

Assessing impact of tillage and mulch on soil erosion estimated by Beryllium-7 and on soil moisture, and runoff in Central Benin

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Abstract

This study was conducted to assess effect of tillage and mulch on soil erosion control in typical agroecological conditions of Benin. In addition, it involved also the assessment of soil moisture and runoff. The experiment was conducted on two sites in Central Benin during the short rain season of 2018. The effect of three tillage practices (contour ridging: CR; slope ridging: SR and no-tillage: NT) and three mulch doses (0 t.ha⁻¹; 3 t.ha⁻¹; and 7 t.ha⁻¹) on soil erosion under maize was investigated at small experimental plots (21 m²). The ⁷Be method was used to assess the erosion rates, runoff was measured by total collection and soil moisture content was determined by thermo-gravimetric method. The results showed a significant decrease in runoff coefficient and soil loss while increase soil moisture under no-tillage and contour ridges compared to slope ridges. This effect was pronounced with greatest. 3 and 7 tha⁻¹. Highest runoff coefficient and soil loss and the lowest soil moisture were observed under slope ridging without mulch (i.e. SR0M). The ⁷Be measurement showed high soil losses under SR0M (-10.19 t ha⁻¹) at Dan and under NT0M (-7.36 t ha⁻¹) at Za-zounmè. The treatments NT7M (0.80 t ha⁻¹); SR7M (0.69 t ha⁻¹); IR3M (2.07 t ha⁻¹) and CR7M (4.05 t ha⁻¹) showed deposition at Dan while SR7M (0.23 t ha⁻¹) and CR7M (3.93 t ha⁻¹) showed deposition at Za-zounmè. This study revealed useful information to be taken into consideration when developing soil and water conservation management strategies in Benin.

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Core Ideas

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Core Idea 1: First application of fallout radionuclides in assessing Short-term soil erosion in Benin.

Core Idea 2: Application of Beryllium-7 provide accurate information on the effects of land management on soil erosion rates

Core Idea 3: No-tillage and Contour ridging reduced erosion and increased soil moisture as compared to slope ridging

Core Idea 4: To have real benefit from mulch, a 3-7 t/ha should be applied.

Core Idea 5: CUST_CORE_IDEA_5 :No data available.

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23 **1. Introduction**

24 Soil erosion is by far the most important soil degradation process and eroded soils
25 represent approximately 84% of degraded areas worldwide (FAO, 2015). A growing body of
26 research over the last years has shown that soil erosion is one of the most important challenges
27 facing humanity (FAO, 2015; Panagos et al., 2016; Alewell et al., 2019). Oldeman et al (1991)
28 estimated that 56% of the world's soils were under the threat of mild to severe forms of water
29 erosion. However, more than 75% of degraded land is located in the developing countries (Mabit
30 et al., 2014). In Africa, many agricultural regions are affected by water erosion (Bossa, 2007;
31 Bashagaluke et al., 2018). In Benin forest destruction, land over-exploitation and unsuitable
32 agricultural practices have contributed to great changes in the agricultural systems. These
33 changes have led to accentuated soil degradation. As a result, most of the agroecological zones in
34 Benin are characterized by high levels of erosion risk. In Centre Benin, the situation is very
35 worrying. Rainfall comes in the form of localized and violent thunderstorms, on bare soil and
36 run-off is instantly causing soil erosion of the soil surface. This results in declining soil fertility
37 and decreasing crop yields (Saïdou et al., 2012). Cereal crops (e.g. maize) that are strategic in
38 maintaining food security for local populations are highly impacted (Akplo et al., 2022).
39 Maintaining food security in Benin urgently requires a soil conservation strategy to minimize soil
40 erosion. This is all the more urgent considering the fact that the quantity and quality of
41 agricultural production is highly dependent on soil quality (World Economic Forum, 2010).

42 Conservation Agriculture (CA) practices are considered as an alternative to traditional
43 agricultural practices for ensuring food security and reducing agricultural related soil degradation
44 (Badgley et al., 2007; Farooq & Siddique, 2015). CA is a set of practices, including minimum
45 soil disturbance, permanent soil cover, diversified crop rotations, and integrated weed

46 management (Hobbs et al. 2008; Friedrich et al. 2012). Reducing and/or reverting soil erosion
47 (Van den Putte et al., 2010), soil organic matter (SOM) decline, water loss, soil physical
48 degradation, and fuel use (Baker et al., 2002) and improvement of crops yield and soil
49 biodiversity (Friedrich et al., 2012) are among the well-known effects of CA. CA promotes
50 minimal soil disturbance through no-tillage or reduced tillage, crop residue management and
51 organic wastes; all aimed at reducing soil erosion (Farooq & Siddique, 2015). In Benin, the
52 contour ridging (CR); slope ridging (SR) are the most common tillage practices (Akplo et al.,
53 2019).

54 The ridges are formed manually using hoe and tape measure and they are 60 cm wide and
55 20 cm high. The ridges are oriented in slope direction in the case of SR system or along the
56 contour lines in the case of CR system. No-tillage (NT) and mulching practices have been
57 promoted but their adoption by farmers remains very rare. Reduction of runoff and erosion and
58 increase of soil organic carbon (SOC) content, root length and density and soil water storage are
59 the main outcomes of NT practices (Lal, 2004; Fiorini et al., 2018). Crop residues as mulch at the
60 soil surface provide shade, protect the soil surface against mechanical impact of raindrops and
61 limit the surface runoff (Bashagaluke et al., 2018), increase carbon sequestration (Balesdent et
62 al., 2000), preserve soil moisture and supports high soil biological activity (Douzet et al., 2010;
63 Mazarei & Ahangar, 2013). In the specific physical context of centre Benin, certain NT and
64 mulching practices can be useful to address the challenges of soil erosion reduction and water
65 conservation. However, traditions and mindset, along with a lack of technical knowledge are
66 major constraints for CA systems adoption in Benin (Akplo et al., 2019). Small traditional
67 farmers are very conservative. They rely on approaches inherited from past and firmly fixed in

68 their traditional way of life (Akplo et al., 2022). Therefore, providing information on the effective
69 soil erosion control practices in Benin is the most important stage for soil conservation.

70 Erosion plots can provide valuable information regarding on-site erosion rates associated
71 with different soil types or crops and different tillage systems, but they are unable to provide the
72 spatially distributed information required to investigate patterns of soil redistribution within
73 individual fields or on the slopes of a small watershed. However, most developing countries do
74 not have the resources to establish institutionalized land care/watershed development programs
75 for implementing long-term soil conservation activities. The quest for alternative techniques of
76 soil erosion assessment to complement existing methods and to meet new requirements has
77 directed attention to a particular group of environmental radionuclides, namely fallout
78 radionuclides (FRNs). The use of FRNs can complement and in some cases even substitute
79 conventional measurements to evaluate erosion and sedimentation processes for developing and
80 improving land management and soil conservation measures (Zapata, 2002; Walling, 2006; Mabit
81 et al., 2008; Porto et al., 2012; Dercon et al., 2012; Benmansour et al., 2013; Gaspar & Navas,
82 2013). Beryllium-7 (${}^7\text{Be}$, $t_{1/2} = 53.3$ days) is a cosmogenic radionuclide produced in the upper
83 atmosphere and lower stratosphere by cosmic ray spallation of nitrogen and oxygen. Because of
84 its short half-life it has a potential to quantify the effects of land use and land management on soil
85 erosion rates and to evaluate the efficiency of soil conservation measures. Further it is able to
86 evaluate micro-spatial variation in erosion at the field scale (Mabit et al., 2008; Schuller et al.,
87 2006; Ryken et al., 2018; Mabit & Blake, 2019).

