

# Flame Synthesis of Pd-TiO<sub>2</sub> Nanocomposite Catalyst for Oxygen Removal from CO<sub>2</sub>-rich Streams in Oxy Combustion Exhaust

Sungyoon Jung<sup>1,1</sup>, Nathan Reed<sup>1</sup>, Gregory Yablonsky<sup>1</sup>, and Pratim Biswas<sup>1</sup>

<sup>1</sup>Washington University in St. Louis

April 28, 2020

## Abstract

Pd-TiO<sub>2</sub> catalysts with five Pd loadings were synthesized using a flame aerosol reactor. Their initial and changed catalytic properties and kinetic characteristics during/for O<sub>2</sub> removal with CH<sub>4</sub> were investigated. Different Pd loadings affected the size of Pd sub-nano clusters/nanoparticles and the speciation fraction of Pd (metallic Pd, PdO and PdO<sub>x</sub> (0 < x < 1)). Increased size of Pd nanoparticles on catalysts' surface due to sintering and the reduction of PdO to metallic Pd or/and PdO<sub>x</sub> were observed during the reaction. Fractions of the total surface area of Pd species were calculated, and correlations to the apparent reaction rate constants were established. Apparent kinetic constants were linearly proportional to fractions of total surface areas of metallic Pd or/and reduced Pd oxide were revealed, representing the intrinsic active site. The linear correlation between the O<sub>2</sub> reaction rate and the CO<sub>2</sub> concentration in the initial gas stream was also observed due to an autocatalytic reaction effect.

## 1. Introduction

The emission of CO<sub>2</sub> from fossil fuel combustion in power plants is one of the dominating contributors to global warming.<sup>1,2</sup> The U.S. Energy Information Administration reported that more than 60% of the energy in the U.S. was produced by fossil fuel combustion in 2018, and approximately half of it was generated from coal combustion.<sup>3</sup> Based on this percentage, energy-related CO<sub>2</sub> emission from coal combustion in 2018 was reported as approximately 1.3 Gt which was 24% of the total CO<sub>2</sub> emissions from fuel sources.<sup>4</sup> To mitigate the CO<sub>2</sub> level in the atmosphere, alternative energy sources, such as nuclear power and renewable energy, can be used,<sup>1</sup> but they currently cannot meet the immediate energy demand. Fossil fuel combustion is still necessary,<sup>1</sup> so removing CO<sub>2</sub> from fossil fuel combustion remains a pressing need.

Oxy combustion is a promising technique that has improved combustion efficiency and produces a flue gas with a high concentration of CO<sub>2</sub>, which can be effectively captured.<sup>1,2,5,6</sup> Conventional coal combustion uses air, which dilutes the CO<sub>2</sub> concentration in the flue gas and thus requires an additional process (e.g., amine stripping) to capture CO<sub>2</sub> from the diluted flue gas. Oxy combustion uses highly pure O<sub>2</sub> (>95%) instead of air, which results in high combustion efficiency, low fuel consumption, and a concentrated CO<sub>2</sub> stream.<sup>1,6</sup> The captured CO<sub>2</sub> can be either sequestered<sup>7</sup> or reused for enhanced oil recovery (EOR).<sup>8</sup> Although a high concentration of CO<sub>2</sub> (~63%) in the flue gas can be achieved, it cannot be directly applied for EOR or sequestration because the residual concentration of O<sub>2</sub> (~3%) is higher than the requirement for EOR (<100 ppmv).<sup>9</sup> Therefore, O<sub>2</sub> must be removed from the flue gas before reuse.

Catalytic O<sub>2</sub> removal with hydrocarbons (e.g., methane) is one promising solution. Up until now, studies have focused on catalytic CH<sub>4</sub> combustion for generating energy in gas turbine combustors, and on using metal doped catalysts to decrease emissions.<sup>10-13</sup> There has been progress toward effective CH<sub>4</sub> oxidation at low temperature (<773 K) and considerable work in studies of this system at different compositions, temperatures, and pressures over different metal doped catalysts (e.g., Pd-Al<sub>2</sub>O<sub>3</sub>, Pt-Al<sub>2</sub>O<sub>3</sub>, Pd-SiO<sub>2</sub>).<sup>11,14</sup> However, there is a significant difference between prior catalytic CH<sub>4</sub> combustion studies and this work. Most

previous studies on catalytic CH<sub>4</sub> combustion used a relatively high O<sub>2</sub> concentration with N<sub>2</sub> or He, as the balance of the gas, or relatively low concentrations of CO<sub>2</sub> (<20%) to investigate their effects on the reaction. The challenge of this work is to decrease oxygen levels in low concentration O<sub>2</sub> streams (from 3% to less than 100 ppmv) in a highly concentrated CO<sub>2</sub> stream. Recent studies have shown the catalytic O<sub>2</sub> removal with CH<sub>4</sub> as a promising technique, and reported high O<sub>2</sub> conversions (>95%) by using noble metal doped catalysts (e.g., Pd-zeolite and Pd (or PdCu)-Al<sub>2</sub>O<sub>3</sub>).<sup>15,16</sup> Even though high O<sub>2</sub> conversion was achieved, two important aspects affecting the catalytic activity for O<sub>2</sub> removal were not fully investigated. First, active sites of the catalysts were not clearly elucidated. Noble metals such as Pd and Pt are known to have high catalytic activity for various applications.<sup>11,17-22</sup> However, there is still an ongoing debate on the active phase of noble metals for catalytic performance.<sup>19-22</sup> For example, the catalytic CH<sub>4</sub> combustion with noble metal supported catalysts strongly depends on the oxidation state of noble metal: Schmal et al.<sup>19</sup> reported that the coexistence of PdO and PdO<sup>δ+</sup> played a crucial role in the enhanced CH<sub>4</sub> combustion. Yang et al.<sup>23</sup> showed that Pd<sup>0</sup>/PdO<sub>x</sub> (0 < x < 1) was the active phase for CH<sub>4</sub> combustion. To design a catalyst which has higher catalytic activity for O<sub>2</sub> removal, it is necessary to fully understand the active phase of noble metal. Second, the effect of excess CO<sub>2</sub> in the initial gas stream on the catalytic performance for O<sub>2</sub> removal has not been explored. Therefore, additional efforts are required to develop effective O<sub>2</sub> removal from oxy combustion systems.

Metal oxide catalysts doped by noble metals have been extensively researched for oxidation studies.<sup>11,24</sup> To synthesize these catalysts, several methods, e.g., wet impregnation, sol-gel, and precipitation, have been widely utilized. However, these methods require additional processes, such as drying and calcination.<sup>25</sup> Unlike these methods, flame synthesis is a continuous one-step process that can be scaled up for high throughput production of nanoparticles.<sup>26-28</sup> Furthermore, many researchers have reported higher catalytic activity of flame-made catalysts due to their excellent dispersion of metal clusters on a metal oxide support.<sup>29-31</sup> Recently, Fujiwara et al.<sup>32,33</sup> synthesized sub-nano scale metal clusters on a metal oxide support by controlling the residence time in a flame and reported a much higher fraction of metal atoms on the catalyst surface and strong metal-support interaction, both of which enhanced the catalytic activity. In addition, Wang et al.<sup>34</sup> developed size-controlled Pt (<2 nm) doped TiO<sub>2</sub> films and found that the size of the Pt particles plays a crucial role in CO<sub>2</sub> photoreduction. However, there is still insufficient information about the fate of the nanoparticle catalysts and its correlation to the active phase of materials during the oxidation reaction.

In this study, Pd-TiO<sub>2</sub> catalysts were synthesized by using a flame aerosol reactor. The kinetic characteristics of the synthesized catalysts for O<sub>2</sub> removal were evaluated. Pd-TiO<sub>2</sub> catalysts were synthesized with five different Pd loadings to investigate their catalytic properties. Their changed catalytic properties during the reaction were also investigated. The total surface area of different Pd species (metallic Pd, PdO and PdO<sub>x</sub> (0 < x < 1)) in the as-prepared and the treated catalysts was calculated for every loading, and the relationship between the fraction of the total surface area of different Pd species and apparent reaction rate constant was established. In kinetic experiments, the effect of different initial gas compositions on O<sub>2</sub> removal was investigated. The goal of this paper is to develop an efficient correlation between structural characteristics and steady-state kinetic characteristics that characterize the prepared catalysts. This relationship can be used as an important tool for primary kinetic characteristics of the catalyst and further catalyst design.

## 2. Experimental section

The synthesis method is described first, followed by characterization methods, and finally, a test plan is presented.

### 2.1 Synthesis of Pd-TiO<sub>2</sub> catalysts using a flame aerosol reactor (FLAR)

The experimental setup for synthesizing Pd-TiO<sub>2</sub> catalysts is shown in Figure S1a in Supporting Information. The flame aerosol reactor (FLAR) system includes a precursor feeding system (bubbler and nebulizer), a diffusion burner, and a quenching and collection system. The bubbler was used for feeding titanium tetraisopropoxide (TTIP, 99.7%, Sigma-Aldrich) with an N<sub>2</sub> carrier gas (1 L min<sup>-1</sup>). The temperature of the oil bath in which the bubbler was placed was maintained at 323 K. The precursor delivery tubes were maintained

at around 373 K. The saturated TTIP precursor vapor was introduced into the central port of the burner. Palladium acetylacetonate ( $\text{Pd}(\text{acac})_2$ , 97%, Sigma-Aldrich) was used as a dopant precursor, and it was dissolved in xylene (reagent grade, Sigma-Aldrich) and acetonitrile (99.8%, Sigma-Aldrich) mixture (2:1, v/v). In this study, five different Pd-TiO<sub>2</sub> catalysts were synthesized by controlling the concentration of the Pd precursor solutions (0.5 mM ~3.0 mM). A three-jet Collision nebulizer was used to generate spray droplets, which were introduced to the central port of the burner. CH<sub>4</sub> and O<sub>2</sub> were introduced through the second and the outer port of the burner, respectively, with flow rates of 0.35 L min<sup>-1</sup> and 2.5 L min<sup>-1</sup>. The distance between the quench ring and the top of the burner was fixed at 3.8 cm. The synthesized catalysts were collected using an isopore membrane filter.

