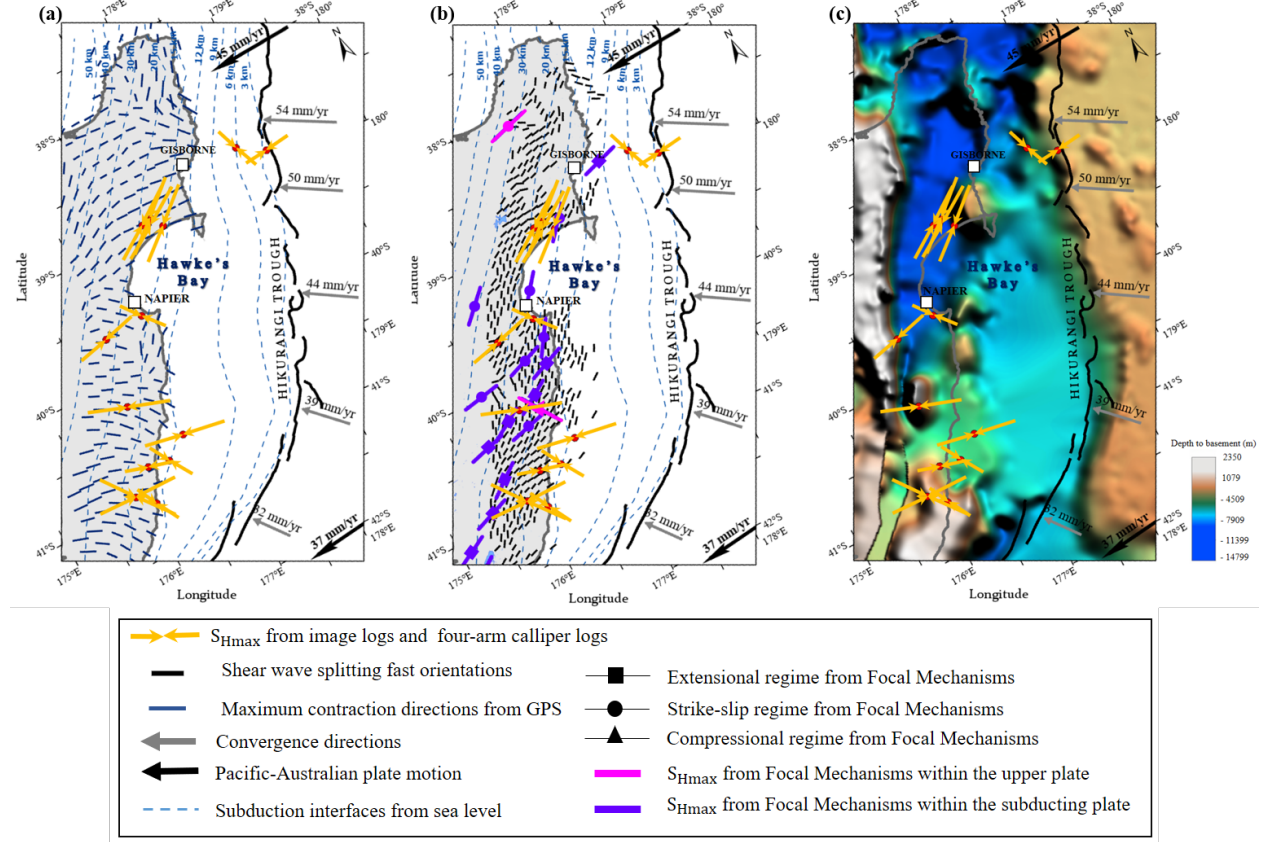
NIDFB, North Island Dextral Fault Belt; TVZ, Taupo Volcanic Zone.

