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*Geophysical Research Letters*

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Supporting Information for

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**Complex 3D Migration and Delayed Triggering of Hydraulic Fracturing-  
Induced Seismicity**

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**Introduction**

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This Supporting Information provides additional texts, figures, and tables to further  
support the arguments and findings presented in the main text. Texts S1 and S2 present  
the technical details of CC calculation and poroelastic modeling, respectively. Figure S1  
displays the histogram of the 49 poorly correlated small earthquakes. Figure S2 shows the  
 $\Delta P$  contribution in determining the  $\Delta CFS$  with different permeabilities for the Mw 3.9  
event. Table S1 summarizes the solid and fluid properties of each layer used in the  
poroelastic model. Table S2 presents the injection data.

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## 32 Text S1. Technical Details of CC Calculation

33 When performing the waveform cross-correlation, the seismic waveforms are band-  
 34 pass filtered from 1 to 10 Hz (*Schmittbuhl et al.*, 2016; *Warren-Smith et al.*, 2017, 2018).  
 35 The cross-correlation window is set to be 10 s, starting from 1 s before to 9 s after the  
 36 theoretical predicted S-arrival (*Schultz et al.*, 2017) based on the ak135 velocity model  
 37 (*Kennett et al.*, 1995). The choice of a 10-s window length is meant to capture the  
 38 strongest and cleanest arrival and sufficient coda waves with a lower level of noise  
 39 contamination. We do not choose a window starting from the P phase because the P  
 40 waves are very small compared with the S phases, thus the result can be easily  
 41 contaminated by noise (*Schultz et al.*, 2017). The correlation is performed by sliding the  
 42 waveform of one event from 4 s before the predicted S arrival of the other event to 4 s  
 43 after, in one-sample increments. A  $\pm 4$  s shift should be adequate to account for any  
 44 predicted phase onset error due to an imperfect velocity model. The maximum value of  
 45 the CC results during the sliding is defined as the final CC value of the event pair.

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## 47 Text S2. Technical Details of Poroelastic Modeling

48 By assuming that the medium is homogeneous and isotropic, the evolution of pore  
 49 pressure can be calculated by solving the coupled diffusion equations, as listed below  
 50 (equivalent forms of the equations can be found in the literature, e.g., *Wang and Kumpel*,  
 51 2003),

$$52 \quad \rho S \frac{\partial p}{\partial t} - \nabla \cdot \left( \rho \frac{\kappa}{\mu_d} \nabla p \right) = Q_m(x, t) - \rho \alpha \frac{\partial \varepsilon_{vol}}{\partial t} \quad (1)$$

$$53 \quad S = \chi_f \theta + \chi_p (1 - \theta) \quad (2)$$

$$54 \quad q = -\frac{\kappa}{\mu_d} \nabla p \quad (3)$$

55 where  $\rho$  is the pore fluid density,  $S$  is the linearized storage parameter,  $p$  is the fluid pore  
 56 pressure,  $\kappa$  is the permeability of the medium,  $\mu_d$  is its dynamic viscosity,  $Q_m$  is the  
 57 volumetric flow rate for a fluid source,  $\alpha$  is the Biot-Willis coefficient,  $\varepsilon_{vol}$  is the  
 58 volumetric strain of the porous matrix,  $\chi_f$  is the compressibility of the fluid,  $\chi_p$  is the  
 59 compressibility of the rock,  $\theta$  is the porosity, and  $q$  is the velocity variable which gives a  
 60 volume flow rate per unit area of porous material. The governing equations for the  
 61 poroelastic model are then given by:

$$62 \quad -\nabla \cdot \sigma = F_v \quad (4)$$

$$63 \quad \sigma_{ij} = \frac{2G\nu}{(1-2\nu)} \varepsilon_{kk} \delta_{ij} + 2G\varepsilon_{ij} - \alpha p \delta_{ij} \quad (5)$$

$$64 \quad \varepsilon_{ij} = \frac{1}{2} ((\nabla \mathbf{u})^T + \nabla \mathbf{u}) \quad (6)$$