## 2.2 Characterization of synthesized Pd-TiO<sub>2</sub> catalysts

The elemental analysis was conducted by both inductively coupled plasma mass spectroscopy (ICP-MS, Elan DRC ii, PerkinElmer) and field scanning electron microscopy (FESEM, JEOL 7001LVF FE-SEM, JEOL Ltd.) coupled with energy disperse X-ray spectroscopy (EDS). X-ray diffraction (XRD, Bruker d8 advance, Bruker) was utilized to investigate the crystallinity of the synthesized Pd-TiO<sub>2</sub> catalysts by using CuK $\alpha$  radiation ( $\lambda = 1.5418 \text{ \AA}$ ) and a step size of 0.02°. The morphology and size of the synthesized catalysts were determined by scanning transmission electron microscopy (STEM) (TEM, JEOL 2100F, Jeol). The oxidation state of Pd was evaluated by X-ray photoelectron spectroscopy (XPS, Versa probe ii, Physical Electronics). Analyses for ICP-MS, XRD, and XPS were performed in triplicate. FESEM-EDS and STEM analyzed many spots for representative data. To investigate the changes in the catalytic properties, catalysts were treated at elevated temperatures up to 773 K for around 1 hr each temperature under the same experimental conditions and hereafter denoted as treated catalysts. They were further characterized by using the same analytical tools mentioned above.

## 2.3 Experimental setup and procedure

Figure S1b shows a differential fixed-bed reactor system. The feed gases are supplied from gas cylinders, and the gas composition is controlled by mass flow controllers. The differential fixed-bed reactor has three indentations in the middle to hold catalysts with glass fiber. Due to the low flowrate (~ 3 mL min<sup>-1</sup>), the glass fiber supports the catalyst well. A thermometer and temperature controller (Econo Temperature Controller, ACE Glass Inc.) are used for temperature control. To perform an experiment, 10 mg of the catalyst was loaded into the reactor. The experiment was conducted at temperatures ranging between 298 K and 773 K and under atmospheric pressure. The gas feed stream consisted of O<sub>2</sub> and CH<sub>4</sub> in balance CO<sub>2</sub>, with a total flow rate of 3.2 mL min<sup>-1</sup>. In this study, three different CO<sub>2</sub> concentrations (i.e., 0%, 53%, and 95% in balance He), and three different ratios between O<sub>2</sub> and CH<sub>4</sub> concentrations (i.e., O<sub>2</sub> rich composition: O<sub>2</sub>/CH<sub>4</sub>  $\cong$  2.4, stoichiometric composition: O<sub>2</sub>/CH<sub>4</sub>  $\cong$  2.0, O<sub>2</sub> lean composition: O<sub>2</sub>/CH<sub>4</sub>  $\cong$  1.6) were used. The compositions of the gas streams were sampled through an automatic gas valve and measured by gas chromatography (GC, 7890B, Agilent Technologies, Inc.), using helium as a carrier gas. The GC was equipped with a porous layer open tubular (PLOT) capillary column (Supelco Carboxen-1010) and a thermal conductivity detector (TCD).

# 3. Results and discussion

## 3.1 Flame synthesis of the catalysts and their structures' characterization

During the synthesis process, TTIP vapors generated from the bubbler and Pd precursor acetylacetonate salts decompose at the different temperature regions in the flame.<sup>26</sup> In the lower temperature region of the flame, TTIP vapors first form TiO<sub>2</sub> monomers, which subsequently undergo particle growth by collision, coalescence, and sintering. In the higher temperature region of the flame, Pd acetylacetonate salts decompose to form Pd vapor molecules, which can either condense or nucleate and subsequently be deposited on the surface of the created TiO<sub>2</sub> nanoparticles.<sup>26</sup> The condensed or deposited Pd molecules on the surface further diffuse and coalesce.<sup>33</sup> Varying the Pd concentrations can change the possibility of colliding with other molecules on the surface, which results in different sizes of Pd clusters/particles on the TiO<sub>2</sub> surface, and a previous study reported increasing sizes of Pd clusters on the TiO<sub>2</sub> surface with increasing Pd loading.<sup>33</sup>

Also, under the flame synthesis conditions, different Pd species (e.g., metallic Pd and PdO) can be expected. At high temperature, some oxidation of Pd can occur due to the presence of excess oxygen.<sup>35</sup> For the same residence time in the flame, the oxidation extent of metal might depend on the metal concentration. In this study, five different Pd-TiO<sub>2</sub> catalysts were synthesized by varying the concentration of Pd precursor solution from 0.5 mM to 3.0 mM. The synthesized Pd-TiO<sub>2</sub> catalysts were characterized by different analytical tools, as described below.

### 3.1.1 Determining Pd loadings (ICP-MS and FESEM-EDS)

ICP-MS confirmed the existence of Pd in the Pd-TiO<sub>2</sub> catalysts, and the specific Pd loading was determined by the same instrument (Table 1). As can be seen in Table 1, the Pd loading values (wt%) obtained from ICP-MS increased from 0.24 wt% to 1.25 wt% with increasing concentrations of Pd precursor solution. It is worth noting that similar Pd loadings were obtained by FESEM-EDS, which reveals that most Pd particles were distributed on the catalyst surface, not in the bulk structure. It should be also noted that the treated catalysts at 773 K showed similar Pd loadings (data not shown), which implies that most Pd particles were still dispersed on the catalyst surface. The values obtained by ICP-MS were used for clarification of catalysts and further calculations. The five different Pd-TiO<sub>2</sub> catalysts are hereafter denoted as catalyst 1 (0.24 wt% Pd), catalyst 2 (0.45 wt% Pd), catalyst 3 (0.76 wt% Pd), catalyst 4 (1.08 wt% Pd), and catalyst 5 (1.25 wt% Pd), respectively. Based on the ICP-MS analytical results, the total Pd masses in 10 mg of Pd-TiO<sub>2</sub> catalyst ( $M_{\text{Total Pd}}$ ), the mass used for all experiments, were calculated ( $10,000 (\mu\text{g}) \times \text{Total Pd loading (wt\%)} / 100$ ) and are shown in Table 1. As the concentrations of Pd precursor solution are increased,  $M_{\text{Total Pd}}$  also increases, from 23.98  $\mu\text{g}$  to 125.25  $\mu\text{g}$ .

### 3.1.2 Distinguishing crystallinities of the catalysts and phase transformation (XRD)

The crystal structures of the synthesized fresh and the treated Pd-TiO<sub>2</sub> catalysts were evaluated by XRD, and Figure 1 shows their XRD spectra in the  $2\theta$  range of 20° to 60°. In the case of the fresh catalysts, a distinct peak of anatase (101) TiO<sub>2</sub> was obtained at a  $2\theta$  angle of 25.3°, and low-intensity of anatase (004), anatase (200), and anatase (211) peaks were observed at  $2\theta$  angles of 37.8°, 48.1°, and 55.1°, respectively. The XRD patterns revealed that the fresh catalysts have only TiO<sub>2</sub> anatase crystal structure, which correlates well with the JCPDS patterns of anatase (00-021-1272). In addition, the peak intensities for all crystal structures of Pd-TiO<sub>2</sub> catalysts were very similar to each other and similar to that of the pristine TiO<sub>2</sub> catalyst, which indicates that the addition of Pd did not change the crystal structure of the TiO<sub>2</sub>. On the other hand, distinct peaks for Pd metal and PdO were not observed, which might be due to the extremely low Pd loading or to the very small sizes of the Pd clusters/particles.

In the case of the treated catalysts, distinct peaks of anatase and rutile TiO<sub>2</sub> were obtained like the fresh catalysts: Noticeable peaks of anatase (101), anatase (004), anatase (200), and anatase (211) were observed. In addition to these anatase peaks, low-intensity of rutile (110) and rutile (101) peaks were obtained at a  $2\theta$  angle of 27.3° and 36.1°, respectively, which match with rutile phase of TiO<sub>2</sub> (JCPDS 75-1753). A slightly shifted peak of Ti<sub>2</sub>O<sub>3</sub> (116) was also observed at approximately 54.2°. As can be seen in Figure 1b, all treated catalysts showed the peaks at the same  $2\theta$  angles, which indicates that they contain the mixed crystalline structures of TiO<sub>2</sub> (anatase and rutile) and Ti<sub>2</sub>O<sub>3</sub>. However, the intensities of the observed peaks were somewhat different. To clearly see the differences, two magnified versions of figures are shown in Figure 1c (the pink-colored region at a  $2\theta$  angle ranging from 26° to 43° in Figure 1b) and Figure 1d (the grey-colored region at a  $2\theta$  angle ranging from 50° to 60° in Figure 1b). According to Figure 1c and 1d, it can be noted that the intensities of peaks of rutile (110), rutile (101), and Ti<sub>2</sub>O<sub>3</sub> (116) were decreased as the Pd loading was increased from catalyst 1 to catalyst 5, while the peak intensity of anatase did not change much. Based on the obtained results, the intensity ratios between anatase (101) ( $I_{A101}$ , the strongest peak of anatase) and rutile (110) ( $I_{R110}$ , the strongest peak of rutile) and between  $I_{A101}$  and Ti<sub>2</sub>O<sub>3</sub> (116) ( $I_{Ti2O3116}$ ) were calculated. The calculated intensity ratio between  $I_{A101}$  and  $I_{R110}$  was decreased from 0.168 to 0.112 as the Pd loading was increased from catalyst 1 to catalyst 5. The calculated intensity ratio between  $I_{A101}$  and  $I_{Ti2O3116}$  also showed the same decreasing trend from 0.184 to 0.166 with increasing the Pd loading. The previous study by Tiwari et al.<sup>26</sup> reported that the phase transformation of TiO<sub>2</sub> can be suppressed under

a high temperature condition by incorporating a noble metal dopant due to its surface modification. Our current result was consistent with this previous study. On the other hand, the low-intensity peak of PdO was observed with treated catalysts and its intensity was increased as the Pd loading was increased. This sudden appearance of PdO in treated catalysts can be attributed to the sintering effect of Pd on the TiO<sub>2</sub> surface, which will be discussed more in further sections.

