

1 **Fault Zone Imaging with Distributed Acoustic Sensing:**
2 **Body-to-Surface Wave Scattering**

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5 **Key Points:**

- 6 • We develop a framework for systematically locating fault zones at sub-kilometer
7 scales using the DAS-measured earthquake wavefield.
8 • We present a model for these fault zones and use simulations to show that this
9 model reproduces first-order observations of scattering.
10 • By comparing observations with synthetics, we use this method to constrain lo-
11 cal fault zone geometry.

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Abstract

Fault zone structures at many scales largely dictate earthquake ruptures and are controlled by the geologic setting and slip history. Characterizations of these structures at diverse scales inform better understandings of earthquake hazards and earthquake phenomenology. However, characterizing fault zones at sub-kilometer scales has historically been challenging, and these challenges are exacerbated in urban areas, where locating and characterizing faults is critical for hazard assessment. We present a new procedure for characterizing fault zones at sub-kilometer scales using distributed acoustic sensing (DAS). This technique involves the backprojection of the DAS-measured scattered wavefield generated by natural earthquakes. This framework provides a measure of the strength of scattering along a DAS array and thus constrains the positions and properties of local scatterers. The high spatial sampling of DAS arrays makes possible the resolution of these scatterers at the scale of tens of meters over distances of kilometers. We test this methodology using a DAS array in Ridgecrest, CA which recorded much of the 2019 $M_w 7.1$ Ridgecrest earthquake aftershock sequence. We show that peaks in scattering along the DAS array are spatially correlated with mapped faults in the region and that the strength of scattering is frequency-dependent. We present a model of these scatterers as shallow, low-velocity zones that is consistent with how we may expect faults to perturb the local velocity structure. We show that the fault zone geometry can be constrained by comparing our observations with synthetic tests.

Plain Language Summary

Fault zones are multi-scale structures that govern where and how earthquakes happen. Characterizing fault zones at all scales is thus important for understanding earthquake ruptures and earthquake-related hazards. However, finding and describing fault zones at small scales remains a persistent challenge in earthquake science. We propose a framework for the characterization of fault zones using distributed acoustic sensing (DAS), a recently developed technique that converts fiber optic cables into dense networks of ground motion sensors. Earthquake waves are scattered when they encounter fault zones, and this scattering creates signatures in DAS data that we can use to locate these fault zones. Additionally, the behavior of fault zone scattered waves with frequency may illuminate detailed characteristics of the fault zone. We test this framework using a DAS network in Ridgecrest, CA that recorded aftershocks of the 2019 magnitude 7.1 Ridgecrest earthquake. We use these recordings to map fault zone locations near the network. These locations are close to previously mapped faults but are more accurate. By comparing the behavior of observed fault zone scattered waves with frequency with that of simulations, we can constrain shallow fault zone geometry.

1 Introduction

The Earth's crust is a geologically heterogeneous medium that hosts myriad sharp material contrasts at multiple scales. Among these heterogeneities are fault zones, features consisting of fault cores and surrounding zones of fracture that accommodate strain. Finding new ways to locate and characterize fault zones may potentially serve a variety of societally and scientifically important functions. Proximity to fault zones increases the likelihood of severe damage to infrastructure, both because fault zones host static deformation, and because fault zones may amplify ground motion (Kurzon et al., 2014). Additionally, the locations of faults control estimates of fault connectivity, which is an important parameter in some probabilistic hazard estimates (Field et al., 2014). Relatedly, relative fault positioning and fault geometry play a pivotal role in the propagation and termination of earthquakes (Harris & Day, 1993, 1999; Wesnousky, 2008). Fault damage zone scaling is expected to play an influential role in earthquake nucleation (Ampuero et al., 2002), earthquake potency (Weng et al., 2016), and long-term earthquake sequence behavior (Thakur et al., 2020). Importantly, fault zones are multi-scale structures (Faulkner et al., 2010), and thus developing a more complete picture of fault zone structure at sub-kilometer scales contributes to these efforts to evaluate earthquake hazard and geological controls on earthquake phenomenology.

Considerable attention is given to major fault zones, those that are large and accommodate significant strain. But, minor and unmapped fault zones are an important consideration when evaluating the structural deformation and earthquake hazards in a region. Plate deformation is usually not accommodated by a single fault zone, but rather by a broad distribution of fault zones that extend sometimes hundreds of kilometers from the plate boundary, and minor fault zones play a key role in the accommodation of this strain (Scholtz, 2019). In the absence of high deformation rates, minor fault zones can develop a high risk potential if strain accumulates over a long time period, the stress state changes (Freed & Lin, 2001), or the stability of the fault is perturbed (Ellsworth, 2013). Relatedly, many significant earthquakes rupture within minor or unmapped fault zones. For example, the 2019 Ridgecrest earthquake sequence, which included the largest earthquake to take place in California in over two decades, ruptured mostly unmapped faults in the Little Lake and Airport Lake fault zones (Ross et al., 2019), which only accommodated approximately 1 mm/y of slip (Amos et al., 2013).

For both major and minor fault zones, shallow fault zone structure is important. The shallowest few hundred meters of fault zones can exhibit sharp and localized velocity reductions (e.g. Zigone et al., 2019; Y. Wang et al., 2019; Share et al., 2020) that can amplify ground motion, and shallow crustal faults play an important role in both facilitating and impeding the transport of groundwater and hydrocarbons (Bense et al., 2013). Shallow fault zone structure may also be used to infer the contribution of deep fault structure, which is very difficult to constrain, by correcting for shallow structure contributions in depth-integrated fault characterization approaches.

Previous efforts to locate and describe shallow fault zone structures at sub-kilometer scales have typically relied on geologic mapping, seismic surveying, and satellite imagery. Geologic mapping over decades has produced excellent records of Quaternary faults (e.g. USGS & CGS, 2022), but discerning faults using geologic mapping requires careful fieldwork and evidence of faulting at the surface. Seismic surveying produces detailed images of the subsurface, with which fault locations can be inferred (e.g. Liberty et al., 2021; Lay et al., 2021), but surveys are often expensive and logistically challenging, particularly in urban settings. Satellite imagery is also used to map faults, often by identifying topographic anomalies in images (Joyce et al., 2009). More involved processing, such as producing phase gradient maps from InSAR interferograms (Xu et al., 2020), can also be used to identify fractures. These techniques are powerful, but they require surficial evidence of strain that can be imaged from above.