88 The primary objective of the study was to assess the impact of different tillage practices
89 and different mulch doses on soil erosion (estimated by Beryllium-7), runoff (measured by total
90 collection at experimental plots) and soil moisture content (measured by thermo-gravimetric

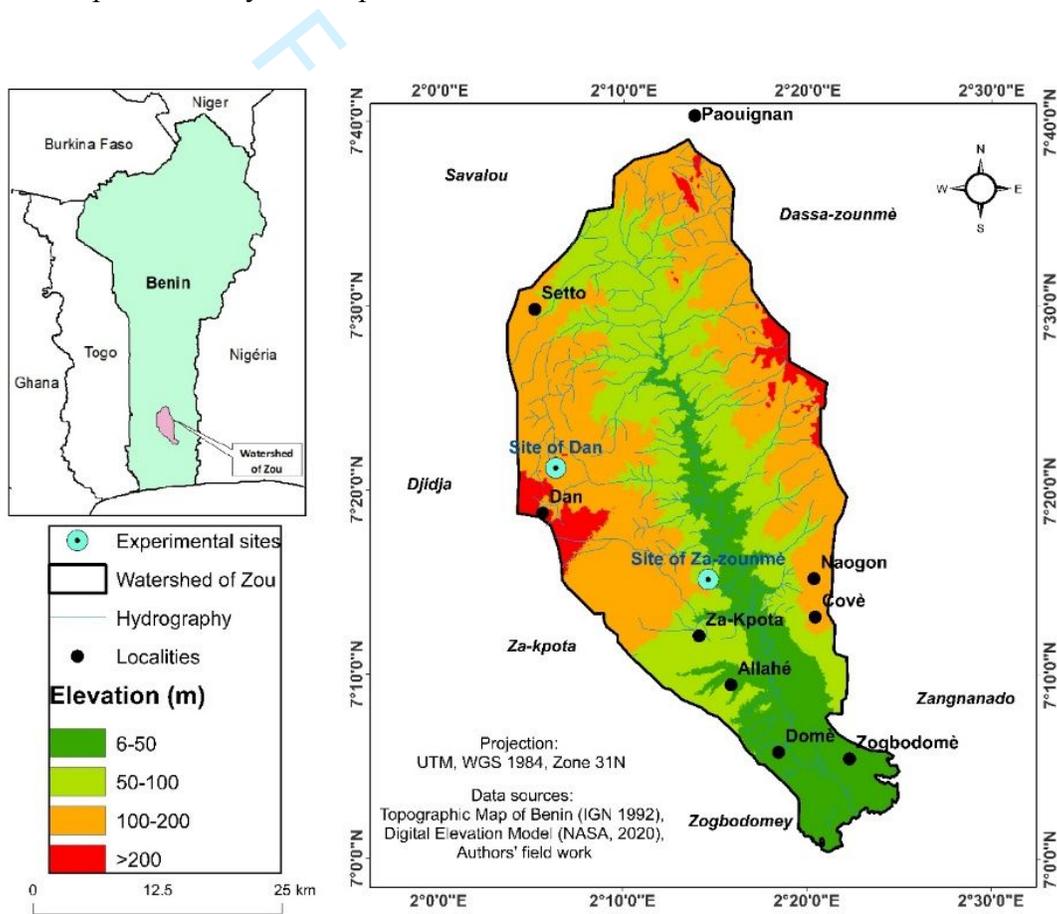
91 method) in agroecological conditions typical for Central Benin. All observations and
92 measurements were done on experimental plots under natural precipitation. Our hypothesis was
93 that both tested conservation measures NT and CR combined with mulching should reduce soil
94 erosion and runoff, and increase soil moisture content.

95 **2. Material and methods**

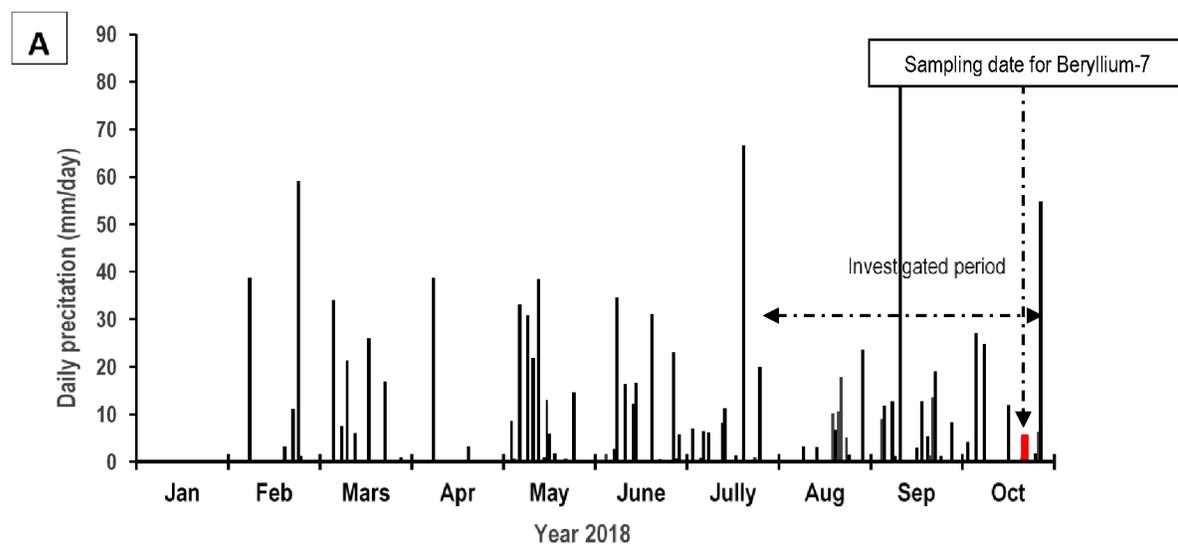
96 **2.1. Study area and experiment period**