### 3.1.3 Investigating similarities and differences of morphology and size of Pd and Pd-TiO<sub>2</sub> between fresh and treated catalysts (STEM)

The surface morphology and size of the synthesized fresh and treated Pd-TiO<sub>2</sub> catalysts were investigated by STEM (Figure 2). In each case, we counted more than 200 particles to evaluate the particle size distribution of the Pd-TiO<sub>2</sub> particles, and the results are shown in the first column of Figure 2a-e and in Table 1. In the case of the fresh catalyst, the five Pd-TiO<sub>2</sub> catalysts had similar size distributions of their bulk structure, and similar average particle sizes ( $d_{av, Pd-TiO_2}$ ):  $7.57 \pm 2.19$  nm,  $7.18 \pm 2.07$  nm,  $7.61 \pm 2.11$  nm,  $7.14 \pm 1.04$  nm, and  $7.34 \pm 1.91$  nm, respectively (red-colored bars in the first column of Figure 2) (Table 1). The five fresh catalysts also had similar spherical shapes, as can be seen in the second column of Figure 2a-e. These results reveal that the addition of Pd did not change the particle morphology and size of the bulk structures. From STEM images, it was confirmed that there were no noticeable Pd subnano-clusters at the lowest Pd loading (catalyst 1) (Table 1). On the other hand, extremely small Pd subnano-clusters/nanoparticles (bright dots, circled in yellow in the second column of Figure 2), were observed. Pd subnano-clusters (<1 nm) were detected in catalysts 2 and 3, while both Pd subnano-clusters and Pd nanoparticles (>1 nm) were observed in catalysts 4 and 5 (Table 1). The size distributions of Pd subnano-clusters/nanoparticles in all cases were evaluated, and the results are shown with red-colored bars in the fourth column of Figure 2b-e and in Table 1. As can be seen in Figure 2 and Table 1, the average size of Pd subnano-clusters/nanoparticles ( $d_{av, Pd}$ ) increased from  $0.51 \pm 0.12$  nm to  $1.04 \pm 0.18$  nm with increasing Pd loading (catalyst 2 to 5), which clearly demonstrates that Pd loading affects the size of Pd subnano-clusters/nanoparticles on the TiO<sub>2</sub> surface. Based on this trend, the size of Pd subnano-clusters in catalyst 1 can be assumed to be less than 0.5 nm.

In the case of the treated catalysts, the average particle sizes of Pd-TiO<sub>2</sub> were slightly increased to approximately 9 nm with the Pd loading was increased, as can be seen in the first column of Figure 2b-e (blue-colored bars). Based on this result, it can be noted that the sintering of the Pd-TiO<sub>2</sub> was not severe at the high temperature condition. Compared to the fresh catalysts showing very small Pd subnano-clusters and nanoparticles less than 1.5 nm, the treated catalysts showed larger nanoparticles and their average sizes were increased as the Pd loading was increased:  $1.17 \pm 0.26$  nm for the treated catalyst 2,  $1.41 \pm 0.28$  nm for the treated catalyst 3, and  $2.27 \pm 0.26$  nm for the treated catalyst 4, respectively. Previous studies have reported the increased size of dopants on the support materials at the high temperature condition due to the sintering of them,<sup>29,36</sup> and our observation showed a similar trend. It is interesting to note that the treated catalyst 5 contains aggregates of Pd nanoparticles on the TiO<sub>2</sub> surface as well as the larger Pd nanoparticles. It has been known that the morphology of the nanoparticle can be affected by both the time for particle-particle collisions and the time for inter-particle coalescence (i.e. sintering).<sup>37</sup> When the time for particle-particle collisions is larger than the time for sintering, the particle coalesces before it collides with another particle, which results in the larger spherical particle. In the opposite case (the time for particle-particle collisions is smaller than the time for sintering), the particle collides with another particle before it coalesces, which causes the aggregates of the particles.<sup>37</sup> In this study, with the largest Pd loading (catalyst 5), the Pd nanoparticles could have more opportunity to collide with other Pd nanoparticles on the TiO<sub>2</sub> surface. Thereby, the time for colliding can be smaller than the time for sintering, resulting in the aggregates of Pd nanoparticles on the TiO<sub>2</sub> surface as can be seen in the third column of Figure 2e. It is also worth noting that the morphology of the TiO<sub>2</sub> was changed to the porous structure, which might be due to the creation of the aggregates of Pd nanoparticles on it.

### 3.1.4 Distinguishing oxidation states of components in fresh and treated catalysts (XPS)

To investigate the effect of different Pd loadings on the Pd species in the synthesized Pd-TiO<sub>2</sub> catalysts, the Pd oxidation state in the fresh catalysts was evaluated by XPS, with the results shown in the left column

of Figure 3 and summarized in Table 2. Three Pd species were identified based on different characteristic Pd 3d<sub>5/2</sub> core level binding energies: metallic Pd (335.7 eV), intermediate PdO<sub>x</sub> (0 < x < 1) (336.42 eV), and PdO (337.4 eV).<sup>29</sup> As can be seen in Figure 3 and Table 2, the XPS spectra confirm that all the Pd-TiO<sub>2</sub> catalysts contained three Pd species, but the percentages of the three Pd species changed as the Pd loading changed. The amount of metallic Pd increased from 33.34 ± 1.23% to 42.32 ± 4.01% as Pd loading was increased from 0.24 wt% to 0.76 wt% (catalyst 1 to catalyst 3). The amount of metallic Pd decreased to 35.78 ± 2.89% as Pd loading was further increased to 1.25 wt% (catalyst 5). On the other hand, the amounts of intermediate PdO<sub>x</sub> and PdO showed opposite trends to that of metallic Pd. As mentioned earlier in 3.1., the extent of the oxidation of Pd could be varied with different Pd loadings at the same flame-synthesizing condition. The results with the fresh catalysts here are in line with this hypothesis. To study the change in the Pd species at the high temperature under the same experimental condition, the Pd oxidation state in the treated catalysts was also characterized by XPS, and the results are shown in the right column of Figure 3 and Table S1. As shown in Figure 3, the treated catalysts also contained three Pd species, i.e. metallic Pd, PdO and PdO<sub>x</sub>. Compared to the fresh catalysts, the proportions of metallic Pd and PdO<sub>x</sub> were increased, while the percentage of PdO was decreased as the Pd loading was increased (Table S1). Previous studies revealed that the Pd<sup>2+</sup> was reduced into Pd<sup>0</sup> and/or Pd<sup>+</sup> at the high temperature during methane oxidation reaction.<sup>23,29</sup> Our analytical results were consistent with these previous findings.

Furthermore, the changes in other species, Ti and O, were evaluated by XPS for both the fresh and the treated catalysts, and the results are shown in Figure S2, S3, Table S2, and Table S3. The Ti 2p spectra in both fresh and treated catalysts were deconvoluted into four peaks at approximately 456.7 eV, 458.5 eV, 460.3 eV, and 464.2 eV, which are denoted as Ti<sup>3+</sup>(2p<sub>3/2</sub>), Ti<sup>4+</sup>(2p<sub>3/2</sub>), Ti<sup>3+</sup>(2p<sub>1/2</sub>), and Ti<sup>4+</sup>(2p<sub>1/2</sub>).<sup>38,39</sup> This observation implies that Ti in both fresh and treated catalysts was mainly in TiO<sub>2</sub> phase, and the small amount of Ti was in Ti<sub>2</sub>O<sub>3</sub> (Ti<sup>3+</sup>) phase. Compared to the fresh catalysts, an increasing amount of Ti<sup>3+</sup> was obtained. In addition, the percentage of Ti<sup>3+</sup> was slightly decreased as the Pd loading was increased. These findings demonstrated the slight phase transformation of TiO<sub>2</sub> toward Ti<sub>2</sub>O<sub>3</sub> and the suppressing effect of Pd on the phase transformation, which were matched with the XRD results in 3.1.2. It should be noted that the intensity of Ti was not different much among samples. For comparison, the XPS spectra of O is in both fresh and treated catalysts are shown in Figure S3 and Table S3. The XPS spectra of both fresh and treated catalysts showed three noticeable peaks, at approximately 529.9 eV, 531.3 eV, and 532.2 eV, which can be assigned respectively to (1) lattice oxygens in a fully-coordinated environment with metal ions (O<sub>lattice</sub>), (2) oxygen deficient regions of the metal oxide (O<sub>deficient region</sub>), and (3) adsorbed oxygen species, such as O<sub>2</sub>, H<sub>2</sub>O, or M(metal)-OH on the surface,<sup>40</sup> which might be produced during the catalyst synthesis process. We can term these species intrinsically adsorbed oxygen, or O<sub>adsorbed</sub>. As can be seen Figure S3, there was no significant change in O<sub>lattice</sub> in the fresh and treated catalysts. On the other hand, an increasing amount of O<sub>deficient region</sub> and a decreasing amount of O<sub>adsorbed</sub>, which indicates the desorption of the adsorbed oxygen species at high temperature and the reduction of Ti and/or Pd.

In the previous sections and this section, it was confirmed that (1) most Pd was deposited on the TiO<sub>2</sub> surface, (2) size of Pd-TiO<sub>2</sub> was not changed much, and (3) the intensity of Ti was not different much among fresh and treated catalysts. Based on these results, the dispersion or sintering of Pd on the TiO<sub>2</sub> surface can be determined by comparing the ratio between the intensity of Pd 3d (I(Pd)) and Ti 2p (I(Ti)) in fresh and treated catalysts. The ratios were calculated, and they were compared by obtaining ( $\frac{Treated(\frac{I(Pd)}{I(Ti)})}{Fresh(\frac{I(Pd)}{I(Ti)})}$ ) (Table S1). The calculated values were decreased as the Pd loading was increased, which could imply the decreased Pd coverage on the TiO<sub>2</sub> surface due to sintering of Pd. This is consistent with our STEM and XRD results showing the increasing size of Pd.

