A Novel Preparation and Vapour Phase Modification of 2D-open Channel Bio-adsorbent for Uranium Separation

Mudasir Ahmad 1 , Jianquan Ren 2 , Tao Xiu 2 , Mehraj-ud-din Naik 3 , Qiuyu Zhang 2 , and Baoliang Zhang 1

May 25, 2022

Abstract

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Abstract: An economical and highly uranium extraction from seawater remains a crucial task for energy sources and environmental safety. Aiming for improving the mass transfer rate of uranium from seawater, a new synthetic strategy was adopted to synthesize 2D-open channel microporous bio-adsorbent for uranium extraction from seawater. Herein, a vapor phase modification approach was adopted to graft divinylbenzene(DVB), and polyacrylonitrile(AN) onto the surfaces of microporous frameworks via a free radical

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polymerization method. The post-synthetic functionalization was carried out by hydrothermal process, where amidoxime groups are structure-directing agents to trap uranium. Further, amidoxime groups not only enhanced hydrophilicity but also adjusts adsorbents pKa. AO-Fc faces minimum interference of competing ions and achieves a high uranium adsorption capacity of 8.57 ± 0.02 and 409 ± 1 mg/g in seawater and simulated solution. Despite its stable structure, AO-Fc exhibits a long life span and negligible weight loss revealed AO-Fc could be applied as a potential adsorbent for radionuclides.

Keywords: Microporous bioadsorbent; 2D-open channel; vapor-phase modification; uranium

Introduction

A rapid increase in energy demands has given rise to energy shortage, nuclear energy with the advantage of low carbon emission plays an important role in sustainable energy source^{1,2}. Uranium plays a key role in nuclear energy sources, therefore its extraction is very important for continuous energy supply³⁻⁵. However, it is estimated uranium in the terrestrial ores is limited and at the current usage, the terrestrial resources might be ended at the end of the current century⁶. Comparatively, it is estimated that 4.5 billion tons of uranium in seawater is a thousand times higher than terrestrial ores⁷⁻⁹. Therefore, a new strategy needs to develop to extract efficient uranium from seawater to fill the energy gap, environmental protection, and sustainable development. However, the presence of competing ions, low uranium concentration (3.3 ppb), and high-cost synthetic preparation hinder the development of materials for the extraction of uranium from natural seawater¹⁰⁻¹⁴. Various materials such as porous organic polymers (POPs)^{15,16}, covalent organic frameworks (COFs)¹⁷⁻¹⁹, porous aromatic frameworks (PAFs)^{3,20}, metal-organic frameworks (MOFs)^{21,22} and biopolymers²³⁻²⁵ have been used for the extraction of uranium from seawater. Among all of them, amidoximemodified adsorbents are promising with the advantage of high selectivity towards uranium in seawater²⁶⁻²⁹. However, the development of most of the material is either expensive, difficult to synthesize, poor stability and low uranium adsorption efficiency in seawater. Recently, efforts have been devoted to developing advanced materials via simple and facile methods from inexpensive raw materials with ample uranium adsorption capacity.

Charcoal-based materials are highly interested due to their low cost, porous structure, and environmentally friendly nature^{1,30-32}. Recently, amidoxime-modified hollow fibers were used for uranium adsorption³³. Zhou et al. reported 1D porous adsorbent from wood waste for adsorption of polycyclic aromatic hydrocarbons³⁴. Liao et al. reported pig manure-based biochar for uranium extraction³⁵. Wang et al. reported 1D amidoxime modified bamboo charcoal for uranium extraction from seawater³⁶. Although fewer amidoxime modified adsorbents show higher uranium adsorption capacity in natural seawater. However, most of them suffer some drawbacks such as high cost, difficult synthetic procedures, and systematic examination is necessary to find the uranium adsorption mechanism. The efficient adsorption of uranium from seawater in a sustainable way remains a major task due to the lack of functional adsorbent.