Geodetic measurements over the last 25 years have been used to determine New Zealand’s contemporary surface strain field (Dimitrova et al., 2016; Haines & Wallace, 2020). The rotation of borehole-derived  $S_{Hmax}$  orientations along the HSM in the upper plate is remarkably consistent with the variation in coupling behavior on the HSM subduction interface (Figure 1b) and the along-strike rotation observed in the maximum contraction directions determined from geodetic measurements along the HSM forearc (Dimitrova et al., 2016; Haines & Wallace, 2020; Figure 6a). Maximum contraction directions determined from campaign GPS data reveal that the central HSM has a dominant E-W maximum contraction direction, whereas the southern HSM shows a NW-SE contraction direction (Figure 6a; Haines & Wallace, 2020), broadly compatible with the borehole-derived  $S_{Hmax}$  orientations reported here. The along-strike variations in maximum contraction directions from GPS are suggested to be related to along-strike changes in interseismic coupling on the HSM plate interface (Wallace et al., 2004; Dimitrova et al., 2016). In the northern and central HSM, the subduction interface is largely creeping and experiences shallow (<15 km), episodic slow slip events on the offshore. At the southern HSM the plate interface is strongly interseismically coupled to ~30 km depth, and is currently accumulating elastic strain in the surrounding crust that will eventually be relieved in future large earthquakes (Wallace, 2020; Figure 1b). The strong agreement between the geodetic maximum contraction directions and the observed stress field from the borehole observations indicate that  $S_{Hmax}$  orientations and their variability at HSM are strongly influenced by along-strike variations in elastic strain accumulation in the overriding plate due to changes in interseismic coupling on the subduction interface.

In the central HSM (where the plate boundary is largely creeping) borehole-derived  $S_{Hmax}$  orientations and maximum contraction directions are reasonably consistent and sub-parallel to far-field relative Pacific-Australian plate motion. In contrast, at the southern HSM borehole-derived  $S_{Hmax}$  orientations and maximum contraction directions are roughly perpendicular to far-field relative Pacific-Australian plate motion, but are parallel to the convergence direction. This observation may be due to the fact that the subducting plate drags the forearc wedge in the direction of subduction and increases elastic compression strain and stress on the plate interface and within the forearc itself aligning elastic strain accumulation and  $S_{Hmax}$  stress orientations into that orientation. These  $S_{Hmax}$  orientation observations are at odds with those of Townend and Zoback (2006) showing that stress orientations in central Japan (from earthquake focal mechanisms) do not agree with maximum contraction directions associated with cyclical subduction zone locking. This difference in the conclusions between our study and Townend and Zoback (2006) may be related to the fact that we utilize shallow (<3 km) stress orientations, which may be more susceptible to temporal changes in elastic strain resulting from interseismic coupling rather than stress orientations from earthquake focal mechanisms sampling greater depths. This observation at the HSM may be reflecting longer-term ac-



cumulation of stress (related to long-term tectonic processes) independent of stage within the earthquake cycle.



**Figure 6.** (a) Map of maximum contraction directions from GPS data (Haines & Wallace, 2020) and borehole-derived  $S_{Hmax}$  orientations (orange arrows) and IODP borehole image analysis from McNamara et al. (2021) (blue arrows). (b) Map of  $S_{Hmax}$  orientations and inferred faulting regime from focal plane mechanisms (0-60 km; square: extensional, circle: strike-slip, and triangle: compressional regime; Townend et al., 2012), seismic anisotropy measurements (0-40 km; black lines). Dashed blue lines show depth of subduction interface from sea level (Williams et al., 2013). (c) The map showing depth to basement map of North Island adapted from FROGTECH (2014). The clockwise rotation of  $S_{Hmax}$  orientation along the HSM strike follows the basement topography. Black arrows indicate the long-term motion of the Pacific relative to Australian Plate from DeMets et al., (1994) and grey arrows show shortening rates at the Hikurangi Trough from Wallace et al. (2012). Red dots show the borehole locations.