### 3.1.5 Total surface area of different Pd species

Based on the  $M_{Total\ Pd}$  (Table 1) and XPS analytical results, the masses of metallic Pd ( $M_{metallic\ Pd}$ ), PdO ( $M_{PdO}$ ) and intermediate PdO<sub>x</sub> ( $M_{PdO_x}$ ) were calculated by

$$M_{\text{metallic Pd}} (\mu\text{g}) = M_{\text{Total Pd}} \times \frac{\text{Metallic Pd} (\%)}{100}, \quad (1)$$

$$M_{\text{PdO}} (\mu\text{g}) = M_{\text{Total Pd}} \times \frac{\text{PdO} (\%)}{100} \times \frac{\text{MW}_{\text{PdO}}}{\text{MW}_{\text{Pd}}}, \quad (2)$$

$$M_{\text{PdO}_x} (\mu\text{g}) = M_{\text{Total Pd}} \times \frac{\text{PdO}_x (\%)}{100} \times \frac{\text{MW}_{\text{PdO}_x}}{\text{MW}_{\text{Pd}}}, \quad (3)$$

where  $\text{MW}_{\text{Pd}}$ ,  $\text{MW}_{\text{PdO}}$  and  $\text{MW}_{\text{PdO}_x}$  represent the molar weights of Pd, PdO and  $\text{PdO}_x$ , respectively. It should be noted that most Pd subnano-clusters/nanoparticles were distributed on the catalyst's surface, which was demonstrated by ICP-MS and FESEM-EDS. Therefore, XPS analytical results could be combined here to calculate the masses of different Pd phases.  $\text{MW}_{\text{PdO}_x}$  was assumed to be an average of  $\text{MW}_{\text{Pd}}$  and  $\text{MW}_{\text{PdO}}$ . The calculated values based on the fresh catalysts are summarized in Table 2, where it can be seen that the mass of each Pd species does not depend on the fraction of Pd species, but instead depends on the Pd loading.  $M_{\text{metallic Pd}}$ ,  $M_{\text{PdO}}$  and  $M_{\text{PdO}_x}$  increased from 8.00  $\mu\text{g}$ , 9.06  $\mu\text{g}$  and 8.72  $\mu\text{g}$ , to 44.81  $\mu\text{g}$ , 36.39  $\mu\text{g}$  and 52.46  $\mu\text{g}$  with increasing Pd loading (catalyst 1 to 5). The total surface area (TSA) of each Pd species was further calculated based on

$$M (\mu\text{g}) = N \times \frac{\pi}{6} \times d^3 \times \rho, \quad (4)$$

$$\text{TSA} (\text{cm}^2) = \frac{6M}{\rho d} = N \times \pi \times d^2, \quad (5)$$

where  $N$ ,  $d$ , and  $\rho$  represent the number, diameter, and density of each Pd species, respectively. For the calculation, the Pd species were assumed to have the same size and spherical shape of Pd subnano-clusters/nanoparticles, and an average density of metallic Pd and PdO was used for the density of  $\text{PdO}_x$ . Because of different masses and densities of the three different Pd species, different volumes and areas of them were expected. The calculated values are summarized in Table 2. It is worth noting that the TSA values of metallic Pd, PdO and  $\text{PdO}_x$  show different trends.  $\text{TSA}_{\text{metallic Pd}}$  increases with increasing Pd loading (catalyst 2 to 3) and reaches the largest value of 245.56  $\text{cm}^2$ . Then, it decreases as the Pd loading is further increased (catalyst 3 to 5). In the case of  $\text{TSA}_{\text{PdO}}$ , a similar trend is found, but the peak value of 296.35  $\text{cm}^2$  is found with catalyst 4. The  $\text{TSA}_{\text{PdO}_x}$  increases with increasing Pd loading (catalyst 2 to 5) and reaches its largest value of 299.68  $\text{cm}^2$  with the highest Pd loading (catalyst 5). However, for any Pd phase (metallic Pd, PdO and  $\text{PdO}_x$ ), the sample-by-sample TSA dependence exhibits the same trend as the percentage of this phase. In the case of the treated catalysts, the comparison was done among catalysts 2, 3 and 4, and the results are shown in Table S1. According to STEM analytical results, there were aggregates of Pd nanoparticles in the treated catalyst 5, and thereby the calculation based on the spherical shape of primary Pd particles could not be applied. As can be seen Table S1,  $\text{TSA}_{\text{metallic Pd}}$  of the treated catalysts followed a similar trend to  $\text{TSA}_{\text{metallic Pd}}$  of the fresh catalysts:  $\text{TSA}_{\text{metallic Pd}}$  was increased from 85.68  $\text{cm}^2$  to 124.70  $\text{cm}^2$  as the Pd loading was increased (catalyst 2 to 3), and then it was decreased to 105.61  $\text{cm}^2$  as the Pd loading was further increased (catalyst 3 to 4). On the other hand, unlike the fresh catalysts,  $\text{TSA}_{\text{PdO}}$  and  $\text{TSA}_{\text{PdO}_x}$  of the treated catalysts show a similar trend to  $\text{TSA}_{\text{metallic Pd}}$  of the treated catalysts: Both were increased to 70.78  $\text{cm}^2$  and 131.74  $\text{cm}^2$  as the Pd loading was increased from catalyst 2 to catalyst 3, and further decreased to 64.75  $\text{cm}^2$  and 120.12  $\text{cm}^2$  as the Pd loading was increased to catalyst 4. It should be noted that all TSA of the treated catalysts were smaller than those of the fresh catalysts because Pd subnano-clusters/nanoparticles were sintered on the  $\text{TiO}_2$  surfaces at the high temperature. The TSA of metal could play a crucial role in the catalytic activity by providing active sites for the reaction, and thus higher catalytic activity is expected with the larger TSA of metal. Because the TSA of all Pd species showed different trends, the important Pd species on the catalytic activity in  $\text{O}_2$  removal could be demonstrated, which is discussed in the following section.

### 3.2. Catalytic activity of the synthesized Pd-TiO<sub>2</sub> catalysts in O<sub>2</sub> removal

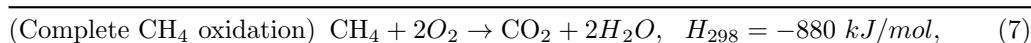
#### 3.2.1 Catalytic activity evaluation in O<sub>2</sub> removal

The synthesized Pd-TiO<sub>2</sub> catalysts were evaluated for O<sub>2</sub> removal. The experiments were conducted under initial O<sub>2</sub> rich composition (O<sub>2</sub>/CH<sub>4</sub>  $\cong$  2.4), with excessive CO<sub>2</sub> as the balance of the gas. The experiments under other initial conditions are shown in the following section, 3.2.3. The O<sub>2</sub> and CH<sub>4</sub> conversions were calculated based on:

$$\text{Conversion (\%)} = \frac{C_i - C_f}{C_i} \times 100, \quad (6)$$

where  $C_i$  and  $C_f$  represent the initial and final concentrations of gas, respectively. Data on “conversion-temperature” dependencies are presented in Figure 4 and Table 3.

Our system consisted of six gaseous substances (CH<sub>4</sub>, O<sub>2</sub>, CO, H<sub>2</sub>O, H<sub>2</sub> and CO<sub>2</sub>) of three elements (C, H, O). Generally, three independent overall reactions are possible (6 substances – 3 elements = 3 independent overall reactions):



All reactants and products were analyzed by using a GC. As can be seen in Figure 4a,b and Table 3, the concentrations of both O<sub>2</sub> and CH<sub>4</sub> decreased as the temperature was increased. CO<sub>2</sub> gas was detected, but in our typical experiment the CO<sub>2</sub> concentration was comparatively high, and its change was hard to monitor. On the other hand, there was no CO observed. In addition, the dry reforming reaction is highly endothermic and requires considerable external energy. The low temperature ([?]773 K) applied to our experimental system may not favor this reaction. Therefore, the partial CH<sub>4</sub> oxidation (Eq. 8) and dry reforming of CH<sub>4</sub> (Eq. 9) reactions can be ruled out. It is worth noting that there is no H<sub>2</sub> observed and thereby, water-gas shift reaction ( $\text{CO} + \text{H}_2\text{O} \rightarrow \text{CO}_2 + \text{H}_2$ ) in the system is negligible.

To confirm the generation of CO<sub>2</sub> as a product via reaction (7), a separate experiment was performed with He gas as the balance of the gas instead of CO<sub>2</sub>, with the results shown in Figure S4. Decreasing trends were found in the O<sub>2</sub> and CH<sub>4</sub> concentrations. Only CO<sub>2</sub> (no CO) was clearly observed as a product, and the total concentration of C remained constant during the reaction. Furthermore, the reaction rate of CH<sub>4</sub> is half the reaction rate of O<sub>2</sub> via reaction (7) ( $R_{\text{CH}_4} = \frac{1}{2}R_{\text{O}_2}$ ). The reaction rate of both CH<sub>4</sub> and O<sub>2</sub> at 723 K and 773 K were summarized in Table S4. Table S4 indicates stoichiometry: the reaction rates of CH<sub>4</sub> are close to the half of reaction rates of O<sub>2</sub> at both 723 K and 773 K ( $\left| \frac{R_{\text{CH}_4} - 1/2 R_{\text{O}_2}}{R_{\text{CH}_4}} \right| \times 100 \leq 6 \%$ ). Therefore, complete CH<sub>4</sub> oxidation (Eq. 7) was the single overall reaction in this system. All catalysts showed the same trends of reactant and product concentrations.

Figure 4 and Table 3 show an enhanced O<sub>2</sub> and CH<sub>4</sub> conversions with Pd-TiO<sub>2</sub> catalysts compared to those with only TiO<sub>2</sub> (~30.9% for O<sub>2</sub>, and ~50.7% for CH<sub>4</sub> at 723 K). This result emphasizes the importance of Pd in effective O<sub>2</sub> removal. In addition, O<sub>2</sub> conversion increased from 55.8% to 77.0% at 723 K with increasing Pd loading (catalyst 1 to 3). However, it decreased when the Pd loading was further increased (catalyst 3 to 5). CH<sub>4</sub> conversion was enhanced from 64.4% to 92.4% as Pd loading was increased (catalyst 1 to 3), and then no significant difference was observed as Pd loading was further increased.