65 where  $\sigma$  is the stress tensor,  $F_v$  is the volume force vector (i.e.,  $F_v = (\rho\theta + \rho_b)g$ , where  $g$   
 66 is the acceleration of gravity, and  $\rho_b$  is the bulk density),  $\delta_{ij}$  is the Kronecker delta (equal  
 67 to 1 when  $i = j$ , and to 0 when  $i \neq j$ ),  $G$  is Young's modulus,  $\nu$  is the Poisson's ratio, and  
 68  $\mathbf{u}$  is the displacement vector.

69 We build a 3D model of  $5 \text{ km} \times 10 \text{ km} \times 5 \text{ km}$  in the x, y and z directions,  
70 respectively, and split the model into four simplified layers (Table S1). From top to  
71 bottom, the four layers correspond to the upper sedimentary section, the Duvernay shale  
72 formation in which the HF horizontal wells are located, the lower sedimentary section,  
73 and the crystalline basement (*Bao and Eaton, 2016*). The solid and hydrogeological  
74 properties of each layer are listed in Table S1. Within the model, we set the so-called  
75 roller condition as the side solid boundaries, i.e., no vertical movement is permitted for  
76 the solid material on the boundary. We then set the bottom and top solid boundaries as  
77 fixed and free surfaces, respectively. Next, we set the fluid boundaries to have no flow. In  
78 addition, at the top, we add a standard atmospheric pressure, and set the pore pressure at  
79 the top surface to 0. Finally, we set the original fluid condition to be hydrostatic  
80 equilibrium.

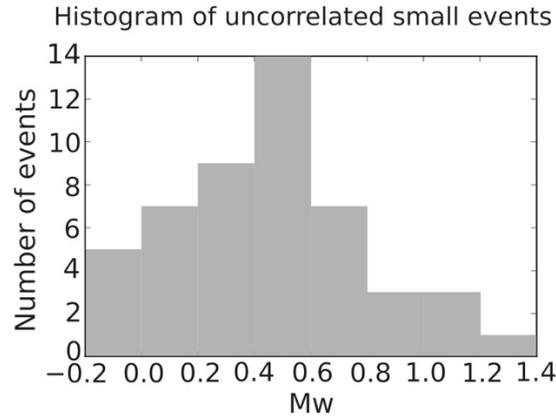
81 In our model, besides the stimulation points, we assume that the HF operations have  
82 created a fracture zone surrounding the horizontal wells (note that the fracture zone is  
83 confined in the Duvernay shale layer), leading to an increased permeability compared to  
84 the unfractured shale formation. The width of the fractures centered at the stimulation  
85 points is set to be 200 m. We assume the permeability of the fractures to be  $5 \times 10^{-15} \text{ m}^2$ ,  
86 the same as that of the fluid channel but three orders higher than the low-permeability  
87 unfractured shale formation ( $1 \times 10^{-18} \text{ m}^2$ , Table S1). As mentioned in the main text, there  
88 are two inferred fault systems, i.e., the east sequence fault and the west sequence fault. In  
89 the model, we create two near-vertical faults on the basis of the Mw 3.9 and Mw 3.2  
90 mainshock and their aftershock locations. We also assume that there is a near-horizontal  
91 basement fault connecting the two vertical fault systems (Figure 3). We set the  
92 permeability along the fault surface for the two vertical faults to be three orders of  
93 magnitude larger than the confining rock (Table S1), as the fault damage zone could  
94 enhance the permeability (*Yehya et al., 2018*). For the near-horizontal fault, it is worth  
95 noting that we have tested multiple permeability values, ranging from the same as the  
96 surrounding rock ( $1 \times 10^{-18} \text{ m}^2$ ) to five orders larger than the surrounding rock  
97 ( $1 \times 10^{-13} \text{ m}^2$ , Figure 4b). This range of permeability includes not only the scenario of a  
98 high-permeable horizontal fault, but also one where the horizontal fault does not exist.