100 Other studies have used the earthquake wavefield to characterize the structure of
 101 major fault zones. For example, some studies have used fault zone head waves, head waves
 102 generated by refraction due to a bimaterial contrast across the fault, to image the fault
 103 interface and constrain the velocity contrast across the fault (e.g. McGuire & Ben-Zion,
 104 2005; Allam et al., 2014; Share & Ben-Zion, 2018; Qin et al., 2020). Additionally, some
 105 studies have used travel-time anomalies from regional and teleseismic events to discern
 106 properties like the width of the damage zone and the velocity reduction within the dam-
 107 age zone (e.g. Cochran et al., 2009; H. Yang et al., 2020; Qiu et al., 2021; Share et al.,
 108 2022). Moreover, low velocity structures can amplify ground motion, and some studies
 109 have used S-wave amplification caused by the reduced velocities in fault damage zones
 110 to delineate their structure (e.g. Qiu et al., 2021; Song & Yang, 2022). Another approach
 111 is to use fault zone trapped waves, waves generated by constructive interference of crit-
 112 ically reflected waves in the fault damage zone, which can be initiated by sources out-
 113 side the fault zone (Fohrmann et al., 2004) and have been used to constrain the struc-
 114 ture of fault damage zones (e.g. Ben-Zion et al., 2003; Catchings et al., 2016; Y. Wang
 115 et al., 2019; Qiu et al., 2021). In general, these techniques are highly effective tools for
 116 capturing geometric and internal properties of major fault zones. But, fault zones usu-
 117 ally need to exhibit relatively large and spatially consistent elastic material contrasts for
 118 these techniques to be used. Hence, these techniques are typically applied to major fault
 119 zones using targeted deployments of dense networks of sensors. These factors make these
 120 methods ineffectual for the discovery and characterization of minor fault zones.

121 The weaknesses of these methods motivate the development of complimentary tech-
 122 niques for identifying and characterizing sub-kilometer scale fractures in the crust. To
 123 this end, we suggest an alternative method for identifying and characterizing fractures
 124 in the crust using distributed acoustic sensing (DAS) data. DAS is an emergent tech-
 125 nology that repurposes fiber optic cables as dense arrays of strainmeters. DAS uses a laser
 126 interrogator unit to emit pulses of light that probe a fiber optic cable, and natural im-
 127 perfections in the fiber send echoes back to the interrogator unit. Perturbations of the
 128 fiber change the travel times of these echoes, and these changes in travel time are quasi-
 129 linearly proportional to the strain induced by the perturbations. The high spatial fre-
 130 quency of DAS data allows for the resolution of high wavenumber phenomena that are
 131 incoherent in more sparsely measured data, which is useful for characterizing fault zones
 132 at high resolution (Jousset, 2019). One such phenomenon is the scattering of earthquake
 133 body waves to surface waves due to small-scale, local heterogeneities in the upper crust.
 134 We show an example of this scattering in Figure 1, and we subsequently refer to these
 135 features as chevrons, owing to their chevron-like shape in DAS data representations. These
 136 chevrons have been observed in other DAS datasets, and the scatterers generating these
 137 chevrons have been inferred to be faults (Lindsey et al., 2019; Spica et al., 2020). More-
 138 over, these scattered surface waves are also visible in empirical Green’s functions derived
 139 in DAS datasets that can be migrated to infer scatterer locations (Cheng et al., 2021;
 140 Y. Yang, Zhan, et al., 2022).

141 Our contributions in this paper are as follows. We suggest a local backprojection
 142 framework for the systematic location of the sources of these chevron-like features and
 143 find a strong spatial correlation between these locations and mapped faults. We suggest
 144 a model of these scatterers as rectangular perturbations in the velocity field, approxi-
 145 mating a fault zone, and show that this model reproduces first-order features observed
 146 in the data. We then show that we can constrain key geometric features of the fault zone
 147 under this backprojection framework.

148 2 Data

149 In early July 2019, a large earthquake sequence initiated in the Eastern Califor-
 150 nia Shear Zone. This sequence, which included a M_w 6.4 foreshock and a M_w 7.1 main-
 151 shock, produced thousands of aftershocks over the course of a few months. Shortly fol-

152 lowing the mainshock, a DAS array was deployed in Ridgecrest, CA using an Optasense
 153 ODH3 interrogator unit in an effort to record this aftershock sequence (Li et al., 2021).
 154 This DAS array began recording on July 10, 2019, and in this study we use recorded af-
 155 tershocks that took place between the initiation of recording and October 4, 2019. The
 156 array is temporally sampled at 250 Hz and is spatially sampled at 8 m intervals over 1250
 157 channels, with a total cable length of 10 km. The deployment of this DAS array ensured
 158 that numerous Ridgecrest sequence aftershocks were recorded nearby at a high spatial
 159 frequency.

160 For this study, we choose a subset of well-recorded, low-noise earthquakes on which
 161 we perform our subsequent analysis. We choose these earthquakes using straightforward
 162 quality control metrics to ensure that scattered surface waves have a high enough signal-
 163 to-noise ratio to be reliably analyzed and that the scattered surface waves are isolated
 164 from any cultural noise that may bias the analysis. As part of this quality control, we
 165 select from only events with $M_l \geq 2$ or $M_w \geq 2$ as determined by the Southern Cali-
 166 fornia Seismic Network catalog. We also restricted our selection to only events that oc-
 167 curred between 11 pm and 4 am local time, thus only keeping events with a low prob-
 168 ability of being partially masked by cultural noise. We then manually inspected all of
 169 the remaining events and ensured that we only kept events with negligible cultural noise.
 170 After performing this processing, we are left with 50 events that meet our quality con-
 171 trol criteria. These events are plotted in geographic context in Figure 1. These events
 172 are reasonably well clustered by distance and azimuth, minimizing variability due to the
 173 directional sensitivity of DAS.

174 3 Mapping faults using local backprojection

175 To quantify the magnitudes and locations of these scatterers, we employ a simple
 176 local backprojection technique to identify the locus points of the scattered waves in the
 177 body wave coda. This backprojection is based on the reasonable assumption that these
 178 chevron-like waves are surface waves generated by earthquake body waves impinging on
 179 a scatterer near the DAS array. We expect this phenomenon to be body-to-surface wave
 180 scattering because the scattered waves are dispersive, which we verify subsequently, and
 181 the onset of these waves occurs early in the body wave coda. We expect these scatter-
 182 ers to be local because the scattered waves attenuate rapidly in space, as exemplified by
 183 the narrow width of these chevrons shown in Figure 1. A schematic example of the gener-
 184 ation of these scattered waves is shown in Figure 2. The driving principle of this method-
 185 ology is the same for standard backprojection techniques used in seismology (Kiser &
 186 Ishii, 2017). In particular, for grid points near or above a scatterer, the backscattered
 187 energy resultant from the scatterer will align and sum coherently, producing a larger am-
 188 plitude than that of a grid point far from any scatterers. In this case, we attempt to back-
 189 project locally scattered surface waves to image the scattering source, illustrated as a
 190 fault zone in Figure 2.