In this work, we have implemented two ways to prepare amidoxime polymer chain grafted charcoal adsorbent material by free radical polymerization for uranium adsorption from seawater. (i) polymerization of AN in presence of azobisisobutyronitrile (AIBN) and (ii) the enhancement of polymerization using DVB as a crosslinking agent. Accordingly, a porous polymer chain grafted adsorbent was synthesized chemically for efficient uranium adsorption. Various batch adsorption experiments, theoretical models, and analytical techniques were used to investigate the adsorption characteristics and adsorption mechanism including adsorption capacity, kinetics, and selectivity, the interaction between uranium and chelating sites, interference due to competing ions, and investigation of uranium recovery and adsorbent stability. The uncertainty in uranium adsorption results due to error propagation is also reported in this study.

2. Experimental section

Materials

Wood (Chinese fir) was obtained from Heilongjiang province, China. AN and AIBN, uranyl nitrate, sodium chloride, and sodium bicarbonate were purchased from Changzhou Qidi Chemical Co., Ltd. DVB, hydro-

xylamine hydrochloride (HAHC). NaOH and ethanol were obtained from Hubei Jusheng Technology Co., Ltd. The double-distilled water was obtained from a laboratory filtration plant.

Preparation of nitrile functionalized charcoal (CN-Fc)

Wood (Chinese fir, 5 g) was used as a starting material for the preparation of charcoal in this study. A simple carbonization process was carried out at 600 °C with a heating rate of 10°C/min in a vacuum for 3 h. Thereafter, fir charcoal (0.5 g) was added to a beaker containing AN (5 g) and AIBN (0.1 g) for 30 min. The sample was taken out and put in a glass tube (100 mm in length and 30 mm in diameter). The glass tube was kept in an oven at 180°C for 5 h. To achieve highly polymer grafted materials, 0.8 g of DVB was added to a solution of AN (5 g), and AIBN (0.1 g) under the same set of reaction conditions mentioned above. The obtained products were denoted as CN-Fc and CN-Fc1, where 1 represents an absence of DVB in the reaction system.

Preparation of amidoxime modified charcoal (AO-Fc)

The nitrile group conversion was carried out by adopting a previous method with small modifications³⁶. HAHC (0.48 g) and NaOH (0.25 g) were dissolved in ethanol (15 mL) using an ultrasonicator for 15 min. In the meantime, CN-Fc (0.48 g) and the prepared solution were transferred in a 50 mL Teflon lined autoclave, which was kept at 70°C for 24 h. After cooling, the product was washed with distilled water several times, dried in a vacuum at 60°C for 12 h and the obtained product was denoted as AO-Fc.

Characterization

The morphology was analyzed by using FEI Verios G4 scanning electron microscopy (SEM) and the energy dispersive spectrum (EDS) was carried out by using a Bruker Everhart-Thornley Detector. For chemical structure determination, FTIR (Bruker TENSOR 27 spectrophotometer) and Powder X-ray diffraction (Thermo Scientific 7000 diffractometer) were used. The hydrophilicity was determined using a contact angle analyzer. The thermal stability was analyzed using a Mettler Toledo Thermogravimetric analyzer with a heating rate of 10 °C/min under a nitrogen atmosphere in a temperature range of 40-800°C. The X-ray photoelectron spectrum was obtained by using Kratos Axis Ultra DLD analyzer and the peak fitting of performed using XPS peak fitting program version 4.1. Nitrogen adsorption-desorption was carried out using the Tristar 3020 Micromeritics analyzer.

Uranium extraction from natural seawater

A homemade experimental setup (Figure S1) was developed to investigate the adsorption capacity of the AO-Fc in simulated seawater and natural seawater. The simulated seawater was obtained by dissolving uranyl nitrate (0.017 g), sodium chloride (25 g), and sodium bicarbonate (0.193) in distilled water and further, diluted to obtain different uranium initial concentrations of 0.003 to 1 mg/L. The influence of pH on uranium adsorption, contact time, initial uranium concentration, and the presence of various competing ions was investigated. The pH of the solution was set by adding the required quantity of 0.1 M HNO3 and NaOH solution. For each experiment, the adsorbent was packed in a syringe to hold it and let the penetration of the adsorption solution. The solution was pumped using a lincolin pump with a flow speed of 150 mL/min at room temperature.