### 3.2.2 Apparent reaction rate constant and total surface area of Pd species

Our preliminary experiments at different temperatures proved that the O<sub>2</sub> removal reaction with Pd-TiO<sub>2</sub> catalysts followed an apparent first order reaction (Figure S5): the natural log of  $C_f/C_i$  plotted versus residence time (min) demonstrates a linear trend ( $R^2 > 0.92$ ) at different temperatures. Therefore, the apparent reaction rate constant ( $k_{\text{app}}$ ) can be determined by



$$\frac{\delta \bar{r}}{\delta \tau} = -k_{app}C, \quad (10)$$

where  $C$  and  $\tau$  represent the concentration of  $O_2$  and residence time (min). The calculated  $k_{app}$  values at 723 K are summarized in Table 3. It should be noted that when the plot of  $k_{app}$  and the total Pd loading was expressed (Figure 5a), an optimal total Pd loading was observed. Because different Pd species (metallic Pd, PdO and PdO<sub>x</sub>) could be involved in the  $O_2$  removal reaction, the relationship between  $k_{app}$  and total Pd loading might not be sufficient to understand the active phase of Pd for the reaction. To reveal the active phase of Pd which is responsible for the catalytic activity, it is necessary to distinguish the contributions of different Pd species on the  $O_2$  removal reaction. Also, it must be understood the change in the catalytic properties during the reaction and corresponding catalytic activity. In the interpretation of kinetic data, the hypothesis of additivity can be formulated. In accordance with this hypothesis, the reaction occurs on different Pd phases (i.e., metallic Pd, PdO and PdO<sub>x</sub>). Previously, Kannisto et al. and Murzin<sup>41,42</sup> analyzed contributions of different geometric sites into the whole catalytic activity. Similar to their additive approach,  $k_{app}$  can be presented as a sum of different contributions:

$$k_{app} = k_{app, metallic Pd} \alpha + k_{app, PdO} \beta + k_{app, PdO_x} \gamma, \quad (11)$$

$$\alpha = \frac{TSA_{metallic Pd}}{TSA_{total}}, \beta = \frac{TSA_{PdO}}{TSA_{total}}, \gamma = \frac{TSA_{PdO_x}}{TSA_{total}}, \quad (12)$$

$$\alpha + \beta + \gamma = 1, \quad (13)$$

where  $k_{app, metallic Pd}$ ,  $k_{app, PdO}$  and  $k_{app, PdO_x}$  represent the apparent reaction rate constants on metallic Pd, PdO and PdO<sub>x</sub>, respectively. The obtained  $k_{app}$  is presented as a function of fractions of the total surface area of each Pd species ( $\alpha$ ,  $\beta$  and  $\gamma$ ). In this study, three different types of  $\alpha$ ,  $\beta$  and  $\gamma$  were obtained based on the analytical results of (1) fresh and (2) treated catalysts, and (3) averages of them:  $\alpha_{fresh}$ ,  $\beta_{fresh}$  and  $\gamma_{fresh}$  represent the fraction of the total surface area of metallic Pd, PdO and PdO<sub>x</sub>, respectively, and those in the treated catalysts were denoted as  $\alpha_{treated}$ ,  $\beta_{treated}$  and  $\gamma_{treated}$ , respectively. In addition,  $\alpha_{avg}$ ,  $\beta_{avg}$  and  $\gamma_{avg}$  were obtained by averaging the analytical results of fresh and treated catalysts. The relationships between the calculated  $k_{app}$  and  $\alpha$ ,  $\beta$  and  $\gamma$  were further investigated: The plots of  $k_{app}$  and fractions in the fresh catalysts ( $\alpha_{fresh}$ ,  $\beta_{fresh}$  and  $\gamma_{fresh}$ ) were expressed with temperatures near at which the catalytic activity was initiated. The plots of  $k_{app}$  and fractions in the treated catalysts ( $\alpha_{treated}$ ,  $\beta_{treated}$  and  $\gamma_{treated}$ ) were displayed with the high temperatures. The moderate temperatures were used for the plots of  $k_{app}$  and average fractions ( $\alpha_{avg}$ ,  $\beta_{avg}$  and  $\gamma_{avg}$ ) as well. In the case of the fresh catalysts, a linear increase was observed with  $k_{app}$  and  $\alpha_{fresh}$  (metallic Pd) ( $R^2 > 0.91$ ) (Figure 5b), while as for the dependencies between  $k_{app}$  and  $\beta_{fresh}$  (PdO) and between  $k_{app}$  and  $\gamma_{fresh}$  (PdO<sub>x</sub>), no correlation was found (Figure S6a,b). Therefore, it can be concluded that for the fresh catalysts, the apparent catalytic activity is governed by metallic Pd and the contribution of Pd oxides is insignificant.

In the cases of the treated catalysts and the averaged values, like the plot of  $k_{app}$  and  $\alpha_{fresh}$  (metallic Pd),  $k_{app}$  was generally linearly increased as both  $\alpha_{treated}$  and  $\alpha_{avg}$  were increased with  $R^2 > 0.85$  and  $R^2 > 0.90$ , respectively (Figure 5c,d). No correlations between  $k_{app}$  and  $\gamma_{treated}$  (PdO<sub>x</sub>) and between  $k_{app}$  and  $\gamma_{avg}$  were observed (Figure S7a,b). It is interesting to note that unlike the plot of  $k_{app}$  and  $\beta_{fresh}$  (PdO),  $k_{app}$  was linearly decreased as both  $\beta_{treated}$  and  $\beta_{avg}$  were increased (Figure S8a,b). These results could indicate the metallic Pd is the active catalytic phase. However, it is risky to conclude that only metallic Pd plays a crucial role in the reaction. The catalysts generally go through a complex process during the reaction in which Pd oxides are partially reduced to metallic Pd or/and PdO<sub>x</sub> ( $0 < x < 1$ ) species, experimentally distinguished (see previous section 3.1.4). The calculated  $k_{app}$  exhibited the linear dependence regarding the combined fractions of the total surface area of metallic Pd and PdO<sub>x</sub> ( $\alpha_{treated} + \gamma_{treated}$ ) (Figure S9). The previous study by Yang et al.<sup>23</sup> reported the reduced form of Pd (Pd<sup>0</sup> and PdO<sub>x</sub> ( $0 < x < 1$ )) was preferential for the effective methane oxidation reaction. A theoretical study by using density functional theory (DFT) calculations also revealed the lower activation energy barrier for methane decomposition, which is widely accepted as the reaction rate limiting step, on the reduced PdO surface.<sup>43</sup> Therefore, it could be concluded that metallic

Pd mainly controls the  $O_2$  removal reaction and the reduced Pd phase, metallic Pd or/and  $PdO_x$ , at high temperature also generates an active phase for the reaction. Our interpretation of results of physico-chemical analysis and kinetic studies, showing the volcano-shaped dependencies (Figure 5a), emphasizes that the Pd loading itself does not affect the intrinsic catalytic property of the synthesized catalyst, but the fraction of active Pd phases, which are metallic Pd or/and reduced Pd ( $PdO_x$ ), significantly determines it. Behind the volcano-shaped dependencies, a linear dependency between the  $k_{app}$  and the fraction of the total surface area of active Pd phases (metallic Pd or/and reduced form of Pd) results in the constant catalytic activity per unit area of metallic Pd or/and reduced form of Pd. It means that we observe the case of so-called structure insensitive catalytic system defined by Boudart.<sup>44</sup> For such systems, the catalytic activity per unit of area is related to the specific active component and does not depend on the preparation method providing a guidance for the catalyst design.<sup>44-46</sup>

### 3.2.3 Influence of reactants and products: Autocatalytic effect; other reactions

The previous experiments were conducted under  $O_2$  rich composition ( $O_2/CH_4 \cong 2.4$ ). In this section, two different initial compositions were considered: first, different  $CO_2$  concentrations (0% and 53%, He as the balance of the gas) under  $O_2$  rich composition in the initial gas stream were applied. Second, different ratios between  $O_2$  and  $CH_4$  concentrations (i.e., stoichiometric composition:  $O_2/CH_4 \cong 2.0$  and  $O_2$  lean composition:  $O_2/CH_4 \cong 1.6$  with excessive  $CO_2$  as the balance of the gas) were tested.

To investigate the effect of  $CO_2$  concentration in the initial gas stream on the  $O_2$  removal (first initial composition), experiments with different  $CO_2$  concentrations (i.e., 0% and 53%, He as the balance of the gas) under  $O_2$  rich composition were conducted, and their results and the previous result with 95% of  $CO_2$  are shown in Figure 6. Complete  $CH_4$  oxidation (Eq. 7) was the main reaction between  $CH_4$  and  $O_2$ , which was proved by the closed values between the reaction rates of  $CH_4$  and the half of reaction rates of  $O_2$  (Table S5). On the other hand, it should be noted that both  $O_2$  and  $CH_4$  conversions were enhanced as the  $CO_2$  concentration was increased. To clearly see the correlation between the reaction rate and the initial  $CO_2$  concentration, the  $O_2$  reaction rate versus the initial  $CO_2$  concentration was plotted in Figure S10. As can be seen in Figure S10, the  $O_2$  reaction rate was proportional to the initial  $CO_2$  concentration: the  $O_2$  conversion rate (mmol/g<sub>cat</sub>/hr) versus the concentration of initial  $CO_2$  (mol/m<sup>3</sup>) at different temperatures could be approximately explained by a linear dependence ( $R^2 > 0.88$ ). It can be defined as an autocatalytic effect. In accordance with our knowledge, this effect can be shown by the linear correlation between the reaction rate and the concentration of product.<sup>47</sup> Previously, the autocatalytic effect on different applications has been reported and the accelerated reaction rates were mostly supported by the lower activation barriers via new intermediates.<sup>48,49</sup> Therefore, it could be concluded that  $CO_2$  is itself involved in the  $O_2$  removal reaction. The process may occur via  $CO_2$ -containing intermediates and the reaction rate is enhanced as the autocatalytic reaction. It is possible that the application of DFT calculations will be useful for understanding this effect.

Results under second initial composition were compared with the previous one which was performed under  $O_2$  rich composition with excessive  $CO_2$  as the balance of the gas (95%) in Figure 7. Figure 7 demonstrates: as the ratio between  $O_2$  and  $CH_4$  was decreased from the  $O_2$  rich composition to the  $O_2$  lean one, the conversion of  $O_2$  was increased. For example, the  $O_2$  conversion was increased from 77% to 88% at 723 K, while the  $CH_4$  conversion was decreased from 92% to 69%. This result indicates that more reaction source ( $CH_4$ ) can enhance the  $O_2$  conversion. It should be also noted that there was a sharp increase in the  $CH_4$  conversion at around 723 K under  $O_2$  lean condition (Figure 7b). This sudden increase in the  $CH_4$  conversion could be due to the dry reforming of  $CH_4$  reaction (Eq. 9). It can be supported by Figure 8, which shows: at high temperature ( $> 723$  K), CO generates under only  $O_2$  lean composition. It can be also shown by the reaction rates of  $CH_4$ ,  $O_2$ , and CO which were summarized in Table S6. Via both complete  $CH_4$  oxidation reaction (Eq. 7) and dry reforming of  $CH_4$  reaction (Eq. 9), the reaction rate of  $CH_4$  is the same as the difference between the half of the reaction rate of  $O_2$  and the half of the reaction rate of CO. Table S6 demonstrates that there was both complete  $CH_4$  oxidation reaction and dry reforming of  $CH_4$  under  $O_2$  lean composition at 773 K. A previous study reported the same trend which shows the decreasing  $CO_2$  selectivity

due to the formation of CO under  $O_2$  lean composition  $O_2/CH_4 \cong 1.5$  and 1.75).<sup>16</sup> This experimental result implies that the excessive  $CH_4$  could cause a nonpreferred reaction by reacting with  $CO_2$  to generate CO.