97 Two experimental fields were selected: Dan (7°21'35" N; 002°05'09" E) and Za-zounmè
98 (7°12'50" N; 002°15'40" E) (Figure 1). The experimental fields were the same as described in
99 Akplo et al. (2022). Before implementing the experiences, both sites were fallowed since 2000
100 without any tillage. However, farmers frequently burned the natural vegetation that grows back
101 when the rainy season resumes. Also, cattle from the area were grazing in the fields (Akplo et al.,
102 2022). The soil of Dan is classified as Acrisol and the soil of Za-zounmè is classified as Ferralsol
103 (IUSS Working Group WRB, 2015). Both sites have similar climate and soil conditions. The sites
104 are situated on gently undulating denudation plateau (the slope inclination is 5% at Dan and 4.6%
105 at Za-zounmè). A baseline soil fertility reference was collected along the diagonal of the field at a
106 depth of 0–20 cm and analyzed at laboratory of soil analysis in Benin. At Dan, the soil is sandy-
107 clay-loam, and the pH (water 1:2.5) is acid (5.63), organic matter content is 13.7 g.kg⁻¹ of soil,
108 exchangeable potassium content is 129.03 mg.kg⁻¹ of soil, Bray P is 12.6 ppm and total nitrogen
109 content of 0.88 g.kg⁻¹ of soil. Water infiltration rate is 41 cm.day⁻¹. At Za-zounmè, the soil
110 texture is sandy-loam, the pH (water 1:2.5) is close to neutral (6.40), organic matter content is
111 12.4 g.kg⁻¹ of soil, exchangeable potassium content is 140.76 mg.kg⁻¹, Bray P is 18.12 ppm, and
112 total nitrogen content is 0.69 g.kg⁻¹ of soil. Water infiltration rate is 120 cm.day⁻¹. The average
113 rainfall varies from 1100 to 1300 mm/year and with a bimodal pattern of rainfall distribution for

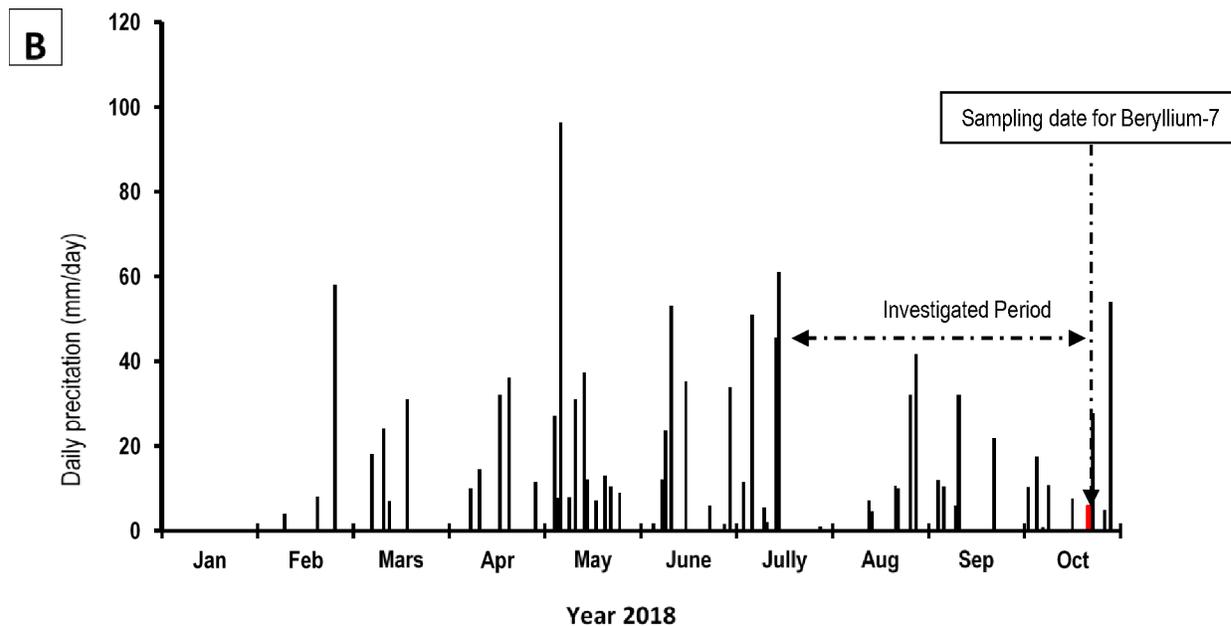
114 both sites. The rainfall record for the period between January 1 and October 31, 2018 is shown in
 115 Figure 2. After a prolonged dry period from November to March, a rainy period followed from
 116 March to July 2018 and was characterized by a total rainfall of 598.7 mm in 44 days at Dan and
 117 736 mm in 35 days at Za-zounmè. In August a short dry season occurred followed by a period of
 118 very heavy rainfall from September to October. For this period 321.3 mm were recorded in 29
 119 rain events at Dan and 220 mm were recorded in 16 rain events at Za-zounmè. The targeted
 120 period of the present study was September to October.



121
 122 Figure 1: Watershed of Zou and experimental field location [Projection: UTM WGS 1984 Zone
 123 31N; Data source: Topographic Map of Benin (IGN 1992), Digital Elevation Map (NASA 2020),
 124 Authors' fieldwork]



126



127

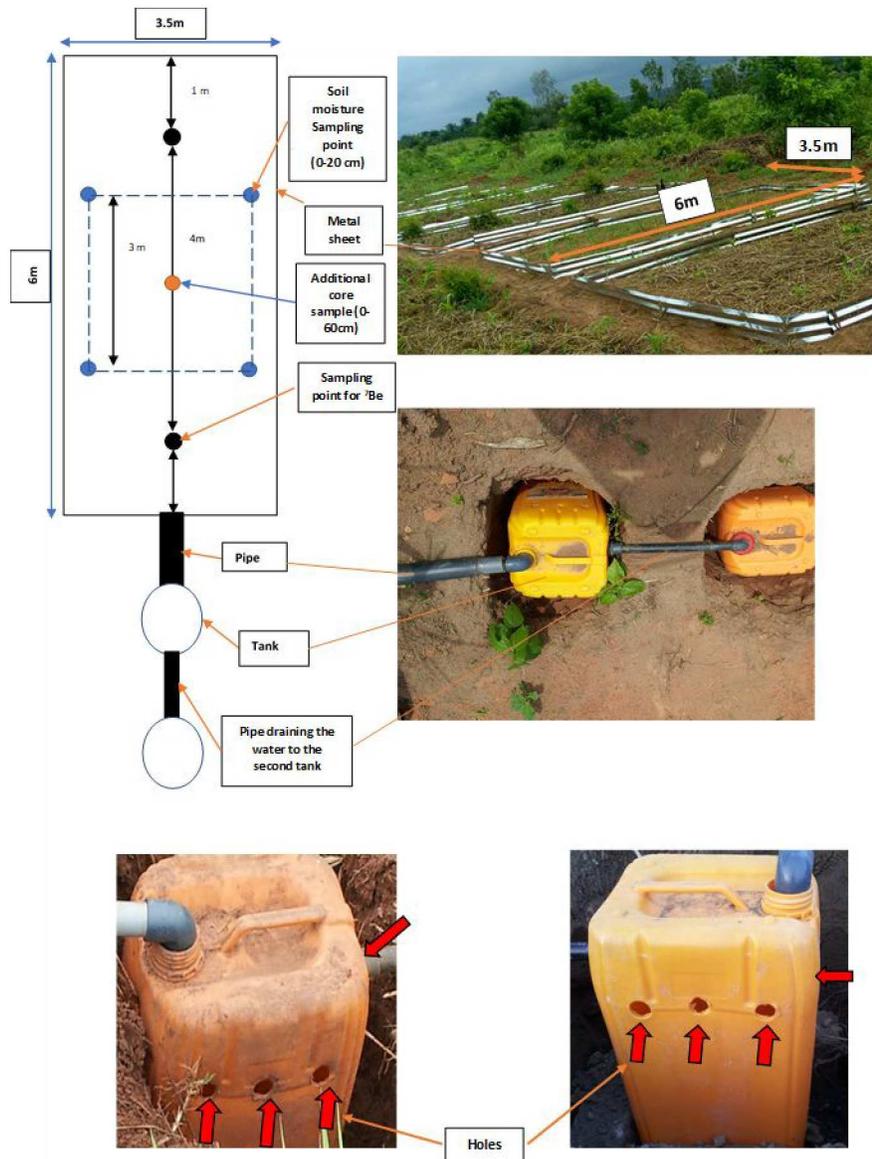
128 Figure 2: The daily precipitation recorded for the study sites (A = Dan and B = Za-Zounmè) for
 129 the period from January 1 to October 31, 2018. The arrow shows the date of the soil sampling for
 130 ^7Be measurements (October 21, 2018 at Dan and October 22, 2018 at Za-Zounmè)