For real seawater, we have packed adsorbent (7 mg) in a syringe to hold the adsorbent. A real seawater 20 L was obtained from the South China Sea near Shandong province. The adsorption capacities of metal ions were estimated by collecting a 5 mL sample every day for 39 days. The metal ions concentration was determined by using an inductively coupled plasma emission spectrometer (ICPS-MS, 6300, ThermoFisher Scientific). The uranium adsorption capacity (q_e mg/g) and adsorption efficiency (Ads %) can be written as shown in equation 1 and 2.

$$q_e = \frac{(C_o - C_e)}{m} \times V (1)$$

$$Ads \% = \frac{(C_o - C_e)}{C_o} \times 100 (2)$$

Where q_e is the equilibrium adsorption capacity weight per unit mass (mg/g) C_o and C_e represent initial concentration and equilibrium concentration weight per unit volume (mg/L), V is the volume of solution in liters (L), and m represents mass of adsorbent in grams (g).

To determine the adsorbent regeneration, the adsorbent (7 mg) was eluted by using a 21 mL elution solution (Na_2CO_3 , 1 M and H_2O_2 , 0.1 M) at room temperature for 1 hour to remove the adsorbed uranium from the adsorbent surface. The elution efficiency can be expressed as shown in equation 3.

$$\frac{C_{\rm el} \times V_{\rm el}}{(C_a - C_o) \times V_a} \times 100(3)$$

Where C_{el} denotes elution concentration (mg/L), V_{el} is the elution volume (L), C_{a} represents uranium concentration in seawater after adsorption (mg/L), C_{o} is the initial concentration of metal ions (mg/L) and V_{a} is the volume of seawater used for adsorption (L).

Results and discussion3.1 Adsorbent synthesis and characterization

To achieve efficient uranium extraction from seawater, it is very difficult to prepare a highly porous adsorbent material with higher selectivity and adsorption capacity for uranium in natural seawater. Recently DVB has been used for the preparation of porous polymers for separation purposes³⁷. In this work, polymerization of AN with AIBN as an initiator in presence of DVB as a crosslinking agent has led to active porous polymer chains grafted onto the FC. A well as well developed nanoporous polymer chains with large accessible nitrile groups, which were then converted into amidoxime groups under alkaline conditions for selective adsorption of uranium from seawater with tunable adsorption capacity and surface functionality³⁸. Two polymers grafted carbonous materials were synthesized by free radical polymerization, that is the comonomer AN, and initiator AIBN was polymerized and grafted on FC which was denoted as CN-FC1. By adding the DVB under the same set of reaction conditions mentioned above, it was possible to adjust the pore size and surface structure of the polymer chains grafted onto FC hereafter denoted as CN-FC (Figure 1).

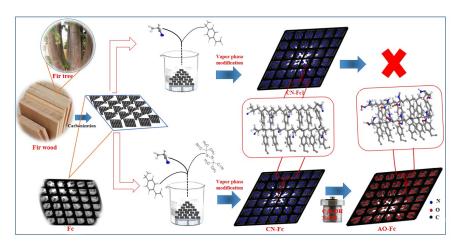


Figure 1 Step by step preparation of AO-Fc adsorbent material

The chemical structure was confirmed by FTIR and XPS analysis. The FTIR spectra of Fc, CN-Fc1, and AO-Fc were shown in Figure 2a. All spectra have similar shapes in the vibration band of carbonaceous material and a peak at 3500-3700 cm⁻¹ was observed due to the presence of OH groups^{36,39}. Afterward, Fc was modified with the aid of AIBN and DVB to yield CN-Fc. On comparing the FTIR spectrum of CN-Fc and CN-Fc1, the peaks in the spectra at 2242 cm⁻¹ were assigned to C[?]N and high peak intensity witnessed the higher payload of nitrile groups were seen on CN-Fc rather than CN-Fc1⁴⁰. The post-synthetic functionalization further converted C[?]N groups into C=N, C-N, and N-O but all of this was confirmed by