#### 4. Conclusions

Pd-TiO<sub>2</sub> catalysts with varying Pd loading (0.24 wt% - 1.25 wt%) were synthesized by using a flame aerosol reactor, and the material and kinetic characteristics of the fresh catalysts and the treated catalysts at high temperature under the same experimental conditions were evaluated. Our study contributes to three major findings:

(1) In the case of the fresh catalysts, the addition of Pd did not change the crystal structure of the base TiO<sub>2</sub>, and the size of the Pd-TiO<sub>2</sub> particle did not change with different Pd loadings, but the size of Pd subnanoclusters/nanoparticles and the oxidation state of Pd (metallic Pd, PdO and PdO<sub>x</sub>) was significantly affected by Pd loading. In the case of the treated catalysts, small change in the phase of TiO<sub>2</sub> from anatase TiO<sub>2</sub> to both rutile TiO<sub>2</sub> and Ti<sub>2</sub>O<sub>3</sub> was observed, but the phase transformation was suppressed with increasing of the Pd loading. Two major changes in Pd on the catalyst's surface were observed: First, increased size of Pd nanoparticles on the catalyst's surface was observed due to the sintering effect. With the highest Pd loading, aggregates of Pd nanoparticles on the catalyst's surface were obtained. Second, some amount of PdO was reduced to either metallic Pd or intermediate PdO<sub>x</sub>.

(2) The total surface areas of different Pd species in the fresh and treated catalysts were evaluated based on the size distribution of Pd and fractions of Pd species. For the fresh catalysts, the apparent reaction rate constants were proportional to the calculated fraction of the total surface area (TSA) of metallic Pd. For the treated catalysts, a linear correlation between the apparent reaction rate constants and the combined fraction of TSA (metallic Pd and reduced Pd oxide, i.e. PdO<sub>x</sub> (0 < x < 1)) was obtained as well. Different catalytic characteristics on Pd loading, i.e. the total surface area of metallic Pd, conversion of O<sub>2</sub> and apparent reaction rate constants, exhibit the volcano-shaped dependencies. However, behind these dependencies, a linear proportionality between apparent kinetic constants and fractions of total surface areas of metallic Pd or/and reduced Pd oxide is revealed using distinguishing different Pd phases, which represents the intrinsic activity of the active site.

(3) Two different initial conditions (i.e., different ratios between O<sub>2</sub> and CH<sub>4</sub> concentrations and different CO<sub>2</sub> concentrations) were tested and revealed CO generation at high temperature under O<sub>2</sub> lean condition. In addition, the reaction rate of O<sub>2</sub> had a linear dependency on the initial CO<sub>2</sub> concentration, which was indicated by an autocatalytic reaction effect.

This study provides structural and kinetic investigation on O<sub>2</sub> removal with flame-synthesized Pd-TiO<sub>2</sub> catalysts and emphasizes the kinetic role of metallic Pd and reduced Pd oxide, i.e. PdO<sub>x</sub> (0 < x < 1). This study also proposed a positive effect of initial CO<sub>2</sub> concentration on O<sub>2</sub> removal via an autocatalytic reaction effect. Detailed role of dry reforming reaction under different initial conditions and autocatalytic reaction effect on O<sub>2</sub> removal will be addressed in our further study.

#### Acknowledgements

This work was supported by a grant funded by the U.S. Department of Energy's National Energy Technology Laboratory under Award Number DE-FE0029161.

#### References

1. Buhre BJP, Elliott LK, Sheng CD, Gupta RP, Wall TF. Oxy-fuel combustion technology for coal-fired power generation. *Prog. Energy Combust. Sci.* 2005;31(4):283-307.
2. Jordal K, Anheden M, Yan J, Strömberg L. Oxyfuel combustion for coal-fired power generation with CO<sub>2</sub> capture-opportunities and challenges. *Greenhouse Gas Control Technologies.* 2005;7:201-209.
3. U.S. Energy Information Administration. What is U.S. electricity generation by energy source? 2018; <https://www.eia.gov/tools/faqs/faq.php?id=427&t=3>.

4. U.S. Energy Information Administration. U.S. Energy-related carbon dioxide emissions, 2018. 2019; <https://www.eia.gov/environment/emissions/carbon/>.
5. Gopan A, Kumfer BM, Phillips J, Thimsen D, Smith R, Axelbaum RL. Process design and performance analysis of a Staged, Pressurized Oxy-Combustion (SPOC) power plant for carbon capture. *Appl. Energ.* 2014;125:179-188.
6. Kanniche M, Gros-Bonnivard R, Jaud P, Valle-Marcos J, Amann JM, Bouallou C. Pre-combustion, post-combustion and oxy-combustion in thermal power plant for CO<sub>2</sub> capture. *Appl. Therm. Eng.* 2010;30(1):53-62.
7. Chu S. Carbon capture and sequestration. *Science* 2009;325(5948):1599-1599.
8. Dai Z, Middleton R, Viswanathan H, Fessenden-Rahn J, Bauman J, Pawar R, Lee SY, McPherson B. An integrated framework for optimizing CO<sub>2</sub> Sequestration and enhanced oil recovery. *Environ. Sci. Technol. Lett* 2014;1(1):49-54.
9. DOE/NETL. Quality guidelines for energy system studies: CO<sub>2</sub> impurity design parameters. 2013.
10. Enger BC, Lødeng R, Holmen A. A review of catalytic partial oxidation of methane to synthesis gas with emphasis on reaction mechanisms over transition metal catalysts. *Appl. Catal. A* 2008;346(1-2):1-27.
11. Gélin P, Primet M. Complete oxidation of methane at low temperature over noble metal based catalysts: a review. *Appl. Catal. B* 2002;39(1):1-37.
12. Hoflund GB, Li Z, Epling WS, Göbel T, Schneider P, Hahn H. Catalytic methane oxidation over Pd supported on nanocrystalline and polycrystalline TiO<sub>2</sub>, Mn<sub>3</sub>O<sub>4</sub>, CeO<sub>2</sub> and ZrO<sub>2</sub>. *React. Kinet. Catal. Lett* 2000;70(1):97-103.
13. Osman AI, Abu-Dahrieh JK, Laffir F, Curtin T, Thompson JM, Rooney DW. A bimetallic catalyst on a dual component support for low temperature total methane oxidation. *Appl. Catal. B* 2016;187:408-418.
14. Muto K, Katada N, Niwa M. Complete oxidation of methane on supported palladium catalyst: Support effect. *Appl. Catal. A* 1996;134(2):203-215.
15. Zheng Q, Zhou S, Lail M, Amato K. Oxygen removal from oxy-combustion flue gas for CO<sub>2</sub> purification via catalytic methane oxidation. *Ind. Eng. Chem. Res.* 2018;57(6):1954-1960.
16. Kuhn AN, Chen Z, Lu Y, Yang H. Sequential oxygen reduction and adsorption for carbon dioxide purification for flue gas applications. *Energy Technol.* 2019;7(4):1800917.
17. Cullis CF, Willatt BM. Oxidation of methane over supported precious metal catalysts. *J. Catal.* 1983;83(2):267-285.
18. Fujimoto K, Ribeiro FH, Avalos-Borja M, Iglesia E. Structure and reactivity of PdO<sub>x</sub>/ZrO<sub>2</sub> catalysts for methane oxidation at low temperatures. *J. Catal.* 1998;179(2):431-442.
19. Schmal M, Souza MMVM, Alegre VV, da Silva MAP, César DV, Perez CAC. Methane oxidation - effect of support, precursor and pretreatment conditions - in situ reaction XPS and DRIFT. *Catal. Today*. 2006;118(3-4):392-401.
20. Weng X, Ren H, Chen M, Wan H. Effect of surface oxygen on the activation of methane on palladium and platinum surfaces. *ACS Catal.* 2014;4:2598-2604.
21. Singh J, Nachtegaal M, Alayon EMC, Stötzel J, van Bokhoven JA. Dynamic structure changes of a heterogeneous catalyst within a reactor: Oscillations in CO Oxidation over a supported platinum catalyst. *ChemCatChem* 2010;2(6):653-657.
22. Makeev AG, Slinko MM, Luss D. Mathematical modeling of oscillating CO oxidation on Pt-group metals at near atmospheric pressure: Activity of metallic and oxidized surfaces. *Appl. Catal. A* 2019;571:127-136.