Although borehole-derived  $S_{Hmax}$  orientations at the HSM are broadly consistent with maximum contraction directions,  $S_{Hmax}$  orientations are not uniform

within the forearc and in places deviate from the observed maximum contraction directions (Figure 6a). Some of these variabilities may be due to longer-term partitioning of oblique relative motion and strain into margin-parallel, margin-perpendicular, and strike-slip components. Similar deviations from maximum contraction directions are observed within the Nankai subduction zone (Chang et al., 2010) and Costa Rica margin (Malinverno et. al, 2016). For example, borehole-derived  $S_{Hmax}$  orientations in the accretionary prism across the Nankai subduction zone are subparallel to the plate convergence vector between the Philippine Sea plate and Japan, perpendicular to the plate boundary, and for one borehole in the shelf edge is parallel to the plate boundary (Lin et al., 2010; Chang et al. 2010; Wu et al. 2012). The variations of stress among these sites and the deviation of borehole-derived  $S_{Hmax}$  orientations from the plate motion vectors derived from GPS data are suggested to be attributed to the strain partitioning into trench-parallel, right-lateral slip and thrust tectonics due to oblique plate convergence (Tobin et al. 2009; Lin et al. 2010). Alternatively, such stress variations have also been attributed to other factors such as thrusting and bending within individual geologic domains and local extension deformations derived by gravitation collapse of the prism in the forearc (Chang et al., 2010; Lin et al., 2016).

Townend et al. (2012) derived  $S_{Hmax}$  orientations from earthquake focal mechanisms using a Bayesian approach for earthquake data between 2004-2011 with  $M_L > 3$ . Their observations reveal that  $S_{Hmax}$  orientation changes from NE-SW in the central HSM to a more oblique  $S_{Hmax}$  orientation, sub-parallel to Pacific-Australia relative plate motion, in the southern HSM (Figure 6b). Only two focal mechanism solutions are located within the upper plate of the HSM or near the subduction interface; one strike-slip event with a NE-SW  $S_{Hmax}$  orientation (latitude 38°S; North of central HSM) at 7 km depth, and one compressional event with a WNW-ESE  $S_{Hmax}$  orientation (latitude 40.5°S; southern HSM) at 25 km depth (at the top of subducting plate near the subduction interface; Figure 6b). In the central HSM (where the plate boundary is largely creeping) borehole-derived NE-SW  $S_{Hmax}$  orientations and maximum contraction directions agree with the NE-SW  $S_{Hmax}$  orientations derived from focal mechanism inversions within the upper plate and subducting plate, implying that far-field plate boundary forces exerted at the HSM primarily control the present-day crustal stresses in the upper plate in this area. In contrast, the southern HSM shows stress field rotation with depth from borehole-derived WNW-ESE/NW-SE  $S_{Hmax}$  orientations (roughly margin-perpendicular) in the shallow crust of upper plate to NE-SW/ ENE-WSW focal mechanism-derived  $S_{Hmax}$  orientations within the subducting plate (Figure 6b). The NE-SW/ ENE-WSW  $S_{Hmax}$  orientations derived from focal mechanism inversions indicate a normal or strike-slip tectonic regime within the subducting plate of the southern HSM. There is one compressional event at ~25 km depth (near the subduction interface) where the borehole-derived  $S_{Hmax}$  orientation agrees with a focal mechanism-derived WNW-ESE  $S_{Hmax}$  orientation (latitude 40.5°S; Figure 6b). This implies that the overriding plate broadly is in a condition of horizontal compression parallel

to convergence direction, potentially as deep as the plate interface ( $\pm 10$  km) (barring localized variations) and the tectonic regime becomes more strike-slip and normal within the subducting plate. The change in stress orientation with depth in the southern HSM is more compatible with a theoretically mechanically weak plate interface with low resolved shear stress and normal effective stress on the plate interface. The fact that the upper plate is in the state of horizontal compression parallel to plate convergence, on the other hand, implies that contemporary  $S_{Hmax}$  orientation is being driven by subduction of Hikurangi Plateau beneath North Island. Taking these observations into consideration, we propose that plate interface remains mechanically weak along the whole HSM and that a small increase of elastic compression strain and stress caused by the interseismically coupled southern HSM interface is sufficient to rotate  $S_{Hmax}$  orientation in the upper plate toward the subduction direction.