respective peaks at 1638 cm⁻¹, 1380 cm⁻¹, and 928 cm⁻¹ indicating the presence of amidoxime groups on the surface of Fc⁴¹. The presence of amidoxime groups were further investigated by XPS analysis (Figure 2); in C 1s high-resolution spectra of AO-Fc (Figure S2a) showed two peaks at 284.45 eV and 285.5 eV assigned to C-N and C=N; in N 1s spectrum of AO-Fc (Figure S2b) showed two peaks at 400.05 eV and 398.40 eV assigned to N-H and C=N respectively³⁶, and the O 1s spectra of AO-Fc (Figure 2b) showed two peaks at 532.5 eV and 531.9 eV assigned to C(NH₂)-N-OH and O-H groups respectively⁴². The powder XRD patterns of Fc, CN-Fc and AO-Fc were shown in Figure 2c. The XRD patterns showed peaks around 16.2° which can be indexed (101) plane and confirmed the amorphous nature of the material⁴³. Furthermore, a broad peak was seen at around 25° and a small peak at nearly 43°, which can be indexed (0002), (1010/1011) plane of graphite and are consistent with the presence of amorphous carbon⁴⁴. The contribution of amidoxime groups on the surface of AO-Fc was calculated by carrying out a thermogravimetric analysis. Compared with Fc, a significant weight loss (80 %) was observed in AO-Fc in the temperature range of 300 °C to 550 °C (Figure 2d). The higher weight loss in AO-Fc was due to a large number of organic groups being thermally decayed, which confirmed the weight contribution of amidoxime groups taken to 80 % of the weight loss of AO-Fc.

Figure 2 FTIR spectra (a), high-resolution XPS spectra of O 1s (b), powder XRD pattern (c), and TGA curves (d)

SEM morphology of the vertical and horizontal cross-section of Fc, CN-Fc1, CN-Fc1, and AO-Fc were shown in Figure 3. The structure of Fc (Figure 3abc) was seen with two-dimensional rectangular two open-end vessels arranged in a proper array with a breadth of 28.6 µm (Figure S3a) and height of 18.3 µm (Figure S3b). SEM images of CN-Fc and CN-Fc1 were not changed obviously after chemical modification (Figure 3de). However, high magnified SEM images showed the rectangular walls were covered with small structures that confirmed the presence of chemical groups. In comparison to Fc, AO-Fc SEM images showed thick wall rectangular vessels (high magnified image) (Figure 3f) without any collapse or damage with a height and breadth of approximately 27.02 µm (Figure S3c) and 14.75 µm (Figure S3d). (Figure 3 j,h,i) showed HAADF-STEM images of CN-Fc, CN-Fc1 and AO-Fc with the corresponding elemental mapping. These images clearly showed a high number of nano precipitates as illustrated in corresponding images (Figure 3 j,k,l,m,n,o) and their elemental percentage was reported in Table 1. These precipitates were mostly C, N, and O which are arranged in a rectangular homogenous pattern. The C and N elements of CN-Fc (Figure 3 j,k) and CN-Fc1 (Figure 3 l,m) were distributed in a rectangular fashion confirming the presence of C and N elements arranged in a homogenous pattern. (Figure 4 n,o) showed the presence of O, and N elements in rectangular patterns confirmed the successful conversion of nitrile groups into amidoxime groups.

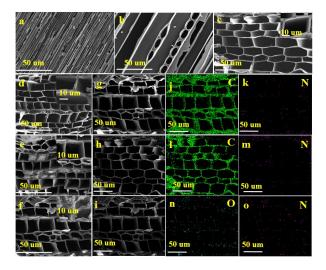


Figure 3 Vertical cross-section SEM images of Fc (a,b), and horizental cross section SEM image of Fc (c),

CN-Fc (d), CN-Fc1 (e) and AO-Fc(f), HAADF-STEM images of CN-Fc (g), CN-Fc1(h), AO-Fc (i), and EDS elemental maping images of CN-Fc (j,k), CN-Fc1(l,m), AO-Fc (n,o)

The bet surface area, pore volume and pore size of Fc, CN-Fc, CN-Fc1 and AO-Fc were analyzed and the results were reported in Table 2. After functionalization of Fc, both surface area and pore volume were decreased from 155 m²/mg to 46 m²/mg and 0.07 cm³/g to 0.007 cm³/g (Figure 4 a,b), because of the large number of amidoxime groups occupying the pores space of Fc. Compared with amidoxime modified bamboo charcoal³⁶, AO-HNTs⁴¹, and fiber⁴⁵ used for uranium extraction, the specific surface area of AO-Fc was relatively higher which might increase uranium adsorption capacity in seawater. The super-hydrophilicity of the material was determined by analyzing water contact angle measurements. The water contact angle of Fc and CN-Fc showed hydrophilicity and reached the water contact angle of 149° and 82.3° at the time of water contact with the adsorbent surface for 13 seconds (see video S1 and S2). On the other side, the water angle of AO-Fc reached 0° angle at a time gap of 0.02 seconds indicating AO-Fc possessed super-hydrophilicity due to the presence of enough hetero groups onto the surface of AO-Fc (see video S3).