131 2.2. Experimental design

132 Maize (*Zea mays* L.) was selected as the suitable crop for this investigation of the tillage
 133 and mulch impact on soil erosion because it is commonly grown in this area and it has low soil
 134 conservation efficiency. The planting density was 35,000 seed hills/ha. The experimental design

135 was Randomly Complete Block with tree replications. The treatments combined three tillage
136 practices: NT (no-tillage); SR (slope ridging, i.e. ridges parallel to the slope); CR (contour
137 ridging, i.e. ridges parallel to contours) and three amounts of mulch: 0M (0 t ha⁻¹); 3M (3 t ha⁻¹)
138 and 7M (7 t ha⁻¹). Maize stover (C:N ratio = 46) was applied for the mulch treatments. In all
139 seasons mulch levels of <3 t ha⁻¹ were used because cereal stover yields of up to 3 t ha⁻¹ are
140 achievable on smallholder farms in central Benin (Saïdou et al. 2018, Akplo et al. 2020). Mulch
141 levels of 7 t ha⁻¹ were selected in order to assess if there is any yield benefit in increasing surface
142 cover beyond 4 t ha⁻¹ which normally gives the minimum 30% cover for Conservation
143 Agriculture systems (Erenstein, 1997). Being the farmer's practice, slope ridge system was used
144 as control in this experiment. The construction of ridges was done manually using hoe and tape
145 measure. The ridges were oriented in slope direction in the slope ridge system) or along the
146 contour lines in contour ridging system. The ridges were 60 cm wide and 20 cm high. On both
147 SR and CR plots, the distances between the ridges were 0.80 m. In the CR system, ridges were
148 made following the width of the plots. So, eight ridges of 3.5 m in length were made of each plot
149 of CR system. In the SR system, ridges were made along the length of the plot and five ridges of
150 6 m in length were made in SR system. In no-tillage system, the crop was sowed directly without
151 any soil preparation. The seedling pop was done with a machete or hoe. The mulch was made
152 using vegetal residues. Runoff plots were established to evaluate the runoff amount as described
153 in Akplo et al. (2022). Each plot was fenced from its surroundings by metal sheets embedded in
154 the ground (Figure 3). The collection of runoff and sediment used fractional approach. At the
155 lower end of the plots all runoff water and eroded soil was drained to a storage system composed
156 of two tanks. The first tank was connected to each plot by a PVC pipe with 40 mm in diameter. It
157 was pierced in its upper part with 8 identical holes, one of which was further connected to the

158 second tank by a PVC pipe of 20 mm diameter while remaining 7 holes were draining the
 159 remaining water and soil to surrounding open space.



160
 161 Figure 3 : The experimental field setup

162 2.3. Soil moisture assessment

163 Soil moisture (%) was determined for the 20 top centimeters after each rain of 40mm or
 164 more. In total 4 soil profiles forming a regular grid of 3m x 3m was installed (4 points) and the
 165 samples were taken at each side of the grid from the top to 20 cm in depth (Figure 3). In order to

166 assess the effect of the tillage and mulching on the depth distribution of soil moisture, one
167 additional core was sampled per plot from the top to 60 cm in depth at a resolution of 10cm (i.e.:
168 0-10 cm; 10-20 cm; 20-30 cm; 30-40 cm; 40-50 cm; 50-60 cm). Soil moisture was determined by
169 ‘‘thermo-gravimetric method’’ (Anderson & Ingram, 1993). The wet weight (P_W) of the samples
170 was determined on site and the dry weight (P_D) determined in the laboratory after oven drying at
171 105°C until a constant dry weight. Soil moisture content (H) was determined by the following
172 formula proposed by Saïdou et al. (2012):

$$173 \quad H (\%) = (P_W - P_D) / P_D * 100$$

174 **2.4. Runoff coefficient estimation**

175 The total volume of each rain event was measured using rain gauge (iMETOS IMT280).
176 Runoff was collected in the tanks with the installed receiving system. The runoff volume (V_r)
177 was estimated as follows:

$$178 \quad V_r = V_1 + (\beta * V_2)$$

179 Where V_1 is the volume of runoff in the first tank; V_2 is the volume of runoff in the second tank; β
180 is a constant associated with the number of holes of the first tank (in our case, $\beta=8$).

181 The runoff coefficient was estimated using the following equation:

$$182 \quad R (\%) = (V_r / V) * 100 \quad \text{Where } V = \text{the total rain amount (in liter)}$$

183 **2.5. Principle of erosion estimation using ^7Be tracer**

184 The ^7Be -method, similarly as other FRN methods is based on ^7Be occurrence only in
185 uppermost soil layer (as it was deposited from atmosphere) and its immobility in soil. The origin
186 of ^7Be is cosmogenic and it is created by interaction of cosmic rays with atmosphere. The
187 estimation of soil erosion rates is based on comparison of ^7Be inventories (Bq m^{-2}) at studied site
188 with reference inventories representing soil undisturbed by erosion (Mabit and Blake, 2019;
189 Blake et al., 2002; Schuller et al., 2006; Walling et al., 1999; Sepulveda et al., 2008; de Rosas et
190 al., 2018; Taylor et al., 2013). When the value of the inventory at the study site is lower than the
191 value of the reference inventory there is erosion and in the opposite case, there is deposition. A
192 simple conversion model (Profile Distribution Model, PDM) based upon the ^7Be depth
193 distribution is used to convert the ^7Be inventory measurements into quantitative soil erosion or
194 deposition rates (Blake et al., 1999; Taylor et al., 2019).

195 2.6. Sampling strategy for ^7Be determination

196 The present investigation was undertaken for the period of heavy rain events from
197 September 2018 to October 2018. The fields were under fallow since 2000. The treatments had
198 been installed since 10th May 2018 at Dan and 12th May 2018 at Za-zounmè. The soil sampling
199 for Be-7 was done on October 21th, 2018 at Dan and October 22nd, 2018 at Za-zounmè. Since
200 fallout radionuclides (i.e., ^{137}Cs ; $^{210}\text{Pb}_{\text{ex}}$; ^7Be) were used as soil tracers, the redistribution rate
201 assessment is based on comparing the inventory measured at a given sampling site with a
202 reference site. Indeed, when the value of the inventory at the study site is lower than the value of
203 the reference inventory the sampled site is affected by erosion and in the opposite case it is
204 affected by deposition (Sepulveda et al., 2008; de Rosas et al., 2018). For this study, the reference
205 sites were selected at each study site (one reference site was sampled at Dan and one at Za-
206 zounmè). They were localized near the installed treatments (described below) on flat ($\approx 1\%$) land

207 uncultivated since august 2016 and without evidence of soil redistribution (erosion or
208 sedimentation). Ten cores were taken following a grid approach (Mabit et al., 2014) for the
209 reference inventory estimation. As the use of ^7Be technique strongly depends on the h_0 parameter,
210 the depth distribution was measured to a depth of 3 cm at a resolution of 3 mm.