More recently, Illsley-Kemp et al. (2019) measured seismic anisotropy using shear wave splitting fast orientations from earthquake data in 2005–July 2018 with  $M_L > 0$ . Some studies consider fast orientations as a proxy for  $S_{Hmax}$  orientation if other significant crustal anisotropies are not present (e.g. fracturing, faulting, grain and crustal preferred orientations). The seismic anisotropy was derived from events 40 km deep and fast orientations were dominantly NE-SW (margin-parallel) for most of the HSM forearc, and more ENE-WSW in the northern and central HSM (Figure 6b). With the exception of some portions of the central HSM, the fast directions from shear-wave splitting studies do not agree well with the  $S_{Hmax}$  orientations we measure in the shallow boreholes. This could mean either (a) that the shear wave splitting fast directions are not controlled by contemporary  $S_{Hmax}$  orientation, or (b) that the fast directions are mainly controlled by structural features such as faults and the stress state at greater depths, which may be different than the near-surface which our study samples. In fact, propagating waves sample the volume of crust above the hypocenter without taking the variation of anisotropic with depth into account.

Long-term tectonic deformation resulting from rapid clockwise rotation of the Hikurangi forearc (Wallace et al. 2004) may also possibly explain the along-strike variation in  $S_{Hmax}$  orientation. The clockwise rotation of forearc, which accommodates the margin-parallel component of oblique Pacific-Australian plate motion, results in significant tectonic transitions along the strike (Nicol et al., 2007; Wallace et al., 2004). Tectonic regime varies from back-arc rifting within the TVZ in the central part of North Island, strike-slip and normal faulting onshore of the northern and central HSM to transpression and reverse faulting at the southern HSM (Figure 5). The rotation of  $S_{Hmax}$  orientations from margin-parallel in the onshore central HSM to margin-perpendicular in the southern HSM likely reflects this transition in the tectonic regime, such that the NE-SW  $S_{Hmax}$  orientation in the central HSM reflects margin-normal extension due to the transmission of slab rollback forces across the forearc and into the adjacent extensional back-arc rift (Wallace et al., 2012b). The clockwise rotation of the Hikurangi forearc may also explain why our observed contemporary  $S_{Hmax}$  orientation of NE-SW is not consistent with active large-scale NE-SW striking

compressional faults in the central HSM. The imaged intervals of the central HSM boreholes are located within the hanging walls of active NE-SW striking compressional faults and within NE-SW oriented fault-bend fold axes identified from seismic reflection profiles (Western Energy New Zealand, 2001; Barnes et al., 2002). It is possible that the deformation and growing rate of these reverse faults within the central HSM have changed through time, allowing forces exerted by forearc rotation surpass the NW-SE compression stress on these active faults. In this case, the rotation of the forearc, which accommodates the margin-parallel component, induces a NE slip motion on these pre-existing faults. This also suggests that these reverse faults in the context of current stress field could be currently active as strike-/oblique-slip faults. Another possibility is that due to frequent earthquakes in this region, the  $S_{Hmax}$  orientation within the central HSM has changed from a potential NW-SE orientation perpendicular to the margin, compatible with the orientation of observed reverse faults and fold axes, to the contemporary NE-SW orientation subparallel to the margin. During the interseismic period, strain and stress accumulation along the reverse faults and subduction interface drives compression in the upper plate parallel to convergence direction. Following great earthquakes or frequent earthquakes, the margin-perpendicular component is reduced due to post-seismic stress release, allowing a strike-slip motion in direction of long-term oblique relative plate motion on these faults. This implies that the stress state associated with seismicity perturbations is quite long lasting (these boreholes are drilled over the course of 4 years) such that stress state require a long time to recover or the perturbations were significant enough to permanently reorient the stress. In this scenario, the intermediate principal stress ( $S_{hmin}$ ) and minimum principal stress ( $S_v$ ) would switch and principal stresses re-orient in response to forces exerted by long-term relative plate motion and fluctuations in the magnitude of stress parallel to plate convergence, modulated by the seismic cycles. Sacks et al. (2013) and Moore et al. (2013) used a similar concept to explain the contrast between  $S_{Hmax}$  orientations and normal fault strikes within Kumano Basin of the Nankai subduction zone.