Figure 4 Nitrogen adsorption and desorption isotherms (a) and distribution of pore size (b)

Table 1 Elemental analysis by weight percentage (%)

Sample	Elements	Elements	Elements
	С %	N %	О %
Fc	100 ± 0.80	-	-
CN-Fc	91 ± 1.2	$8.5 {\pm} 0.6$	-
CN-Fc1	95.2 ± 0.36	4.9 ± 0.12	-
AO-Fc	57.3 ± 0.36	$28 {\pm} 1.54$	14.7 ± 0.86

Table 2 Nitrogen-adsorption desorption analysis of Fc, CN-Fc1, CN-Fc, and AO-Fc

Sample	Pore size nm	Pore volume cm ³ /g	Surface area m ² /mg
Fc	1.3	0.07	155
$\mathrm{CN} ext{-}\mathrm{Fc}$	0.5	0.04	53
CN-Fc1	1.1	0.05	48
AO-Fc	0.4	0.005	46

3.2 Uranium recovery tests in simulated seawater

3.2.1 Analysis of optimal pH for uranium adsorption

It is well known the pH value of the adsorption solution markedly affects the uranium adsorption performance of the adsorbent due to the presence of different ionic charges present on the adsorbent surface and the uranium ions. Herein we study the effect of pH on uranium adsorption in the pH range of 3 to 10. From Figure 5a, as we have seen the adsorption capacity increased rapidly with increasing pH 3 to 8, at pH 8 the maximum adsorption capacity of AO-Fc was 411±2 mg reported. With a further increase in pH, the adsorption capacity started to decrease. The optimum pH with maximum adsorption capacity of Fc, CN-Fc, and AO-Fc was 5, 6, and 8 confirming the grafting of amidoxime groups adjusted the pKa value, resulting in shifting of pH to alkaline which is favorable for uranium under seawater conditions. The AO-Fc showed a positive shift towards an optimal pH of 8 towards the alkaline phase whereas the CN-Fc showed a small shift with an optimal pH of 6, confirming the role of amidoxime groups to shift the pKa of the base material. Further, NaCl showed no influence on uranium adsorption of AO-Fc, CN-Fc, and Fc (Figure 5b) indicated a high concentration of NaCl in seawater would not affect the uranium adsorption capacity of AO-Fc in seawater conditions.

Figure 5 Effect of solution pH (a) and various concentration of NaCl (b) on uranium adsorption capacity (mg/g)

3.2.2 Effect of contact time for uranium adsorption capacity

To investigate the adsorption kinetics, the influence of contact on uranium adsorption onto adsorbent was analyzed for the contact time ranges of 5 to 450 min. As shown in Figure 6a, AO-Fc showed adsorption amount increasing rapidly from 5 to 80 min, indicating strong uranium adsorption from the initial uranium concentration solution. However, after 80 min the adsorption rate was decreased due to a decrease in diffusive resistance and active sites on the surface of AO-Fc during the adsorption process of uranium by amidoxime groups. After 350 min, there was no significant change in the adsorption amount of AO-Fc, confirming the absorption process achieved the equilibrium of adsorption at 350 min. CN-Fc and Fc showed lower adsorption capacity in comparison to AO-Fc due to the presence of low chelating sites and no significant adsorption capacity was increased after 150 min equilibrium of adsorption indicating equilibrium of adsorption was achieved. It is worth to report the longer equilibrium time and slower diffusion were attributed due to the low surface area and internal microporous structure of AO-Fc. To analyze the adsorption kinetics and mechanism various theoretical models including linear pseudo-first order (LPFO) and pseudo-second order kinetics(LPSO) and non-linear pseudo-first order (NLPFO), and pseudo-second order kinetics (NLPSO) (supporting information).