211 Two soil cores ($\text{Ø} = 25$ cm, $h = 3$ cm) were sampled at each experimental plot (Figure 4),
212 in its upper and lower part of the plot using a surface cylindrical collector. The sampling points
213 were at 4m distance each from the other). The collected samples were bulked to analyze the total
214 inventory of ^7Be . On the plots with mulch, the samples of mulch were taken in order to quantify
215 the fraction of beryllium adsorbed by mulch. The ^7Be fraction intercepted and adsorbed by the
216 mulch was estimated and subtracted from the initial reference inventory as the reference site was
217 a bare soil. These values were used as reference values depending on the amount of the mulching.
218 However, for the plot without mulching, the initial reference inventory was used as baseline.
219 Collected samples were air-dried, grinded by hand and sieved at 2 mm.

220 2.7. Gamma spectrometry analysis

221 ^7Be was measured by gamma spectrometry using a High Purity Germanium (HPGe)
222 detector, p-type, with a relative efficiency of 45 % and energy resolution of 2 keV at 1332 keV.
223 ^7Be activity was determined from the net peak area of gamma ray at 477.6 keV (emission
224 intensity of 10.4% Energy and efficiency calibrations were performed by using a certified
225 multigamma standard source (^{137}Cs ; ^{60}Co ; ^{57}Co , ^{139}Ce , ^{109}Cd , ^{113}Sn , ^{88}Y and ^{241}Am). Standard and
226 unknown samples were prepared in the same cylindrical geometry of 100ml. The efficiency at the
227 energy of 477.6 keV of ^7Be was calculated by using the polynomial equation obtained by fitting
228 the efficiency versus energy experimental curve obtained from the analysis of the multigamma

229 standard source. The counting time for the samples was 24 h, to reach a precision of
230 approximately 10% at the 95% level of confidence. Due to the short half-life (53.3 days) of ^7Be ,
231 the activities have been corrected for decay between the collection period and counting time
232 using the following equation (Mabit et al., 2014):

$$233 \frac{\lambda t}{1 - \exp(1 - \lambda t)}$$

234 Where: λ is the decay constant and t the elapsed time (time variation between the sampling time
235 and the analysis time).

236 **2.8. Estimation of soil redistribution using ^7Be tracer**

237 As explained above, stable reference site was selected to measure the baseline ^7Be
238 inventory, which is compared with the ^7Be inventory at the sampling locations. We used the
239 Profile distribution model (PDM) described in Blake et al. (1999) to convert the ^7Be inventories
240 into erosion or deposition rate. This model is based on the depth distribution of the radionuclide
241 in the soil column at undisturbed site. Soil mass depth is used to measure depth in soil and is
242 calculated by dividing the soil mass (kg) by the area of soil layer (m^2). The initial depth
243 distribution $C(x)$ of ^7Be is commonly exponential (Sepulveda et al., 2008; Zhang et al., 2014; de
244 Rosas et al., 2018) and can be expressed as:

$$245 C(x) = C(0)e^{-\frac{x}{h_0}}$$

246 Where x is the mass depth from the soil surface (positive downward) (kg m^{-2}), $C(x)$ is the mass
247 activity of ^7Be at a depth x (Bq kg^{-1}), $C(0)$ is the mass activity of the surface soil (at $x=0$ Bq
248 kg^{-1}), and h_0 is the relaxation mass depth (kg m^{-2}) at which 63% of the total ^7Be activity is found

249 above and is used to quantify the ^7Be penetration into soil (Zhang et al., 2014; Ryken et al.,
250 2018).

251 The ^7Be reference inventory, A_{ref} (Bq m^{-2}), represents the total areal activity at a reference site
252 within the study area:

$$253 \quad A(0) = A_{ref} = \int_0^{\infty} C(x) dx = C(0)h_0$$

254 Considering the initial distribution, the areal activity density below mass depth x , $A(x)$ (Bq m^{-2}),
255 is therefore:

$$256 \quad A(x) = \int_{-x}^{\infty} C(x) dx = A_{ref} e^{(x/h_0)}$$

257 The measured ^7Be inventory A (Bq.m^{-2}) at the specific sampling point will reflect the depth of
258 soil lost x (kg.m^{-2} , negative) and can be represented as:

$$259 \quad x = h_0 \ln\left(\frac{A}{A_{ref}}\right)$$

260 Deposition of sediment is reflected in an excess of ^7Be inventory at the sample site with respect
261 to the reference site. The depth of deposition, x' (kg m^{-2} , positive), can be calculated as:

$$262 \quad x' = (A - A_{ref})/C_d$$

263 Where C_d (Bq kg^{-1}) is the ^7Be concentration of deposited sediment, which may be estimated
264 using the mean ^7Be concentration of the sediment eroded from the upslope eroding areas
265 calculated as:

$$C_d = \int_S x C_e dS / \int_S x dS$$

The ^7Be activity concentration in the eroding sediment at each upslope point, C_e (Bq kg^{-1}), can be calculated from the loss of inventory divided by the mass of soil loss:

$$C_e = (A_{ref} - A) / x$$

2.9. Statistical analysis

Series of statistical analysis were performed. First, multi-site mixed-effect analysis of variance models matching the study design were conducted for each of the collected variable; site, tillage system and mulch input rates effects as fixed effects; and tillage system nested in block nested in site as random effects. This first analysis showed a significant site effect. Given the significant site effect, a three-way analysis of variance (ANOVA) using PROC MIXED procedure was conducted on each site. Tillage system and mulch input rates were taken as a fixed effect while block was considered as random effect. Significant fixed effects were further dissected by extracting means and performing Tukey's Honestly Significant Difference pairwise comparisons. The normality and homogeneity of the data for each variable was tested by Shapiro-Wilk test (Shapiro & Wilk, 1965) and by Bartlett test (Bartlett, 1937), respectively. Relationships between soil erosion variables and soil physical properties were assessed using Pearson correlation test. All statistical analyses were conducted in SAS 9.4 (SAS Institute, 2015) with an alpha of 0.05. Due to interactions between tillage and mulch input rates, the main effects were not reported.