191 To accomplish this backprojection, we first bandpass our data to a narrow frequency
 192 band; this frequency band can vary depending on the desired dimensional sensitivity. We
 193 select frequency bands with 1 Hz widths and center frequencies spanning 2-10 Hz at 0.5
 194 Hz intervals. For each of these frequency bands, we partition the earthquake wavefield
 195 by velocity in the curvelet domain (Atterholt et al., 2021), using a curvelet basis to mute
 196 sections of the frequency-wavenumber domain and thus isolate desired wavefield com-
 197 ponents. This is equivalent to frequency-wavenumber filtering with specialized tapers that
 198 minimized velocity filtering artifacts. We use this wavefield-partitioning technique to se-
 199 parate the scattered wavefield and the direct waves into two separate windows. We clas-
 200 sify velocities below 750 m/s to be the scattered wavefield and velocities above 1000 m/s
 201 to be the direct wavefield. Of the scattered wavefield, we select only the scattered waves
 202 from the early-onset body waves, because these early-onset scattered waves are typically
 203 more pronounced relative to the earthquake wavefield and are not convolved with earthquake-

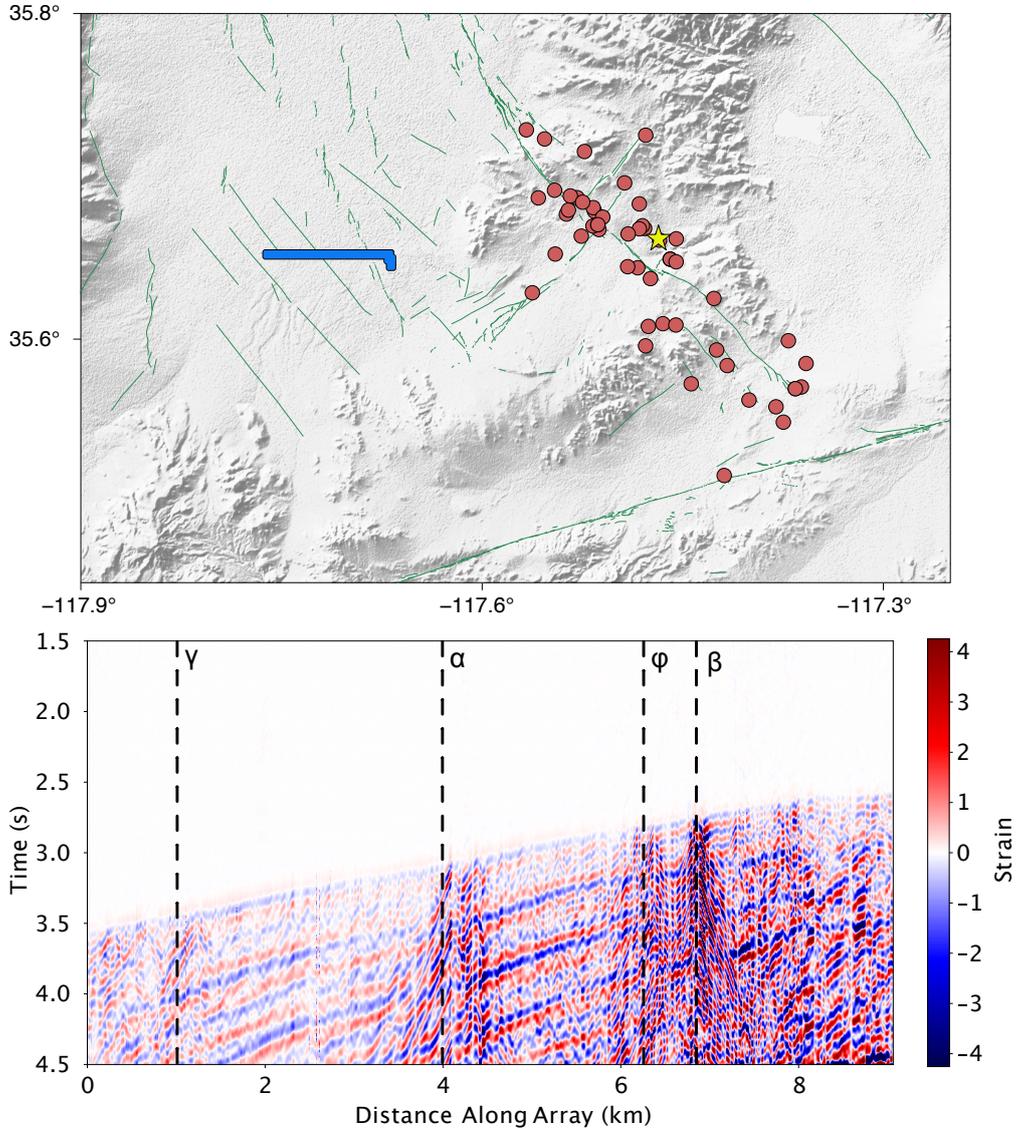


Figure 1. Top: The geographic setting of the data used in this study. Blue line corresponds to the DAS array. Red dots correspond to the epicenters of the events used in this study. Yellow star corresponds to the epicenter of the event shown below (depth 5.6 km). Green lines correspond to the USGS-mapped Quaternary faults in the area. Bottom: Example of the DAS-measured wavefield of the onset of an event used in this study. Black dotted lines correspond to the locations of the chevron-like features that are mapped in Figure 3.

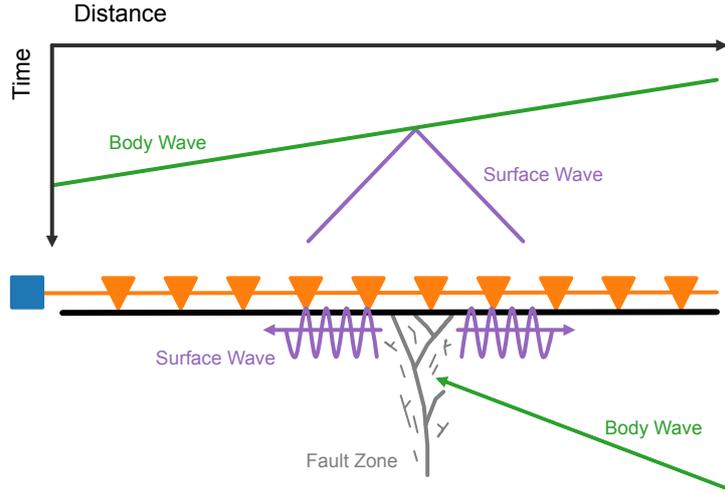


Figure 2. Schematic illustration of the phenomena observed in the earthquake wavefields used in this study. Top: Record section corresponding to the processes illustrated below. Bottom: Illustration of the phenomena resulting in the generation of the chevron-like features shown in Figure 1. Colors represent the same phenomena in both top and bottom. Green corresponds to incident body wave. Gray features indicate a fault zone. Purple corresponds to the scattered surface waves resulting from the body waves impinging on the fault zone. Orange line and triangles indicate the fiber optic cable and stations, respectively. Blue box represents the DAS interrogator unit.