Both linear and non-linear plots of the pseudo-first order model and pseudo-second order model and their kinetic parameters were shown in Figure 6b, Figure S4, Figure S5, Table 3, and Table S1. The kinetic parameters of linear plots of the pseudo-first order model and pseudo-second order model were obtained by easily plotting a graph between $\ln (q_e-q_t)$ versus t and t/qt versus t and the relevant parameters for studying the uranium adsorption were listed in Table 3 and Table S1. The kinetic parameters of non-linear plots of the pseudo-first order model and pseudo-second order model were calculated by plotting a graph between q_tversus t and the relevant parameters were shown in Table S2. From the results of both linear and non-linear model fit (Table 3, Table S1, and Table S2), the correlation coefficient (R²) of the pseudosecond-orde model was close to unity than the pseudo-first order model, confirming the pseudo-second order was better to discuss the adsorption behavior over entire adsorption process. The pseudo-second kinetic model is based on the assumption that the rate-limiting step follows the chemisorption process through sharing valance electrons between uranium and the chelating site. Also, the validity of the pseudo-second order model fit was investigated by calculating the p-value, q_{ecal} value (Figure S6), and statistical errors (supporting information), indicating the experimental data were best fitted with the pseudo-second order. According to the theoretical calculation of Azizian et al. the adsorption experiment was carried out at a high initial concentration of solute >250 mg/L, the adsorption data were best fitted with pseudo-first order rather than the pseudo-second order⁴⁶.

3.2.3 Effect of equilibrium concentration on uranium recovery

To determine the adsorption capacity of AO-Fc, equilibrium adsorption studies were performed in a simulated uranium solution at different initial uranium concentrations. As shown in Figure 6c, the uranium adsorption amount increased rapidly with increasing the initial uranium concentration, but in due course, the absorption capacity reached a plateau, which meant the adsorption capacity had reached the maximum adsorption capacity of the adsorbent. It was attributed, to more opportunities to adsorbent intact with the higher uranium initial concentration until the maximum adsorption capacity was achieved. Further, the adsorption capacity of AO-Fc was higher than CN-Fc and Fc due to the presence of amidoxime groups. To measure the adsorption amount of adsorbent for uranium, various linear and non-linear isotherm models such as the Langmuir isotherm model, Freundlich isotherm model, and Temkin isotherm model were applied to treat the experimental adsorption data at various uranium concentrations (Supporting information).

The fitting results of AO-Fc, CN-Fc, and Fc were shown in Figure 6d, Figure S7, and Figure S8, and the values of various parameters are listed in Table 4 and Table S3, and Table S4. From results listed in Table 4 and Table S3 and Table S4, for AO-Fc the Langmuir isotherm model showed a higher regression

coefficient (R^2 =0.998) than the Freundlich isotherm(R^2 =0.944) and Temkin isotherm (R^2 =0.985), confirming the uranium adsorption onto the surface of AO-Fc followed a homogenous and monolayer adsorption coverage. Moreover, the applicability of the isotherm model was checked by calculating various statistical errors. For AO-Fc the Langmuir isotherm model showed lower error values as compared to the Freundlich isotherm and Temkin isotherm, indicating the experimental data were best fitted with the Langmuir isotherm. Also, for AO-Fc the q_m (mg/g) calculated from the Langmuir isotherm model was 420 ± 12 mg/g at an equilibrium concentration of (0.5 mg/L), which was compared with the previously reported amidoxime adsorbents till now (Table 5). The results from Table 5 showed a higher adsorption capacity for AO-Fc, indicating that it had greater potential to extract uranium from an aqueous solution.

Figure 6 Adsorption kinetics of uranium onto AO-Fc, CN-Fc, and Fc, the effect of contact time (a), linear fitting by the pseudo-second order (b) (T = 303 K and adsorbent dosage = 0.01 mg/L), the effect of uranium initial concentration (c) and linear fitting by the Langmuir isotherm (d) (T = 303 K; adsorbent dosage = 0.01 mg/L and t = 350 min)

Table 3 Kinetic parameters for uranium obtained by linear regression.