99 To simulate the multi-stage fluid injection process, we assume that fluid is injected at  
100 a single point of each stage, and the consecutive stages migrate along the horizontal well  
101 bore. Each stage's fluid injection rate is the ratio between stage injection volume and  
102 duration time (calculated from Table S2). The outcomes (stress tensor and pore pressure  
103 change) from the poroelastic modeling are then used to calculate the  $\Delta CFS$  as discussed  
104 in the main text.

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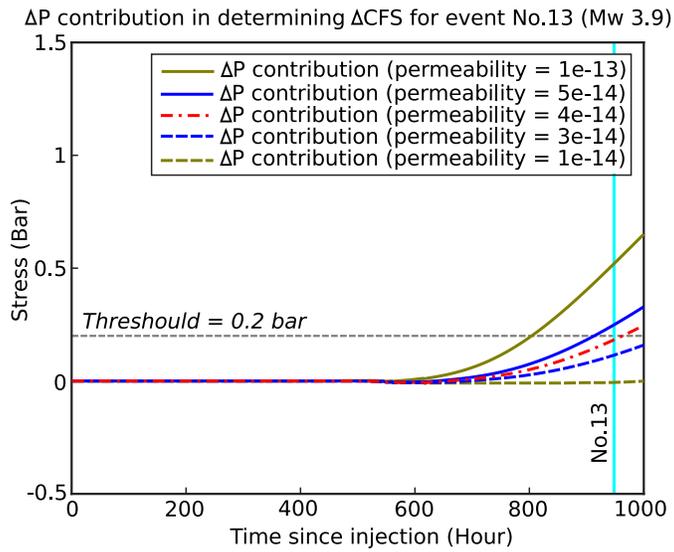
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**Figure S1.** Histogram of the 49 poorly correlated small earthquakes.

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**Figure S2.** ΔP contribution in determining the ΔCFS for the Mw 3.9 event.

116 **Table S1.** Solid and fluid properties of each layer used in the model. Note that for the  
 117 fracture zone, the permeability is  $5 \times 10^{-15} \text{ m}^2$  and the solid properties are the same as that  
 118 of the confining Duvernay shale layer. For the two vertical faults, their solid properties  
 119 are the same as the horizontal layers, and the permeability along the fault is  $5 \times 10^{-15} \text{ m}^2$ .  
 120

	Layer 1	Layer 2 (HF layer)	Layer 3	Layer 4
Depth	0-3.3 km	3.3 km-3.4 km	3.4 km-4.1 km	4.1 km-5 km
Biot-Willis	0.7	0.7	0.7	0.7
P-wave velocity	5000 m/s	6100 m/s	6300 m/s	6900 m/s
S-wave velocity	2800 m/s	3520 m/s	3630 m/s	3983 m/s
Bulk Density ( $\rho_b$ )	2500 kg/m <sup>3</sup>	2600 kg/m <sup>3</sup>	2750 kg/m <sup>3</sup>	2900 kg/m <sup>3</sup>
Permeability	$7.5 \times 10^{-16} \text{ m}^2$	$1 \times 10^{-18} \text{ m}^2$	$5 \times 10^{-18} \text{ m}^2$	$1 \times 10^{-18} \text{ m}^2$
Porosity ( $\theta$ )	0.1	0.05	0.05	0.08
Fluid density ( $\rho$ )	1000 kg/m <sup>3</sup>	1000 kg/m <sup>3</sup>	1000 kg/m <sup>3</sup>	1000 kg/m <sup>3</sup>
Fluid compressibility ( $\chi_f$ )	$4.5 \times 10^{-10} \text{ Pa}^{-1}$			
Fluid dynamic viscosity ( $\mu_d$ )	$0.79 \times 10^{-3} \text{ Pa*s}$			

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**Table S2.** Injection data.