23. Yang S, Maroto-Valiente A, Benito-Gonzalez M, Rodriguez-Ramos I, Guerrero-Ruiz A. Methane combustion over supported palladium catalysts I. Reactivity and active phase. *Appl. Catal. B* 2000;28(3-4):223-233.
24. Ortloff F, Bohnau J, Graf F, Kolb T. Removal of oxygen from (bio-)methane via catalytic oxidation of CH<sub>4</sub>-Reaction kinetics for very low O<sub>2</sub>:CH<sub>4</sub> ratios. *Appl. Catal. B* 2016;182:375-384.
25. Wang ZM, Yang G, Biswas P, Bresser W, Boolchand P. Processing of iron-doped titania powders in flame aerosol reactors. *Powder Technol.* 2001;114(1-3):197-204.
26. Tiwari V, Jiang J, Sethi V, Biswas P. One-step synthesis of noble metal-titanium dioxide nanocomposites in a flame aerosol reactor. *Appl. Catal. A* 2008;345(2):241-246.
27. Dhumal SY, Daulton TL, Jiang J, Khomami B, Biswas P. Synthesis of visible light-active nanostructured TiO<sub>x</sub> (x < 2) photocatalysts in a flame aerosol reactor. *Appl. Catal. B* 2009;86(3-4):145-151.
28. Strobel R, Pratsinis SE. Flame aerosol synthesis of smart nanostructured materials. *J. Mater. Chem.* 2007;17(45):4743-4756.
29. Niu F, Li S, Zong Y, Yao Q. Catalytic behavior of flame-made Pd/TiO<sub>2</sub> nanoparticles in methane oxidation at low temperatures. *J. Phys. Chem. C*. 2014;118(33):19165-19171.
30. Stark WJ, Wegner K, Pratsinis SE, Baiker A. Flame aerosol synthesis of vanadia-titania nanoparticles: Structural and catalytic properties in the selective catalytic reduction of NO by NH<sub>3</sub>. *J. Catal.* 2001;197(1):182-191.
31. Strobel R, Pratsinis SE, Baiker A. Flame-made Pd/La<sub>2</sub>O<sub>3</sub>/Al<sub>2</sub>O<sub>3</sub> nanoparticles: thermal stability and catalytic behavior in methane combustion. *J. Mater. Chem. C* 2005;15(5):605-610.
32. Fujiwara K, Müller U, Pratsinis SE. Pd subnano-clusters on TiO<sub>2</sub> for solar-light removal of NO. *ACS Catal.* 2016;6(3):1887-1893.
33. Fujiwara K, Pratsinis SE. Atomically dispersed Pd on nanostructured TiO<sub>2</sub> for NO removal by solar light. *AIChE J.* 2017;63(1):139-146.
34. Wang WN, An WJ, Ramalingam B, Mukherjee S, Niedzwiedzki DM, Gangopadhyay S, Biswas P. Size and structure matter: Enhanced CO<sub>2</sub> photoreduction efficiency by size-resolved ultrafine Pt nanoparticles on TiO<sub>2</sub> single crystals. *J. Am. Chem. Soc.* 2012;134(27):11276-11281.
35. Kumfer BM, Shinoda K, Jeyadevan B, Kennedy IM. Gas-phase flame synthesis and properties of magnetic iron oxide nanoparticles with reduced oxidation state. *J. Aerosol Sci.* 2010;41(3):257-265.
36. Willis JJ, Goodman ED, Wu L, Riscoe AR, Martins P, Tassone CJ, Cargnello M. Systematic identification of promoters for methane oxidation catalysts using size- and composition-controlled Pd-based bimetallic nanocrystals. *J. Am. Chem. Soc.* 2017;139(34):11989-11997.
37. Li S, Ren Y, Biswas P, Tse SD. Flame aerosol synthesis of nanostructured materials and functional devices: Processing, modeling, and diagnostics. *Prog. Energy Combust. Sci.* 2016;55:1-59.
38. Ghazzal MN, Wojcieszak R, Raj G, Gaigneaux EM. Study of mesoporous CdS-quantum-dot-sensitized TiO<sub>2</sub> films by using X-ray photoelectron spectroscopy and AFM. *Beilstein J. Nanotechnol.* 2014;5:68-76.
39. Masiala TM, Bantu AKM, Bakambo GE, Lunguya JM, Kanza JLK, Muamba OM. Influence of pH preparation on the photo-response of electrodeposited titanium dioxide (TiO<sub>2</sub>) thin films. *International Journal of Materials Science and Applications.* 2016;5:207-213.
40. Liu P, Chen TP, Li XD, Liu Z, Wong JI, Liu Y, Leong KC. Effect of exposure to ultraviolet-activated oxygen on the electrical characteristics of amorphous indium gallium zinc oxide thin film transistors. *Ecs Solid State Lett.* 2013;2(4):Q21-Q24.

41. Kannisto H, Arve K, Pingel T, Hellman A, Härelind H, Eränen K, Olsson E, Skoglundh M, Murzin DY. Murzin, On the performance of Ag/Al<sub>2</sub>O<sub>3</sub> as a HC-SCR catalyst - influence of silver loading, morphology and nature of the reductant. *Catal. Sci. Technol.* 2013;3(3):644-653.
42. Murzin DY. On cluster size dependent activity and selectivity in heterogeneous catalysis. *Catal. Lett.* 2012;142(11):1279-1285.
43. Hellman A, Resta A, Martin NM, Gustafson J, Trinchero A, Carlsson PA, Balmes O, Felici R, van Rijn R, Frenken JWM, Andersen JN, Lundgren E, Grönbeck H. The active phase of palladium during methane oxidation. *J. Phys. Chem. Lett.* 2012;3(6):678-682.
44. Crampton AS, Rötzer MD, Ridge CJ, Yoon B, Schweinberger FF, Landman U, Heiz U. Assessing the concept of structure sensitivity or insensitivity for sub-nanometer catalyst materials. *Surf. Sci.* 2016;652:7-19.
45. Benson JE, Kohn HW, Boudart M. On the reduction of tungsten trioxide accelerated by platinum and water. *J. Catal.* 1966;5(2):307-&.
46. Ostrovskii V. Surface "Homogeneity vs. Heterogeneity" problem for thermally stabilized crystalline bodies and the nature of heterogeneous catalysis. *Journal "Scientific Isrel- Technological Advantages"*. 2011;13(4).
47. Bissette AJ, Fletcher SP. Mechanisms of autocatalysis. *Angew. Chem. Int. Ed.* 2013;52(49):12800-12826.
48. Masunov AE, Wait E, Vasu SS. Chemical reaction CO+OH<sup>\*</sup>-CO<sub>2</sub>+H<sup>\*</sup> autocatalyzed by carbon dioxide: Quantum chemical study of the potential energy surfaces. *J. Phys. Chem. A* 2016;120(30):6023-6028.
49. Yang Y, Mims CA, Mei DH, Peden CHF, Campbell CT. Mechanistic studies of methanol synthesis over Cu from CO/CO<sub>2</sub>/H<sub>2</sub>/H<sub>2</sub>O mixtures: The source of C in methanol and the role of water. *J. Catal.* 2013;298:10-17.

Table 1. Total Pd loading, total Pd mass in 10 mg of Pd-TiO<sub>2</sub> catalyst ( $M_{\text{Total Pd}}$ ), and the average size of Pd-TiO<sub>2</sub> particle ( $d_{\text{av, Pd-TiO}_2}$ ), and the average size of Pd subnano-cluster/nanoparticle ( $d_{\text{av, Pd}}$ ) as determined from ICP-MS, FESEM-EDS and STEM analyses.

	Pd precursor feed concentration (mM)	Total Pd loading <sup>a</sup> (wt%)	Total Pd loading <sup>b</sup> (wt%)	$M_{\text{Total Pd}}$ (μg)	$d_{\text{av, Pd-TiO}_2}$ (nm) <sup>c</sup>	$d_{\text{av, Pd}}$ (nm) <sup>c</sup>
catalyst 1	0.5	0.24	0.21	23.98	7.57 ± 2.19	<0.5
catalyst 2	1.0	0.45	0.44	45.30	7.18 ± 2.07	0.51 ± 0.12
catalyst 3	1.3	0.76	0.75	75.96	7.61 ± 2.11	0.66 ± 0.16
catalyst 4	2.1	1.08	1.00	107.91	7.14 ± 1.04	0.85 ± 0.17
catalyst 5	3.0	1.25	1.25	125.25	7.34 ± 1.91	1.04 ± 0.18

	Pd precursor feed concentration (mM)	Total Pd loading <sup>a</sup> (wt%)	Total Pd loading <sup>b</sup> (wt%)	$M_{\text{Total Pd}}$ ( $\mu\text{g}$ )	$d_{av, \text{Pd-TiO}_2}$ (nm) <sup>c</sup>	$d_{av, \text{Pd}}$ (nm) <sup>c</sup>
<sup>a</sup> Total Pd loading was determined by ICP-MS.	<sup>a</sup> Total Pd loading was determined by ICP-MS.	<sup>a</sup> Total Pd loading was determined by ICP-MS.	<sup>a</sup> Total Pd loading was determined by ICP-MS.	<sup>a</sup> Total Pd loading was determined by ICP-MS.	<sup>a</sup> Total Pd loading was determined by ICP-MS.	<sup>a</sup> Total Pd loading was determined by ICP-MS.
<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).	<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).	<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).	<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).	<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).	<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).	<sup>b</sup> Total Pd loading was determined by FESEM- EDS. <sup>c</sup> Sizes were determined by STEM (see Figure 2).

Table 2. Fractions of metallic Pd, PdO and intermediate PdO<sub>x</sub> as determined from XPS analysis, masses of metallic Pd ( $M_{\text{metallic Pd}}$ ), PdO ( $M_{\text{PdO}}$ ) and intermediate PdO<sub>x</sub> ( $M_{\text{PdO}_x}$ ), and total surface area of metallic Pd ( $\text{TSA}_{\text{metallic Pd}}$ ), PdO ( $\text{TSA}_{\text{PdO}}$ ) and intermediate PdO<sub>x</sub> ( $\text{TSA}_{\text{PdO}_x}$ ).

catalyst 1  
catalyst 2  
catalyst 3  
catalyst 4  
catalyst 5

<sup>a</sup> The molecular weight of PdO<sub>x</sub> was assumed to be the average of the molecular weights of the metallic Pd and PdO. <sup>b</sup> Th

Table 3. O<sub>2</sub> and CH<sub>4</sub> conversion, and apparent reaction rate constant ( $k_{\text{app}}$ ) with TiO<sub>2</sub>, catalyst 1, catalyst 2, catalyst 3, catalyst 4 and catalyst 5 at 723 K.