204 generated surface waves, which can bias the final result. To isolate the early-onset scattered
 205 waves, we window the scattered wavefield over the time interval between 2 seconds
 206 prior to the onset of the P-wave and 5 seconds after the onset of the P-wave. Once we
 207 have isolated the scattered waves, we perform a local backprojection of surface wave energy
 208 according to a local velocity model across the array. For the local velocity model,
 209 we use a 1-dimensional velocity model made by taking averages of each period of the velocity
 210 model developed by Y. Yang, Atterholt, et al. (2022). We perform this averaging
 211 to avoid biasing of the result due to lateral slopes in the model. We then define a grid
 212 of potential scattering sources along the array geometry, and we backproject the surface
 213 waves recorded by the surrounding channels, up to a fixed distance, according to their
 214 distance from the potential source. Our grid of potential source locations is spaced at
 215 8 m along the array, which coincides with the station spacing. In this study, by inspecting
 216 the data, we fix the maximum distance to be 250 m based on the expected distance
 217 from the chevron center over which we can expect to get significant constructive interference
 218 by aligning the waveforms. We then stack the backprojected channels and sum
 219 the absolute value of the stack, giving us an amplitude for the grid point. We only define
 220 the grid at the surface along the array, because linear DAS array geometry poorly
 221 constrains backprojection images along orthogonal axes. But, the rapid attenuation of
 222 these surface waves suggests that most of the energy in the scattered wavefield is generated
 223 very close to the array, minimizing the consequence of this poor constraint. Furthermore,
 224 scattered waves from more distant scatterers will have higher apparent velocities, minimizing
 225 the impact of these scatterers in a backprojection framework that uses true velocity.
 226

227 We can verify that these scattered waves are dispersive under this framework. That
 228 is, we apply this backprojection framework to the earthquake wavefield shown in Fig-

229 ure 1 over a range of velocities for each frequency, rather than using a single velocity model.
 230 We can then sum across each resultant profile to get a single value for each frequency
 231 and velocity pair. From this we can determine which velocities produce the largest sum
 232 at each frequency, which we expect to be correlated with the amount of constructive in-
 233 terference due to waveform alignment. In this way we can construct a dispersion curve
 234 using only the scattered wavefield. This is a similar approach to that taken by Spica et
 235 al. (2022), but because we sum across the entire profile, this produces a velocity spec-
 236 trum that averages the contributions of the scattered waves produced across the array.
 237 A plot of this velocity spectrum is shown in Figure S1. This spectrum shows a clear dis-
 238 persion pattern that is well matched by the dispersive relationship for this setting com-
 239 puted in Y. Yang, Atterholt, et al. (2022).

240 Since DAS measures longitudinal strain, which is distinct from conventional inertial
 241 seismometers, the sensitivity of DAS to these scattered waves is also distinct. For
 242 surface waves generated by scattering from a fault that runs orthogonal to the array, the
 243 recorded surface waves will propagate parallel to the fiber. Consequently, a significant
 244 component of the particle motion will be parallel to the fiber, motion to which DAS is
 245 most sensitive. For a fault that runs oblique to the array, the surface waves will not prop-
 246 agate exactly parallel to the fiber, and the apparent velocity will increase and the sen-
 247 sitivity of the DAS array to the waves will decrease. However, since these waves atten-
 248 uate rapidly in space, the majority of the recorded energy will have been scattered very
 249 close to the array, minimizing variability due to obliquity. Additionally, because DAS
 250 is more sensitive to lower velocities, surface waves are amplified in DAS data relative to
 251 the other components of the earthquake wavefield. This potentially explains why these
 252 surface waves are such a common and well-recorded observation in DAS data (e.g. Lind-
 253 sey et al., 2019; Spica et al., 2020; Ajo-Franklin et al., 2022). These factors suggest that
 254 the variability in scattered waves measured across the DAS array is largely due to vari-
 255 ability in the strength and geometry of the scatterers near the array. Additionally, be-
 256 cause we’re using array seismology, we need to consider apparent velocity when perform-
 257 ing velocity filtering and backprojecting these waves. But, since the recorded surface waves
 258 propagate approximately parallel to the fiber, the apparent velocity of locally scattered
 259 surfaces waves is very close to the true velocity. In particular, the apparent velocity fol-
 260 lows $v_t/\cos(\theta)$; where v_t is the true velocity and θ is the incident angle relative to the
 261 array geometry. In the case of surface waves scattered very close to the array, θ is close
 262 to zero.

263 We apply this backprojection technique to the 50 high quality events recorded by
 264 the DAS array in Ridgecrest, CA described in the preceding section. Backprojecting the
 265 scattered wavefields of these earthquakes results in an ensemble of profiles of scattering
 266 across the Ridgecrest DAS array. To ensure that the within-array and between-event am-
 267 plitudes are comparable, we normalize the profile amplitudes by the sum of the abso-
 268 lute value of the body waves that occupy the same window used for each grid point in
 269 each profile. For this normalization, we account for the variability in azimuth and in-
 270 cident angle according to the directional sensitivity of strainmeters (Benioff, 1935). In
 271 particular, noting that the dominant body wave signal we use for this normalization is
 272 the P-wave, we divide the direct wavefield by $\cos^2(\theta)$. We smooth these profiles with a
 273 Gaussian kernel with a standard deviation of 5 channels to minimize any high-frequency,
 274 stochastic variability in these profiles. We show these ensembles of backprojection pro-
 275 files computed at 4 and 7 Hz center frequencies in Figure 3. These profiles are generally
 276 ”bumpy,” and it can be difficult to determine to which of these peaks to assign signif-
 277 icance. Additionally, some peaks are of low amplitude, but are noteworthy because they
 278 are positioned in areas with low noise floors. To help us determine which peaks are most
 279 likely associated with scatterers, we use the metric from mountaineering of topographic
 280 prominence, which is a measure of the height of a peak relative to its surroundings. We
 281 plot the prominence profiles alongside the backprojection amplitude profiles in Figure
 282 3. Additionally, we superimpose these prominence profiles on the DAS array geometry