Lateral variations in surface and basement topography may also play a role in the observed along-strike variation in upper plate borehole-derived  $S_{Hmax}$  orientations (Figure 6c). Basement structures such as faults, folds, and seamounts that are not covered by thick sediments can cause significant stress rotation at both regional and large scales by introducing geomechanical inhomogeneities and lateral discontinuities (Gale et al., 1984; Enever et al. 1999; Rajabi et al., 2016a). In fact, the presence of seamounts on the incoming plate have been suggested as a possible localized effect on stress field orientations and shear-wave splitting fast directions in the offshore northern HSM (McNamara et al., 2021; Zal et al., 2020). The SEEBASE™ model of New Zealand, a depth to basement map based on the integrated interpretation of gravity, magnetic, borehole, and seismic data (Figure 6c) clearly shows a significant change in sediment thickness overlying the basement rocks, and basement topography along the HSM margin (FROGTECH, 2014). The onshore northern and central HSM basement is

located at depths ~9-15 km and covered by thick Neogene sediments, whereas at the onshore and offshore southern HSM the Mesozoic greywacke basement is uplifted and located at relatively shallow depths ( $<5$  km), and in some locations above sea level. Thin sediment packages directly overlying mechanically strong basement rocks, may be more reflective of the tectonic stresses experienced by the basement. Hence, it is possible that the basement compressional structures striking NNE/NE-SSW/SW control the observed margin-perpendicular, NW-SE  $S_{Hmax}$  orientation within the shallow crust of the southern HSM.

In addition to large-scale stress variations, localized variations have been observed between and within individual boreholes which could be attributed to local active geological structures such as faults, surface topography, and variable mechanical properties. For instance a localized NW-SE  $S_{Hmax}$  orientation ( $144^\circ \pm 11^\circ$ ) is noted from four-arm caliper data in borehole Whakatu-1 (south of Napier; Figure 5), perpendicular to the dominant NE-SW  $S_{Hmax}$  orientation of the central HSM. The NW-SE  $S_{Hmax}$  orientation in Whakatu-1 is margin-perpendicular implying a localized compressional tectonic regime at this locale, which agrees well with observed onshore and offshore active, NNE-SSW striking, compressional faults in this region (Figure 5; Litchfield et al. (2014); Langridge et al, (2016)), such as the reverse fault responsible for growth of the Cape Kidnapper’s anticline (Hull, 1987). Furthermore, Dimitrova et al. (2016) reported a possible locked patch in southern central HSM between shallow SSEs on the East Coast and deep Kaimanawa SSEs west of the East Coast (Figure 1b). Downdip changes in interseismic coupling behavior of the subduction interface and the accumulated strain associated with the locked patch could also be influencing the compressional tectonic regime in this region and borehole Whakatu-1.

## 6 Conclusions

This paper presents the first comprehensive analysis of contemporary  $S_{Hmax}$  orientations along the HSM, and discusses stress field orientation variability within the context of variable tectonics and slip behavior of this subduction margin.  $S_{Hmax}$  orientations in the central HSM are predominately NE-SW (sub-parallel to plate boundary), which rotates to a dominantly WNW-ESE  $S_{Hmax}$  orientation in the southern HSM (approximately perpendicular to the plate boundary). Our borehole-derived  $S_{Hmax}$  orientations agree with the maximum contraction strain directions from GPS measurements along the HSM suggesting that the observed stress orientations along the HSM are influenced by elastic strain accumulation due to interseismic coupling on the Hikurangi subduction interface. The long-term tectonic deformation arising from rapid rotation of the Hikurangi forearc, causing reverse faulting and strike-slip in the southern part of the margin and a combination of extension and strike-slip in the northern and central margin and the basement topography may also be at play in influencing the along-strike variations in observed stress orientations. In the southern HSM, borehole-derived  $S_{Hmax}$  orientations are inconsistent with  $S_{Hmax}$  orientations derived from focal mechanism solutions in the subducting plate, implying that the southern HSM interface is mechanically weak. Further interpretation of

HSM stress state could be achieved by constraining stress magnitudes, which will be the focus of future studies.

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### Data Availability Statement

This research used data provided by the New Zealand Petroleum and Minerals group (NZPM) within the Ministry for Business, Innovation and Employment (MBIE). The borehole image logs and oriented four-arm caliper data used in this paper can be accessed through MBIE's database. All additional data used in this article was collected from published sources referenced in the text. In Supporting Information, data set 1 contains all borehole breakouts presented in this study.

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