Pseudo second order model

Adsorbent	$ m K_2~g/mg~min^{-1}$	q _{eexp} mg/g	q _{ecal} mg/g	\mathbb{R}^2	p-value	SSE	SAE	X^2	$\Delta q(\%)$
AO-Fc	$0.00012{\pm}2\text{E-}05$	410.000 ± 0.004	400 ± 10	0.996	9.6E-08	15.9	9.2	12.2	3.2
CN-Fc	$0.00094 \pm 7 \text{E-}05$	30.00 ± 0.01	29 ± 1	0.996	1.1E-08	1.6	4.7	1.0	3.3
Fc	$0.00124 {\pm} 0.0001$	19.000 ± 004	19 ± 1	0.989	1.1E-07	1.2	10.0	1.8	3.5

Table 4 Isothermal parameters for uranium obtained by linear regression

	Langmuir isotherm model	Langmuir isotherm model	Langmuir isotherm model	Langmuir isotherm model	Langmuir isotherm model	Langmuir isotherm model	Langmuir isotherm model	Langmuir isotherm model	La iso mo
Adsorbent	q_{eexp} mg/g	$ m K_L \ L/mg$	q _{ecal} mg/g	q _m mg/g	\mathbb{R}^2	SSE	SAE	X^2	$\Delta \epsilon$
AO-Fc	409±1	73.03638010 09	0 ±20 E65±0.02	420 ± 12	0.998	70	67	237	7
CN-Fc	30 ± 1	10.280936±3	$3E29.560\pm0.003$	232.5 ± 0.7	0.998	2	3	4	3
Fc	17±2	6.82781±4E- 05	- 16.330±0.004	419±2	0.999	2	1	4	3

3.3 Uranium recovery in seawater

To analyze the uranium adsorption capacity of AO-Fc in real seawater, an adsorbent (7 mg) was added to a homemade adsorbent holder (syringe, Figure S1) and exposed to 20 L seawater and the complete homemade uranium adsorption set-up was shown in (Figure S1). The amount of uranium adsorbed from seawater was analyzed by knowing uranium concentration at different time intervals using (ICP-MS). For industrial applications, the adsorbent can be directly used to lower surface seawater for uranium extraction. The uranium adsorption kinetic results revealed that AO-Fc showed 6.60 mg/g adsorption capacity within one week, which was 75% of the total uranium adsorption. The maximum adsorption capacity reached 8.57 mg/g with 100% adsorption efficiency after 11 days of the adsorption experiment (Figure 7ab). In comparison, AO-Fc showed efficient uranium adsorption from seawater (Table 5). Uranium adsorption capacity reflects the direct measurement of the amount of uranium adsorbed by an adsorbent and the distribution coefficient (K_d), determines the adsorbent affinity towards adsorbate. These results indicated that the adsorbent retaining

high uranium adsorption capacity in presence of other coexisting ions might have a correspondingly higher K_d value than other coexisting ions in Figure S9. Based on that, the evaluation of K_d (L/g) is an important parameter for choosing the most suitable adsorbent for further analysis.

Figure 7 Kinetics of uranium extraction (a) and adsorption efficiency of adsorbent in seawater (b)

Table 5 Comparison of various adsorbents for uranium extraction in seawater

Adsorbent	Volume of seawater (L)/location	Adsorbent mass grams	Adsorption time(days)	Adsorption capacity(mg/g)	References
UiO-66-AO	1/Bohai Seawater	1	3	2.7	47
Anti-UiO-66	10	2	30	4.6	48
Anti-UiO-66	Simulated solution	-	-	2.84	
UiO-66-3C4N	100/South China Sea	0.2	28	6.9	49
UiO-66-3C4N	Simulated solution	-		380.3	
BP@CNF- MOF	100/ South China Sea	1	42	6.8	50
UiO-66-NH- (AO)	25/South China Sea	0.2	8	5.2	51
AOÓBCH	Simulated seawater	-	30	6.7	36
AI Series Adsorbents	Sequim Bay	-	56	3.52	52
Amidoxime PVC-co- CPVC fiber	Sequim Bay	-	42	3.2	53
AO-Fc	20/South China Sea	0.35	11	8.6	Present work
AO-Fc	Simulated solution	-	0.236	409 ± 1	