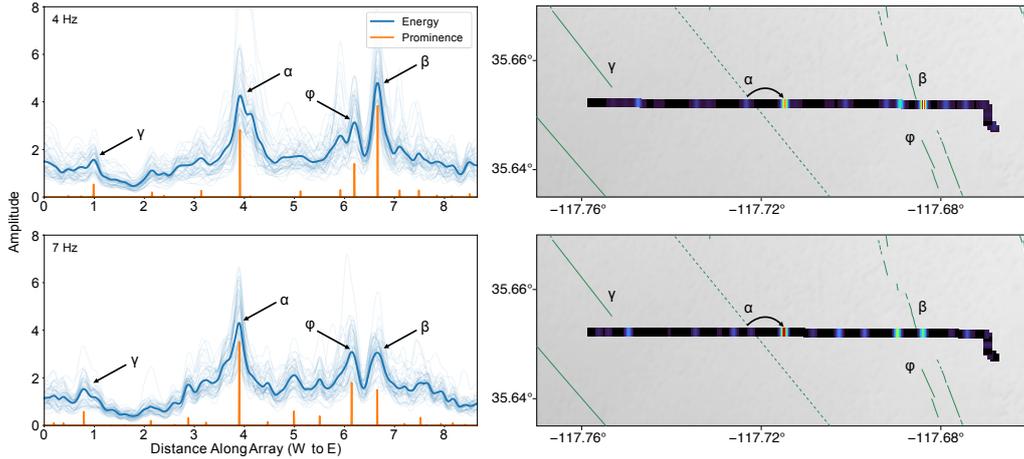


Figure 3. Left: Backprojection profiles made using 50 events recorded by the DAS array in Ridgecrest, CA. Light blue lines correspond to profiles made using a single event. Dark blue lines correspond to the mean profile. Orange lines correspond to the topographic prominence of the mean energy profile. Top and bottom plots correspond to profiles generated with 4 and 7 Hz center frequencies, respectively. Black arrows point to referenced peaks α , β , γ , and ϕ . Right: Prominence profiles to the left, convolved with Gaussian kernel to widen peaks for representation, plotted on the DAS array geometry shown in Figure 1. Color corresponds to prominence amplitude. Green lines correspond to fault locations. Solid lines are moderately or well constrained fault locations, and dotted lines are inferred fault locations. Faults are labeled according to associated peaks indicated in the profiles to the left. Curved black arrows indicate the proposed relocation of the fault associated with peak α .

283 in Figure 3. Indeed, there is a spatial correlation between peaks in the prominence pro-
 284 file and the locations of USGS-mapped Quaternary faults near the array. This spatial
 285 correlation partially evidences the argument that the nearly ubiquitous chevron-like fea-
 286 tures in the DAS measured wavefield are fault-zone scattered waves. In Figure 3, we make
 287 note of four peaks, which we term peaks α , β , γ , and ϕ . These are the most prominent
 288 peaks in both frequency bands, and by visual inspection we can associate these peaks
 289 with mapped faults nearby. In particular, peaks α and β are noteworthy in that they
 290 are prominent enough that we can analyze their behavior with space and frequency. We
 291 use peaks α and β to infer properties of the associated fault zones subsequently.

292 4 Modeling scatterers as fault zones

293 To further investigate the nature of the sources of scattering evident in DAS data,
 294 we present a model for these scatterers as rectangular perturbations in the 2D velocity
 295 structure. Although natural faults are neither perfect rectangles nor uniform velocity per-
 296 turbations, this simple parameterization allows us to capture first order structural prop-
 297 erties of fault zones without including more complexity than we can feasibly resolve given
 298 our data. The few free parameters of this fault model are burial depth, maximum depth,
 299 width, and percent change in velocity. For a background velocity model, we use a com-
 300 bination of the aforementioned shear wave velocity model from Y. Yang, Atterholt, et
 301 al. (2022) for the shallowest 150 m and a local 1D velocity profile taken from the SCEC
 302 Unified Community Velocity Model (Small et al., 2017) for depths deeper than 150 m;
 303 we combine these two models using a linear interpolation. We then create a model fault

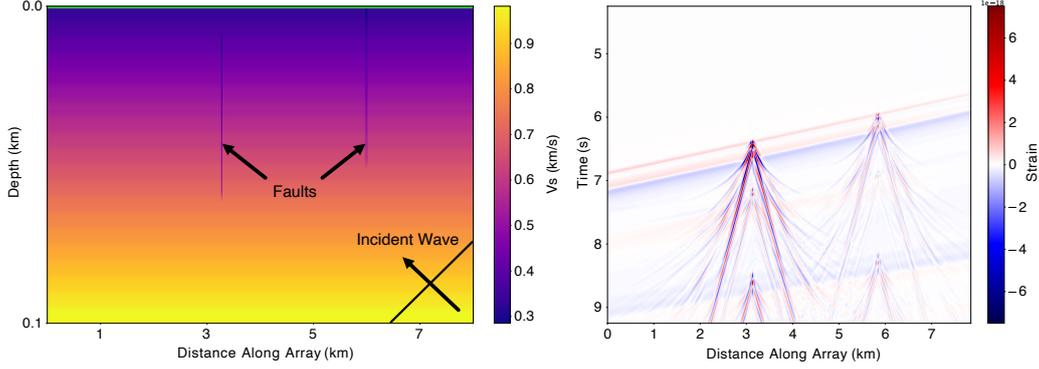


Figure 4. Left: Example of velocity model modified from (Y. Yang, Atterholt, et al., 2022) and (Small et al., 2017) with two fault zone-approximating velocity perturbations emplaced in the model. Green line corresponds to array of strainmeters. Black arrows point to incident wave direction and fault locations. Note the large vertical exaggeration. Right: Record section generated from scenario illustrated to the left.

304 zone by multiplying a section of the background model with an assigned rectangular ge-
 305 ometry by a constant of proportionality.