3. Results

286 3.1. Tillage and mulching effect on soil moisture

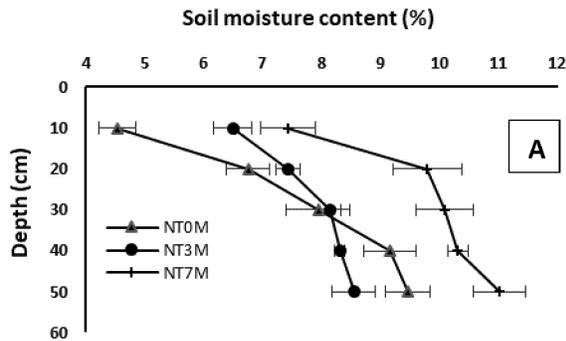
287 The soil moisture of topsoil was very low at both sites, especially at Za-zounmè (6.3-
 288 12.1%) but also at Dan (12.6 – 17.7%). Statistical differences were observed between the
 289 treatments at both Dan and Za-zounmè (Table 1). At both sites, the gravimetric soil moisture
 290 content was lowest on the NT0M plots (12.55% at Dan and 6.33% at Za-zounmè) and highest on
 291 the CR7M plots (17.7% at Dan and 12.1 at Za-zounmè). The difference between the extremes
 292 was 5.1% at Dan and 5.8% at Za-zounmè). The examined soil conservation treatments have
 293 impact also on the soil moisture in the deeper part of soil profile (below 30 cm). The depth
 294 distribution of soil moisture is shown on Figure 4. For all treatments the moisture in deeper part
 295 of soil profile (30 cm and more) is considerably higher than in the topsoil. Mulch increases soil
 296 moisture for all three tillage treatments and this effect is well pronounced especially if the amount
 297 of mulch is great. The differences between 7 tons of mulch and 3 tons of mulch are usually
 298 greater than the differences between 3 tons of mulch and no mulch.

299 Table 1: Effect of studied treatments on soil moisture content of topsoil and runoff (mean \pm
 300 standard deviation)

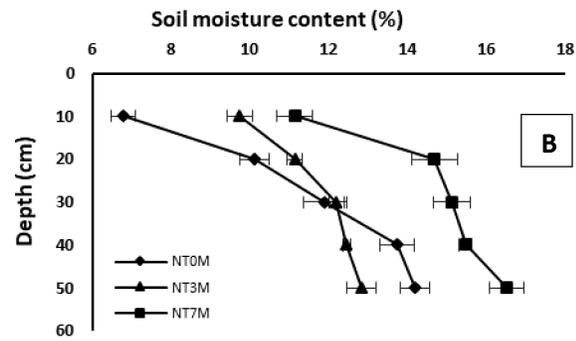
Treatments	Soil moisture content (%)		Runoff coefficient (%)	
	Dan	Za-zounmè	Dan	Za-zounmè
NT0M	12.55 \pm 0.11e	6.32 \pm 0.21c	1.26 \pm 0.54b	2.19 \pm 0.54b
NT3M	13.22 \pm 0.55de	6.74 \pm 0.31c	0.56 \pm 0.18c	0.58 \pm 0.22c
NT7M	15.68 \pm 0.21bc	6.54 \pm 0.1c	0.46 \pm 0.11c	0.59 \pm 0.1c
SR0M	14.98 \pm 0.25c	6.25 \pm 0.41c	4.56 \pm 0.67a	3.89 \pm 1.01a
SR3M	13.73 \pm 0.06d	6.4 \pm 0.49c	0.42 \pm 0.13c	0.47 \pm 0.19c
SR7M	16.29 \pm 0.20b	8.55 \pm 0.18b	0.22 \pm 0.07d	0.2 \pm 0.05c
CR0M	13.79 \pm 0.42d	6.83 \pm 0.19c	0.54 \pm 0.1c	0.65 \pm 0.06c
CR3M	17.48 \pm 0.86a	6.99 \pm 0.10c	0.40 \pm 0.05c	0.44 \pm 0.07c
CR7M	17.70 \pm 0.60a	12.08 \pm 0.19a	0 \pm 0d	0 \pm 0d
p-value	<0.0001	<0.0001	<0.0001	<0.0001

301 *NT0M*: No tillage + 0 t/ha of mulch; *NT3M*: No tillage + 3 t/ha of mulch; *NT7M*: No tillage + 7 t/ha of mulch; *SR0M*: Slope Ridging + 0 t/ha; *SR3M*: Slope Ridging + 3 t/ha of mulch; *SR7M*:
 302 Slope Ridging + 7 t/ha of mulch; *CR0M*: Contour ridging + 0 t/ha of mulch; *CR3M*: Contour ridging + 3 t/ha of mulch; *CR7M*: Contour ridging + 7 t/ha of mulch.

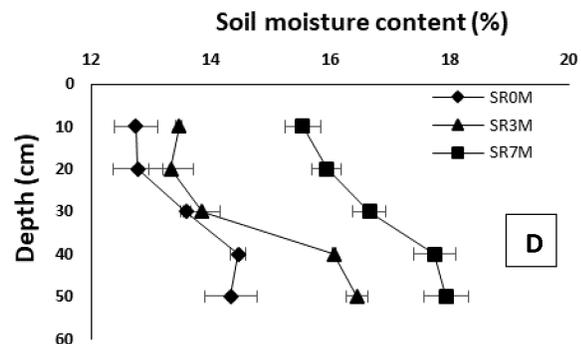
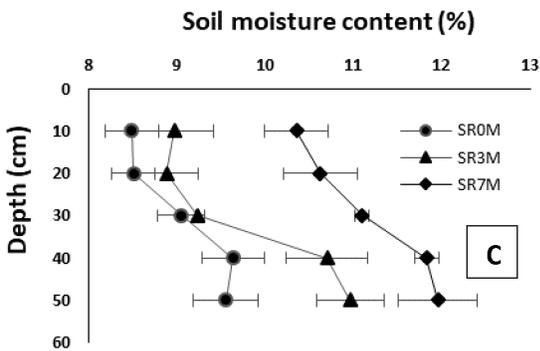
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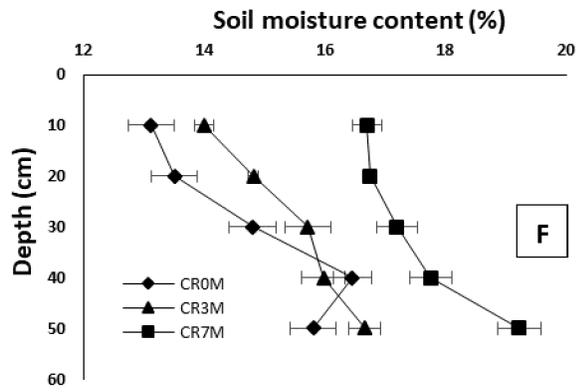
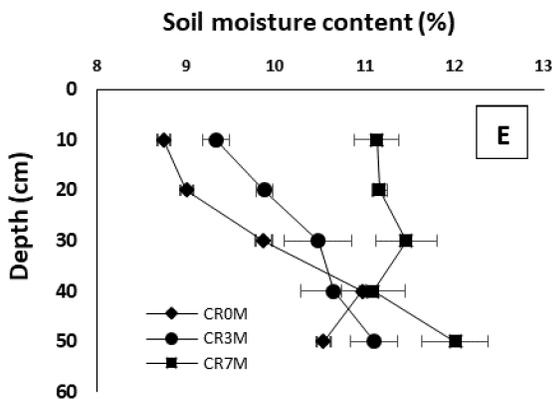
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306



307 Figure 4: Effect of tillage and mulching on the depth distribution of soil moisture: a) no-tillage
 308 treatments at Dan; b) no-tillage treatments at Za-zounmè; c) slope ridging at Dan; slope ridging at
 309 Za-zounmè; e) contour ridging at Dan; f) contour ridging at Za-zounmè. The error bars represent
 310 the standard deviation for each treatment.