3.4 Adsorbent stability and interaction with uranyl ions

The morphology of the adsorbent after uranium extraction/elution was analyzed by using SEM analysis. From Figure S10, the SEM image of AO-Fc after uranium extraction (Figure S10a) and uranium elution (Figure S10b) confirmed that seawater exposed AO-Fc maintained the integrity of structure after reuse of several cycles for a long time of seawater exposure. The detailed chemical composition of the uranium-loaded adsorbent (AO-Fc-U) adsorbent was analyzed by XPS and FTIR analysis and the results were compared before uranium adsorption of adsorbent (AO-Fc) (Figure 8). The uranium-loaded adsorbent (AO-Fc-U) showed two peaks at 390.9 eV and 380.1 eV assigned to U $4f_{5/2}$ and U $4f_{7/2}$ confirming the presence of uranium on AO-Fc (Figure 8a). As shown in Figure S11a, two types of Nitrogen peaks were observed at 400.05 eV and 398.4 eV assigned to N-H and C=N respectively. And also from Figure S11b, the binding energy of both N-H and C=N shifted to higher binding energy at 400.9 eV and 399.1 eV. The positive shift in N-H and C=N groups confined the coordination of nitrogen and uranium ions. Further, the uranium-loaded adsorbent was analyzed by FTIR and the results were compared (Figure 8b), the uranium-loaded spectra

showed shifts at various peaks or increase peak intensity. What is more, in the FTIR spectrum of AO-Fc, two new peaks were observed at 937 cm⁻¹ and 1161 cm⁻¹ confirming the presence of uranium on AO-Fc^{54,55}.

3.5 Adsorbent regeneration and elution efficiency

Reusability is an important parameter for the industrial application of adsorbents that influences the cost of the adsorbent. For the reusability test, AO-Fc (7 mg) was used in 20 L seawater and the elution solution (1 M Na₂CO₃ and H₂O₂ 0.1 M) was fixed at 3 mL per milligram of seawater exposed adsorbent. For uranium elution, the elution efficiency reached 99.9 % within 20 min, indicating the desired elution solution was better for uranium removal from AO-Fc (Figure 8c). The overall decrease in adsorption capacity and elution efficiency of AO-Fc were 1.8 % and 2 % up to seven cycles (Figure 8d and Figure S12a), confirming the adsorbent can be used for several cycles, which would significantly decrease the uranium extraction cost. The decrease in adsorption capacity and elution efficiency might be due to the strong binding of uranyl ions with active functional groups. The adsorbent showed excellent structural stability and negligible weight loss of adsorbent (Figure S12b) after seven adsorption-desorption cycles of AO-Fc.

Figure 8 High-resolution XPS spectra of U 4f (a), FTIR spectra (c), elution efficiency of uranium in 1 M Na₂CO₃ and H₂O₂ 0.1 M (c), and uranium adsorption capacity of AO-Fc in seawater (d)

Conclusion

In conclusion, the new low-cost and facile prepared amidoxime modified adsorbent were analyzed qualitatively and quantitively and can be considered as a potential adsorbent for uranium recovery from seawater. AO-Fc showed significant adsorption capacity and higher uranium selectivity, which is attributed due to amidoxime groups being present on the surface of the 2D-open channel. In addition, the addition of amidoxime groups not only enhanced the adsorption capacity and cracks the hydrophilicity but also adjusted the adsorbent pKa value.

The BET surface area of AO-Fc was lower as compared to Fc, indicating the surface area was not a grim factor for the adsorption mechanism. The uranium adsorption on AO-Fc was strongly dependent on pH value confirming the adsorption mainly occurred due to surface complexation.

The experimental adsorption simulation by various isotherm models exhibited that the R^2 value of Langmuir isotherm was close to unity obtained by linear regression. Also, the q_e calculated and the statistical analysis confirmed the adsorption data were best fitted with the Langmuir isotherm than other isotherm models.

Kinetic studies showed very fast uranium adsorption and the equilibrium of adsorption was achieved in 11 days, which was a lower contact time as compared to the adsorbents reported in Table 5 for uranium extraction from natural seawater.

The desorption and regeneration showed the adsorbent is economically and environmentally efficient. The higher adsorption capacity of AO-Fc towards uranium exhibits that the materials can be potential adsorbents for uranium extraction under seawater conditions.

Acknowledgment

This work was financially supported by the National Natural Science Foundation of China (No.21975206).

Conflict of interest

The authors declare no conflict of interest.

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