306 We then use this model to perform synthetic tests that we can compare to our ob-
 307 servations to assess the feasibility of this scatterer model. We generate these synthet-
 308 ics using Salvus (Afanasiev et al., 2019), a full waveform modeling software that simu-
 309 lates wave propagation using the spectral element method. We approximate the DAS
 310 array at Ridgecrest as a linear, 8 km array of strainmeters at the surface of our Earth
 311 model. We emplace a 2D double couple source with a 0.1 s half-duration Gaussian rate
 312 source time function 30 km east of the array at 10 km depth, a representative distance
 313 and depth for the earthquakes used in this study. We generate an adaptive mesh with
 314 which we can compute these synthetics up to 10.5 Hz with at least one element per wave-
 315 length. We use the same setup to perform tests of the fault geometry that we describe
 316 subsequently. We show an example of a simulation for a model with two faults with dif-
 317 ferent geometries and velocity reductions in Figure 4. The faults in Figure 4 were pa-
 318 rameterized using models for the faults associated with scatterers α and β that are pro-
 319 posed in the subsequent section. In particular, the fault on the left is parameterized as
 320 a 30% velocity reduction with a width of 20 m and a depth extent of 10 to 60 m. The
 321 fault on the right is parameterized as a 10% velocity reduction with a width of 50 m and
 322 a depth extent of 0 to 50 m. Both fault parameterizations are vertical. The resultant scat-
 323 tered waves in the synthetic wavefield match many of the first-order characteristics of
 324 the scattered waves in the observations of Figure 1. In particular, we have reproduced
 325 the observation of low-velocity scattered surface waves emanating from a narrow source.
 326 We can evaluate the similarities in the velocity content of the synthetic data and the ob-
 327 served data by computing the velocity spectrum of the scatterer component of the syn-
 328 thetic wavefield, as outlined in the preceding section. We show the velocity spectrum in
 329 Figure S2. The dispersion of the scattered wavefield in the synthetic test is a close match
 330 to the dispersion for the real data in Figure S1. These simulations thus further confirm
 331 that these scatterers may be related to faults. As is clear in Figure 4, variations in the
 332 properties of the model fault zones create visually apparent differences in the strength
 333 of the scattered wavefield.

5 Constraining fault geometry

Now that we have a method of quantifying the degree of scattering in data and a means of simulating our observations using a reasonable model, we can constrain the properties of the sources of scattered waves by comparing features between the data and synthetics under this backprojection framework. As is evident in Figure 3, the peaks in these backprojection profiles have variant properties in space and frequency, and this variability may inform a better understanding of the faults that generate these peaks. Moreover, since we performed this backprojection for many events, we have an ensemble of profiles with which we can evaluate how well constrained the fault-zone properties that control these peak shapes are.

To generate our synthetics, we use the velocity model and source described in the preceding section. We also incorporate attenuation into our model. Since we do not have a priori estimates of the attenuation at this site, we parameterize the attenuation using the functional decay of the peaks from our backprojection profiles to obtain a rough estimate of the local attenuation structure. We assume an empirical relationship between shear wave velocity and attenuation structure, a common assumption when building an Earth model with heterogeneous attenuation structure (Graves & Pitarka, 2010), and may be denoted as $Q_\mu = cV_s$. To test the attenuation of surface waves away from a local scatterer, we define a fault zone according to the aforementioned simplified fault model with a width of 20 m, a depth extent of 0-100 m, and a 30% velocity reduction. We test several values for c and compare the spatial decay of the resultant synthetic peaks to those of peaks α and β at 4 Hz. We find that the data are best fit by a value of $c = 50$, a reasonable value for this relationship (Lin & Jordan, 2018; Lai et al., 2020). These peak comparisons are shown in Figure S3. This empirical relationship between attenuation and velocity is imperfect, as other parameters such as temperature and fluid content also control attenuation (Brocher, 2008; Eberhart-Phillips et al., 2014), and other factors such as structural heterogeneity can control surface wave amplitude (Bowden & Tsai, 2017). But, since we are only trying to obtain a reasonable attenuation parameterization for our forward model, this approximation is sufficient for our purposes.

To constrain the local fault zone properties, we note that the backprojection profiles shown in Figure 3 are functions of the frequency band in which we filter the data, and that each peak behaves differently with frequency. We investigate this property by evaluating the backprojection profiles for all narrow frequency bands for which we computed profiles in this study, with center frequencies ranging from 2 to 10 Hz. By plotting the mean profiles at each center frequency together, we can better inform our understanding of the behavior of the frequency dependence of individual scattering features along the array. We plot these mean profiles against center frequency and distance as a pseudocolor plot in Figure 5. As is evident in Figure 5, there are peaks that are traceable across a range of center frequencies, and there is a high degree of variability in the behavior of these peaks with frequency.

We then focus on the two most prominent peaks in this image, peak α and peak β , both of which are spatially correlated with USGS-mapped faults (USGS & CGS, 2022). By taking cross sections of the center frequency versus distance along array plot, we can determine the frequency dependence of these specific scatterers along this profile. Clearly, these peaks have different frequency dependences, which likely reflects a variability in the depth and geometry of the scattering fault zone. To discern the properties of these faults, we test different fault zone geometries to match these frequency dependent trends. Because the amplitudes of DAS data are not well understood, we only attempt to match the shape of the synthetic profile with the shapes of the peak profiles, and we thus normalize the synthetic profile amplitude by the ratio of the integrated amplitude of the mean peak profile to the integrated amplitude of the synthetic peak profile. We attempted to reproduce these frequency-amplitude trends by performing synthetic simulations that included fault zones with varying free parameters. These simulations were too expen-