311 3.2. Tillage and mulching effect on runoff

312 At both Dan and Za-zounmè, the control (slope ridging + 0 t ha⁻¹ of mulch, i.e. SR0M)
 313 recorded the highest runoff coefficient (4.56 ± 0.67% at Dan and 3.89 ± 1.01% at Za-zounmè)

314 while the lowest runoff coefficient was obtained for contour ridging and 7 t ha⁻¹ of mulch (Table
315 1). Compared with the control, NT0M, NT3M and NT7M respectively reduced the runoff
316 coefficient by 70%; 88% and 90% at Dan and by 43%; 85% and 85% at Za-zounmè. However,
317 the difference observed between the runoff coefficient recorded for the treatments NT3M and
318 NT7M were not significant. The runoff coefficient of CR3M and CR0M were considerably lower
319 as compared with the control. These treatments have reduced the runoff coefficient respectively
320 by 91% and 88% at Dan and by 88% and 83% at Za-zounmè.

321 3.2.1. Sediment transport based on ⁷Be measurement

322 The depth distribution of ⁷Be at the reference sites is shown at Figure 5. For both
323 reference sites, the ⁷Be activity decreased exponentially with increasing mass depth from the top
324 layer to a depth of 3 cm. However, for the reference site of Dan, the mass depth was found to be
325 higher (43.39 kg m⁻²) than at Za-zounmè (29.62 kg m⁻²). At both reference sites, 63% of the total
326 areal activity was found in the soil above a mass depth of 5 kg m⁻² (respectively h₀= 5.75 at Dan
327 and h₀= 5.46 at Za-zounmè), i.e., the upper 3 mm. We found initial ⁷Be concentration C(0) of
328 55.58 Bq kg⁻¹ and 78.51 Bq kg⁻¹ at Za-zounmè and Dan respectively corresponding to an areal
329 activity of 302 Bq m⁻² and 451 Bq m⁻² (Table 2). Owing to uncertainties from sampling, the
330 gamma spectrometry measurements and the curve fitting, the inventory (A_s) obtained by
331 summing the ⁷Be areal activity of the depth incremental samples collected from the reference site
332 was different from that derived by integrating the area above the fitted curve [A(0)] at Dan (Table
333 3). The measured ⁷Be inventory of the whole core sampled at reference site was 313.65 ± 50 Bq
334 m⁻² for Za-zounmè and 392.78 ± 37 Bq m⁻² for Dan. As explained above the ⁷Be fraction
335 intercepted and adsorbed by the mulch were considered (Table 3) and it was found that this
336 fraction ranges from 4% (for 3 t ha⁻¹ of mulch) to 16% (for 7 t ha⁻¹ of mulch). By subtracting the

337 ^7Be uptake by the mulch, the initial amount of ^7Be received by the soil (A_{used}) under each
 338 treatment were calculated (Table 3). At Dan, the inventory values used as reference are 392.78
 339 Bq m^{-2} for the 0M plots; 377.12 Bq m^{-2} for the 3M plots and 352.91 Bq m^{-2} for the 7M plots and
 340 at Za-zounmè it was 313.65 Bq m^{-2} ; 290.32 Bq m^{-2} and 255.10 Bq m^{-2} respectively for the 0M
 341 plots; the 3M plots and the 7M plots.

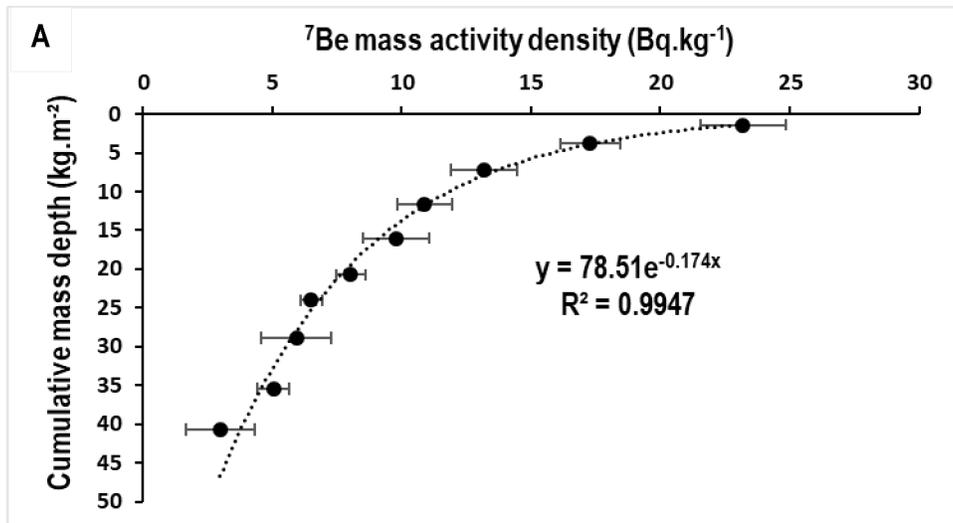
342
 343 Table 2. Expression of the initial ^7Be distribution (the uncertainties represent the standard
 344 deviation)

Site	Mass activity distribution	Areal activity distribution	h_0 (Bq m^{-2})	A_m (Bq m^{-2})	$A(0)$ (Bq m^{-2})	A_{initial} (Bq m^{-2})
Za-zounmè	55.58 exp (-x/0.183)	302 exp (-x/0.183)	5.46	304.77 ± 57	302.05	313.65 ± 50
Dan	78.51 exp (-x/0.174)	451 exp (-x/0.174)	5.75	393.75 ± 88	451.21	392.78 ± 7

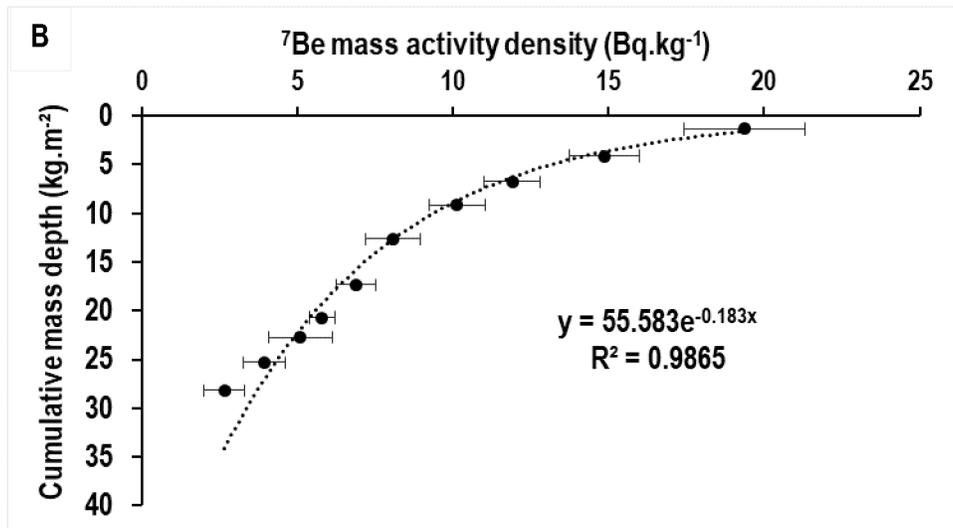
345
 346 Table 3. ^7Be reference inventory for each plot (the uncertainties represent the standard deviation)