	O <sub>2</sub> conversion (%)	CH <sub>4</sub> conversion (%)	$k_{\text{app}}$ (min <sup>-1</sup> )
TiO <sub>2</sub>	30.9	50.7	7.71
catalyst 1	55.8	64.4	17.01
catalyst 2	67.0	81.9	23.10
catalyst 3	77.0	92.4	30.62
catalyst 4	75.3	93.8	29.13
catalyst 5	70.1	93.0	25.15

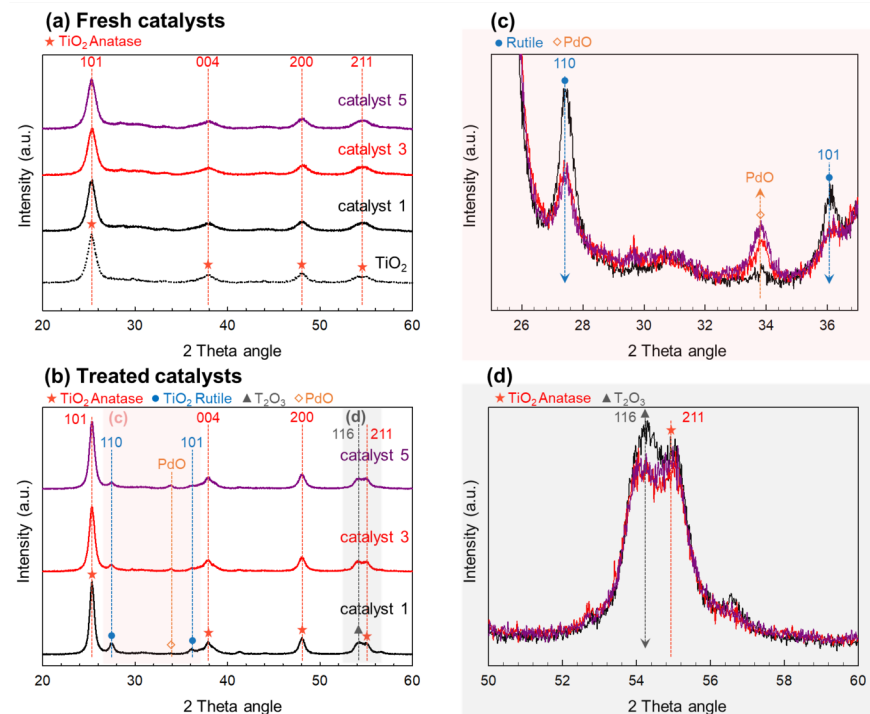


Figure 1. XRD patterns of a) fresh catalysts and b-d) treated catalysts.



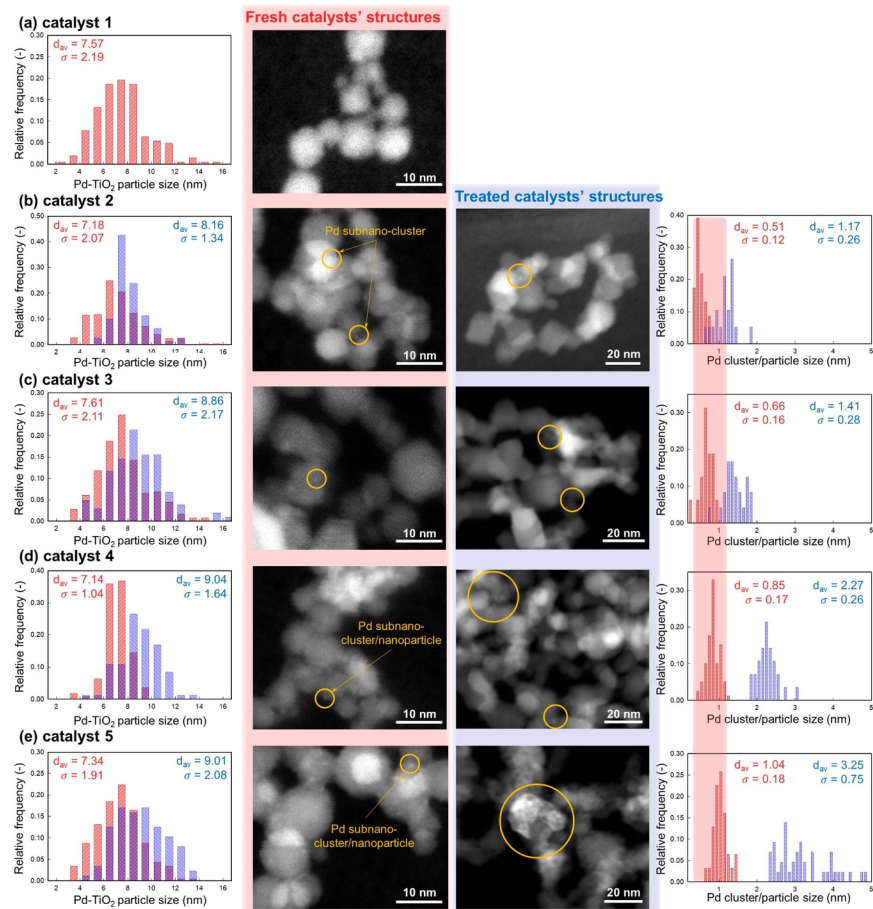


Figure 2. Bulk Pd-TiO<sub>2</sub> nano particle and Pd subnano cluster/nano particle size distributions, and STEM images of a) catalyst 1, b) catalyst 2, c) catalyst 3, d) catalyst 4, and e) catalyst 5. Results related to the fresh catalysts are denoted with red-color and results related to the treated catalysts are shown with blue-color.

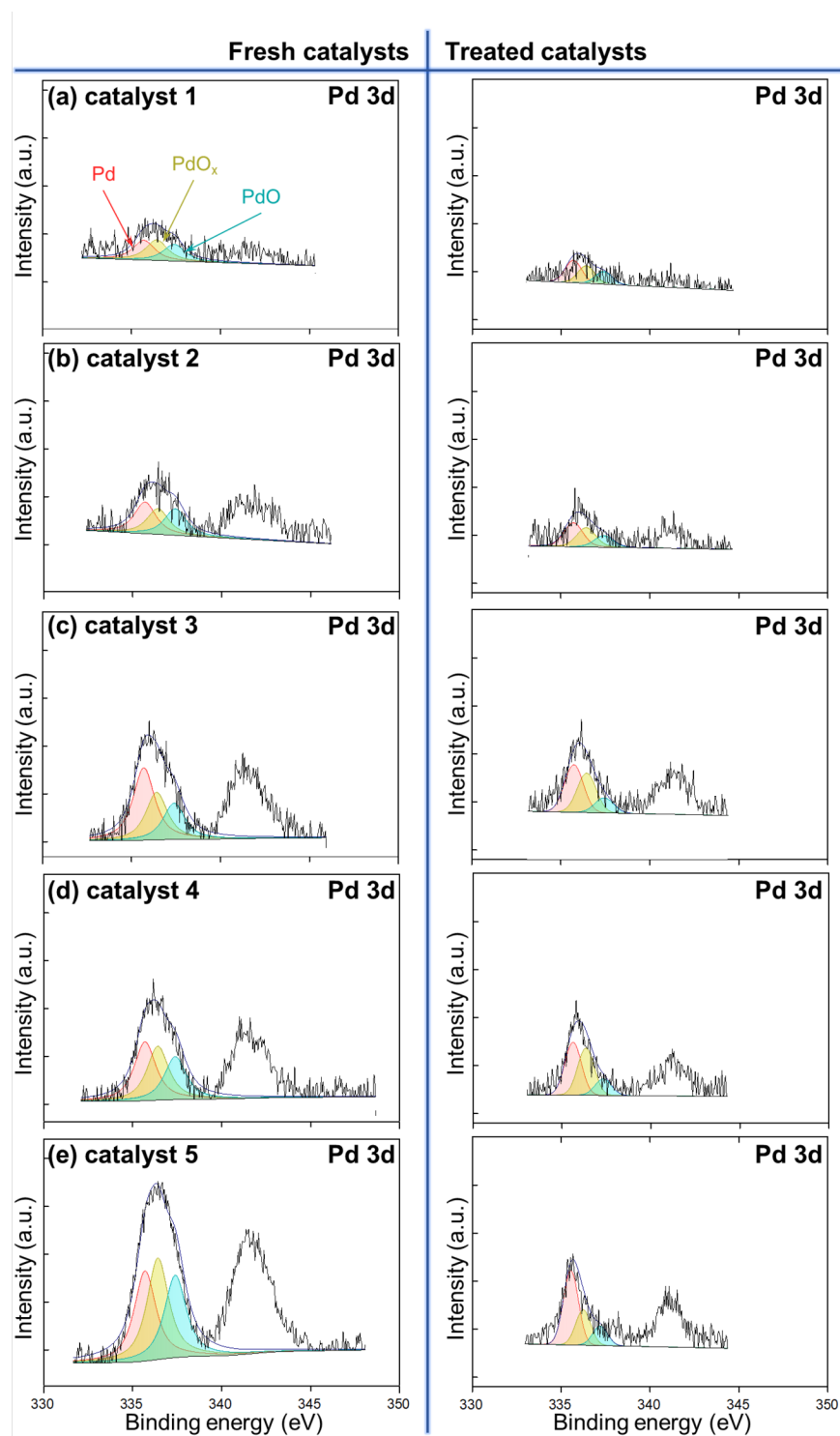


Figure 3. XPS spectra of fresh and treated Pd-TiO<sub>2</sub>catalysts: Pd metal (black, 335.7 eV), PdO<sub>x</sub> (dark gray, 336.42 eV), PdO (gray, 337.4 eV).

Hosted file

image4.emf available at <https://authorea.com/users/308763/articles/440166-flame-synthesis-of-pd-tio2-nanocomposite-catalyst-for-oxygen-removal-from-co2-rich-streams-in-oxy-combustion-exhaust>

#### Hosted file

image5.emf available at <https://authorea.com/users/308763/articles/440166-flame-synthesis-of-pd-tio2-nanocomposite-catalyst-for-oxygen-removal-from-co2-rich-streams-in-oxy-combustion-exhaust>

Figure 5. (a) Variation of the apparent reaction rate constant ( $k_{app}$ ) with (a) Pd loading, (b) the fraction of the total surface area of metallic Pd in the fresh catalysts ( $\alpha_{fresh}$ ), (c) the fraction of the total surface area of metallic Pd in the treated catalysts ( $\alpha_{treated}$ ), and (d) the average fraction of the total surface area of metallic Pd ( $\alpha_{avg}$ ) at different temperatures.

#### Hosted file

image6.emf available at <https://authorea.com/users/308763/articles/440166-flame-synthesis-of-pd-tio2-nanocomposite-catalyst-for-oxygen-removal-from-co2-rich-streams-in-oxy-combustion-exhaust>

Figure 6. (a)  $O_2$  and (b)  $CH_4$  conversion vs. temperature with catalyst 3 under different initial compositions (0%, 53%, and 95% of  $CO_2$  in balance He).

#### Hosted file

image7.emf available at <https://authorea.com/users/308763/articles/440166-flame-synthesis-of-pd-tio2-nanocomposite-catalyst-for-oxygen-removal-from-co2-rich-streams-in-oxy-combustion-exhaust>

#### Hosted file

image8.emf available at <https://authorea.com/users/308763/articles/440166-flame-synthesis-of-pd-tio2-nanocomposite-catalyst-for-oxygen-removal-from-co2-rich-streams-in-oxy-combustion-exhaust>