Well	Stage	Stage-start	Stage-end	Total Fluid (m <sup>3</sup> )
1	1	17-12-2014--00:38	17-12-2014--04:02	1417
1	2	17-12-2014--18:08	17-12-2014--21:30	1288
1	3	18-12-2014--04:17	18-12-2014--07:10	1196
1	4	18-12-2014--13:53	18-12-2014--16:31	1196
1	5	18-12-2014--21:37	19-12-2014--00:11	1220
1	6	19-12-2014--04:50	19-12-2014--07:25	1217
1	7	19-12-2014--14:30	19-12-2014--18:47	1367
1	8	19-12-2014--23:44	20-12-2014--02:16	1123
1	9	20-12-2014--08:46	20-12-2014--11:01	1065
1	10	21-12-2014--00:33	21-12-2014--02:50	1101
1	11	21-12-2014--10:23	21-12-2014--13:36	1189
1	12	30-12-2014--03:43	30-12-2014--06:00	907.4
1	13	31-12-2014--11:45	31-12-2014--14:23	1199
1	14	31-12-2014--23:28	01-01-2015--02:26	1234
1	15	01-01-2015--11:35	01-01-2015--14:20	1266
1	16	01-01-2015--22:40	02-01-2015--01:34	1226
1	17	03-01-2015--22:43	04-01-2015--01:45	1333
1	18	04-01-2015--11:17	04-01-2015--13:56	1265
1	19	04-01-2015--21:24	05-01-2015--00:21	1268
1	20	05-01-2015--07:21	05-01-2015--10:26	1210.7
1	21	05-01-2015--18:17	05-01-2015--21:10	1174
1	22	06-01-2015--04:29	06-01-2015--06:55	1102
1	23	06-01-2015--17:30	06-01-2015--20:33	1301
1	24	07-01-2015--08:54	07-01-2015--11:05	987
1	25	09-01-2015--14:35	09-01-2015--17:26	1084
2	1	17-12-2014--06:52	17-12-2014--10:44	1253
2	2	20-12-2014--03:56	20-12-2014--07:00	1128
2	3	20-12-2014--13:06	20-12-2014--15:55	1219
2	4	21-12-2014--04:44	21-12-2014--07:21	1282
2	5	29-12-2014--17:52	30-12-2014--01:40	1294

2	6	30-12-2014--11:45	30-12-2014--14:36	1290
2	7	30-12-2014--20:26	30-12-2014--23:11	1305
2	8	31-12-2014--04:33	31-12-2014--07:20	1309
2	9	31-12-2014--17:58	31-12-2014--20:53	1192
2	10	01-01-2015--06:03	01-01-2015--08:49	1324
2	11	01-01-2015--16:46	01-01-2015--19:02	1087
2	12	02-01-2015--03:29	02-01-2015--06:18	1219
2	13	02-01-2015--10:36	02-01-2015--13:19	1278
2	14	03-01-2015--00:58	03-01-2015--20:28	1834
2	15	04-01-2015--06:01	04-01-2015--08:39	1267
2	16	04-01-2015--16:04	04-01-2015--18:42	1266
2	17	05-01-2015--02:36	05-01-2015--05:20	1218
2	18	05-01-2015--12:44	05-01-2015--15:17	1171
2	19	05-01-2015--23:03	06-01-2015--01:45	1212
2	20	06-01-2015--13:02	06-01-2015--15:22	1056
2	21	06-01-2015--21:58	07-01-2015--00:35	1101
2	22	07-01-2015--04:03	07-01-2015--06:49	1267
2	23	07-01-2015--21:09	07-01-2015--23:45	957
2	24	08-01-2015--03:35	08-01-2015--06:26	1144
2	25	08-01-2015--10:42	08-01-2015--13:04	1010