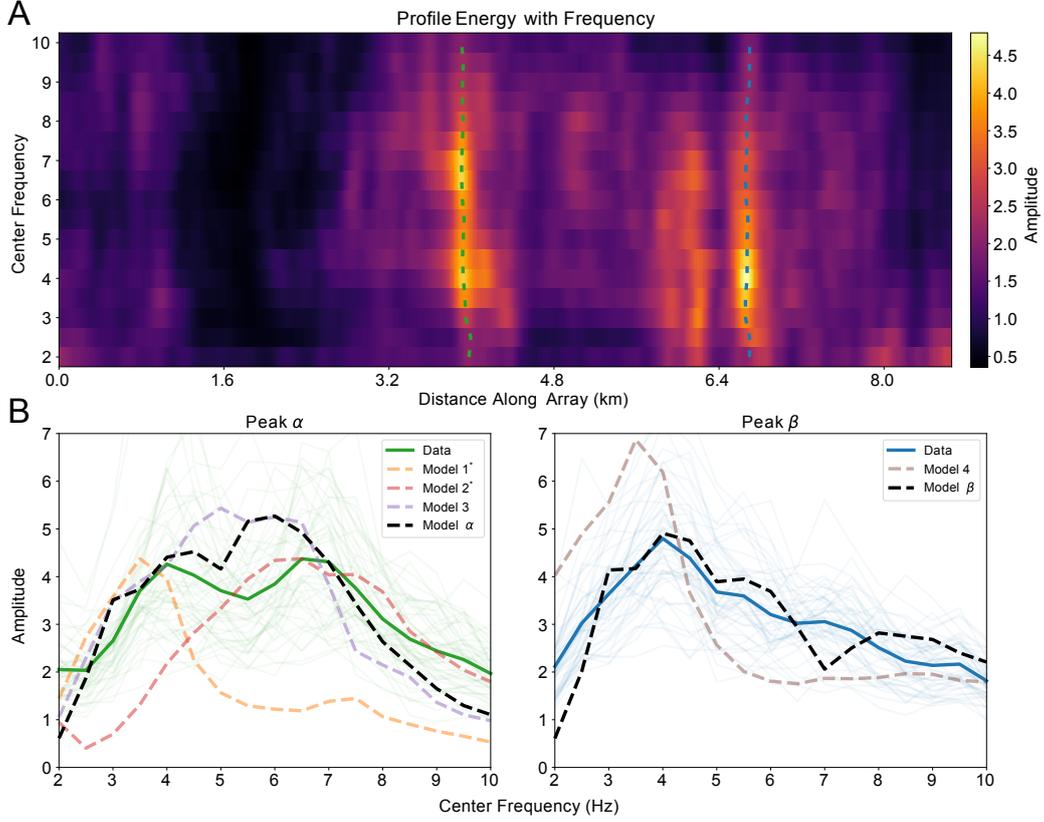


Figure 5. A. Pseudocolor plot of mean backprojection amplitude plotted against center frequency and distance along array. Dotted green and dotted blue lines correspond to cross sections of this plot, associated with peaks α and β , respectively. B. Plots of backprojection amplitude versus center frequency for the cross-sections shown in A. Light green and light blue lines are the frequency-amplitude curves determined for a single event for peaks α and β , respectively. Dark green and dark blue lines are the mean frequency amplitude curves for peaks α and β , respectively. Dotted black lines correspond to the frequency-amplitude curves for our preferred fault zone model for each peak. Dotted colored lines are frequency amplitude curves for fault zone models with variant parameters to illustrate the constraints of this methodology. The parameters used for each model are given in Table S1. The asterisk in the legend indicates that, for visualization purposes, the corresponding model is normalized by the maximum height of the data curve rather than the integrated sum.

387 sive to perform a full grid search over all the fault model parameters, but by identify-
 388 ing patterns between fault zone parameterizations and subsequent simulated frequency-
 389 amplitude profiles, we were able to find fault zone models that produced good fits to the
 390 profile ensembles for both faults, as shown in Figure 5B. Indeed, reproducing the frequency-
 391 amplitude curves for the different peaks requires the use of variant fault zone parame-
 392 terizations. Peak α is best fit by a 30% velocity reduction that is 20 m wide and spans
 393 10 to 60 m depths. Peak β is best fit by a 10% velocity reduction that is 50 m wide and
 394 spans 0 to 50 m depths. The results for peak α suggest that we may be able to detect
 395 and constrain properties of small-scale buried faults.

396 6 Discussion

397 The spatial correlation between the locations of sources of scattering and the mapped
 398 faults near the Ridgecrest DAS array shown in Figure 3 suggests that the source of at
 399 least some of these scatterers are faults, and thus DAS arrays can detect measurable sig-
 400 natures of fault zones. An example of the potential utility of this technique is readily avail-
 401 able in this dataset. In particular, peak α is located near, but is offset from, a mapped
 402 fault extending across the array. The Quaternary Fault Catalog (USGS & CGS, 2022)
 403 records this fault’s location as inferred rather than directly observed; thus, we can use
 404 our backprojection profile to refine the location of this fault, treating peak α as a po-
 405 tential node of the fault trace. This node provides a stronger constraint on this fault’s
 406 location near the town of Ridgecrest, CA, which has important implications for the lo-
 407 cation of possible static strain in the event of the activation of the Little Lake Fault Zone.
 408 This technique is generalizable to all DAS arrays that record seismicity, and may then
 409 be used elsewhere to systematically refine inferred fault locations and suggest the pres-
 410 ence and locations of previously unmapped faults.

411 The profiles in Figure 3 bear a resemblance to results from distinct fault zone char-
 412 acterization methodologies, namely S-wave amplification analysis (e.g. Qiu et al., 2021).
 413 Both techniques can be used to locate faults at small spatial scales using the peak lo-
 414 cations, but these techniques otherwise provide complimentary information. For exam-
 415 ple, the shape of the peaks in S-wave amplification profiles can be interpreted as an es-
 416 timate of the lateral characteristics of the fault damage zone, while the shape of the peaks
 417 in this study are largely reflective of the processing workflow and amplitude attenuation.
 418 But, the methodology presented in this study is more sensitive to small variations in the
 419 frequency of scattered waves that are reflective of characteristic dimensions of the fault
 420 zone, which includes constraints on the depth-dependence of the fault zone. Addition-
 421 ally, the methodology presented in this study is more readily applicable to DAS, both
 422 because DAS amplitudes are not well understood due to variability in coupling of the
 423 fiber and because DAS is particularly sensitive to low velocity surface waves.

424 The synthetic simulations in this study provide additional evidence that these chevron-
 425 like observations in DAS data are well-explained by fault zones. In particular, as shown
 426 in Figure 4, an approximation of a fault zone as a rectangular perturbation in velocity
 427 reproduces the first order features of these chevron-like observations. Additionally, the
 428 complexity in the frequency-amplitude curves shown in Figure 5 evidences a necessary
 429 variability in the finite properties of the scattering fault zones (Almuhaidib & Toksöz,
 430 2014). But, importantly, this representation is non-unique, and the diversity of geologic
 431 heterogeneity in the upper crust suggests that features other than fault zones are likely
 432 responsible for at least some of the chevron-like observations we see in DAS data.

433 The geometric constraints we place on the faults in this study illustrate that, us-
 434 ing DAS recorded earthquakes, we can constrain some aspects of the subsurface geom-
 435 etry of fault zones on the scale of tens of meters, potentially even for buried faults as is
 436 the case for peak α . Although these solutions are non-unique, they provide robust con-
 437 straints on the approximate scaling of these subsurface structures. As stated prior, we

438 were able to approach fault models that fit these data by identifying patterns in the re-
 439 lationship between fault zone geometry and the resultant synthetics. One interesting re-
 440 lationship, made clear in Figure 5, is related to the observation that peak β has a uni-
 441 modal frequency-amplitude curve while peak α has a bimodal frequency-amplitude curve.
 442 The simulations suggest that two characteristic lengths produce distinct modes in these
 443 frequency-amplitude curves: the fault zone width and the fault zone depth extent. In
 444 particular, we obtain a unimodal frequency-amplitude curve when these lengths are the
 445 same (as with peak β) and a bimodal frequency-amplitude curve when these lengths are
 446 distinct (as with peak α), with the smaller characteristic dimension responsible for the
 447 highest frequency mode and vice versa. We demonstrate that variant characteristic di-
 448 mensions can account for each frequency mode of peak α by running separate simula-
 449 tions for square-shaped buried faults, with velocity perturbations equivalent to the best
 450 fitting model for peak α , that extend up to 10 m depth with side lengths of 50 m and
 451 20 m, lengths which match the depth extent and width, respectively of the best fitting
 452 model for peak α . The amplitude-frequency curves of these simulations are plotted as
 453 Models 1 and 2 in Figure 5, respectively. Both of these models well approximate one of
 454 the individual modes of the bimodal data curve for peak α . Finally, although we nor-
 455 malize by amplitude, the magnitude of the velocity perturbation subtly changes the shape
 456 of the synthetic curves in our simulations in Figure 5; however, this is a weakly constrained
 457 parameter in this methodology.

458 Although this is not the first study to attempt to map fault zones using scattered
 459 waves in DAS data, a key contribution of this study is that it provides a framework to
 460 systematically locate the origins and discern the dimensions of these scatterers using the
 461 earthquake wavefield. Importantly, when using the earthquake wavefield, we are mostly
 462 looking at body-to-surface scattered waves, which have a different depth sensitivity than
 463 surface-to-surface scattered waves. In particular, body-to-surface wave scattering has a
 464 deeper depth sensitivity than surface-to-surface wave scattering because body waves can
 465 propagate at depth while surface waves have a frequency-limited depth extent (Barajas
 466 et al., 2022). But, body-to-surface wave scattering at a given frequency is still only sen-
 467 sitive to depths at which a scattering source can excite surface waves. Differences in sen-
 468 sitivity are important to consider when comparing this methodology to other scatterer
 469 characterization methods that use surface-to-surface wave scattering. Since we can only
 470 feasibly apply this technique between 2-10 Hz, this depth sensitivity constraint suggests
 471 that this methodology is only sensitive to the top few hundred meters. But, we suggest
 472 that the depth extents determined in this study are well-constrained by the data. To il-
 473 lustrate this, we perform a simulation for a fault with the same parameters as the best
 474 fitting model for peak β , but change the depth extent from 0-50 m to 0-100 m. The frequency-
 475 amplitude curve for this simulation is plotted as Model 4 in Figure 5. This curve shows
 476 that for a deeper fault, we would expect to observe a frequency-amplitude curve more
 477 depleted in higher frequencies and enriched in lower frequencies.

478 In Y. Yang, Zhan, et al. (2022), the authors discern properties of the fault zone as-
 479 sociated with peak α in this study as a 30% velocity reduction that is 35 m wide and
 480 spans 0 to 90 m depths. While this geometry is very close to our result and provides a
 481 useful verification of our technique, the differences that arise are likely due to the dif-
 482 ferent sensitivities of the measurements and the different frequencies used to fit the fault
 483 model. Namely, the geometry of the faults discerned in this study were partially con-
 484 strained by measurements over 6 Hz, which were not used to constrain the geometry in
 485 Y. Yang, Zhan, et al. (2022). The higher frequency content used in this study likely ex-
 486 plains why the characteristic dimensions discerned in this study are both smaller than
 487 those found in Y. Yang, Zhan, et al. (2022). The higher frequency content may account
 488 for our ability to resolve a shallow burial depth. This fault burial depth is largely con-
 489 strained by subtle variations in the peak shape. To illustrate this, we generate synthet-
 490 ics for a fault model with the same parameters as the best fitting model for peak α , but
 491 use a depth extent of 0-50 m instead of 10-60 m. The frequency-amplitude curve for this

synthetic test is plotted as Model 3 in Figure 5. This result shows, that for an unburied fault, we achieve a slightly different shape that does not capture any separation of the high and low frequency modes of the data curve for peak α .

Finally we note that, although this study focused on relatively minor faults, this methodology can be readily extended to major fault zones, and requires only an across-fault DAS array and earthquake observations. Indeed, since the interrogation length for DAS units is increasing, and since many in situ fibers cross major faults, we can expect the number of DAS arrays sensing structure over major fault zones to increase rapidly over time. The technique presented in this paper presents an opportunity to leverage these DAS arrays to measure the fracture density and characteristics within major fault zones. Moreover, this study only covers one method with which DAS can be used to characterize major fault zones. Many of the aforementioned techniques which have previously used densely deployed conventional seismometers can be performed with DAS. The key challenges in applying these techniques, however, are that DAS provides a different observation than traditional seismometers, single component strain, and that DAS amplitudes are not well understood due to variability in coupling. These differences make some traditional fault characterization techniques, such as detecting fault zone head waves using particle motion analysis or measuring S-wave amplification, more difficult to apply using only DAS data. But, including some conventional inertial seismometers along a DAS array has the potential to diminish some of the challenges of DAS data (e.g. H. F. Wang et al., 2018; Lindsey et al., 2020; Muir & Zhan, 2021; Y. Yang, Atterholt, et al., 2022). For the fault zone characterization case, including collocated 3-component seismic sensors allows for amplitude calibration of DAS data and provides local particle motion observations. In this way, we can leverage the high station density and extensive deployments of DAS data while minimizing its limitations.

7 Conclusions

In this study we present a framework for the systematic location and characterization of fault zones using the DAS measured earthquake wavefield. This framework, which relies on the simple backprojection of the scattered wavefield following an earthquake, yields profiles of the scattered wave energy across the array. We apply this framework to 50 earthquake record sections recorded by a DAS array in Ridgecrest, CA, yielding an ensemble of profiles of scattered wave energy across the array. With these profiles, we identify numerous scattering peaks that are spatially well-correlated with mapped faults in the area, suggesting that these observed scattered waves are faults. Using these backprojection profiles, we suggest a correction to the location of one of the mapped faults in the area. Moreover, we present a model for these scattering sources as rectangular perturbations in the velocity structure, which is a simple approximation of a fault zone, and through simulations we show that this model reproduces first order observations of the observed scattered waves. Using this backprojection technique and these simulations, we establish a framework for using the locally scattered wavefield to evaluate shallow attenuation structure and infer characteristic dimensions of fault zones. We then apply this framework to the profiles computed for the Ridgecrest DAS array and consequently make claims about the fault zone structure near the array. We use the frequency decay of the profile peaks and synthetic simulations to image local faults at the scale of tens of meters, and with these images we distinguish between a fault that is surface-breaching and a fault that is buried.

Open Research

The data used in this study are available online (<https://doi.org/10.22002/D1.20038>) as 30-second record sections that include the initial onset of the earthquake wavefield for the 50 high signal-to-noise ratio aftershocks recorded by the distributed acoustic sens-

ing (DAS) array in Ridgecrest, CA referenced in this study. The simulations performed for this study were done using the software Salvus, (Afanasiev et al., 2019), available at <https://mondaic.com/>. Figure 1 was made using The Generic Mapping Tools (GMT), version 6 (Wessel et al., 2019), available at <https://www.generic-mapping-tools.org/>.

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