Site	Mulch amount (t ha^{-1})	A_{initial} (Bq m^{-2})	A_{uptake} (Bq m^{-2})	% relative to no mulch	A_{used} (Bq m^{-2})
Za-zounmè	0	313.65 ± 50.44	0	0	313.65 ± 50.44
	3	313.65 ± 50.44	23.33 ± 1	6	290.32 ± 0.99
	7	313.65 ± 50.44	58.55 ± 3.65	16	255.10 ± 3.63
Dan	0	392.78 ± 7.65	0	0	392.78 ± 7.65
	3	392.78 ± 7.65	15.65 ± 0.23	4	377.12 ± 23.00
	7	392.78 ± 7.65	39.87 ± 1.23	10	352.91 ± 12.3

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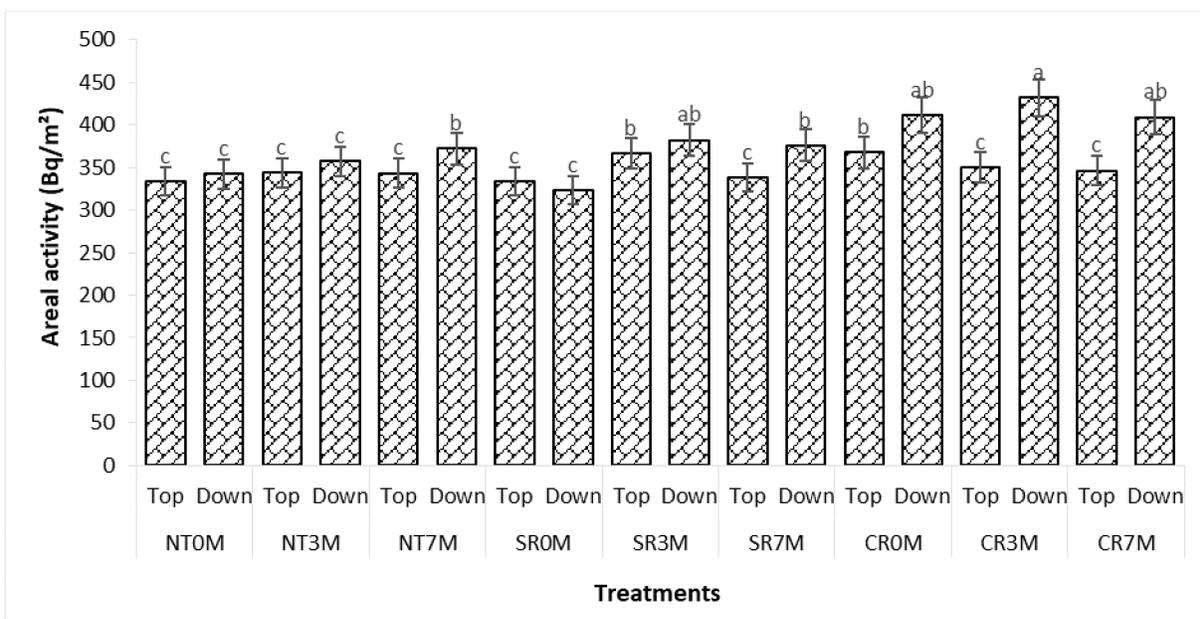


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353 Figure 5: The depth distribution of ${}^7\text{Be}$ mass activity: A) at Dan and B) at Za-zounmè. The error
354 bars represent the precision of gamma spectrometry measurements at the 95% confidence level.

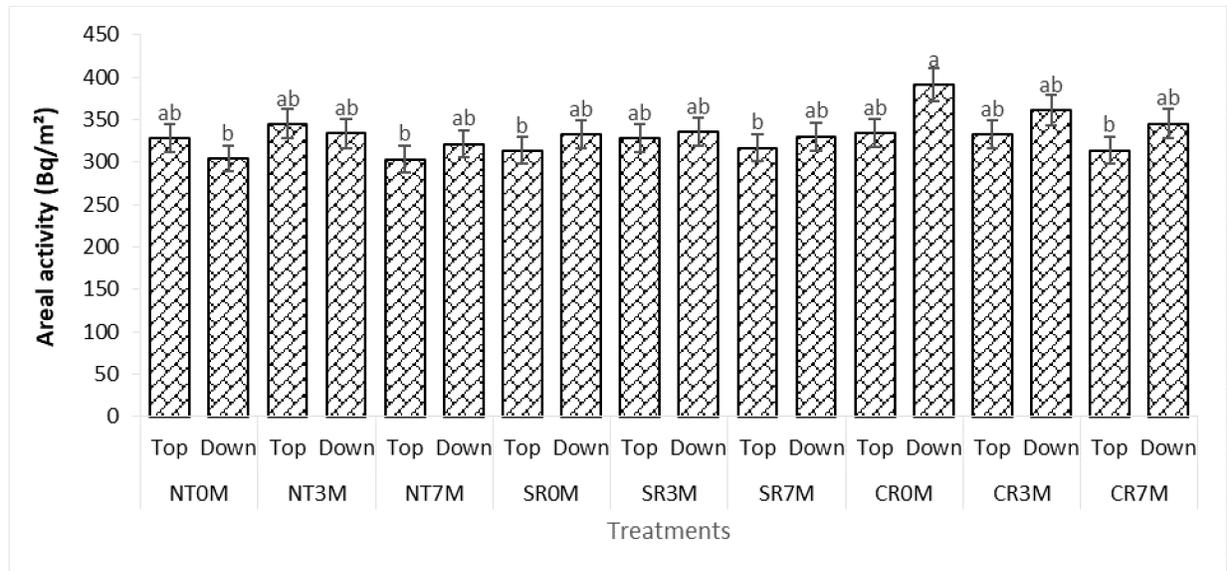
355 The ${}^7\text{Be}$ inventories (Bq m^{-2}) associated with the treatments are shown in Figures 6 and 7.
356 The observed levels range from 323.75 to 411.37 50 Bq m^{-2} with an average of 362.89 ± 30.50
357 Bq m^{-2} at Dan, and from 303.39 Bq m^{-2} to 390.62 Bq m^{-2} with an average of 331.77 ± 20.74 Bq
358 m^{-2} at Za-zounmè. As explained above, two samples were taken at each experimental plot (in
359 upper and lower part of the plot). The ${}^7\text{Be}$ inventories at the upper slope positions on all plots are
360 lower than the reference values. At the lower slope position, the ${}^7\text{Be}$ inventories are higher than
361 the reference inventory for NT7M; SR3M; CR0M; CR3M and CR7M at Dan (Figure 6) and

362 SR7M; CR3M and CR7M at Za-zounmè (Figure 7). However, at Dan, the mean inventory of ^7Be
 363 on the treatments NT0M; NT3M; SR0M; SR3M and CR0M was lower than the reference
 364 inventory indicating net soil loss, while for NT7M; SR7M, CR3M and CR7M it was higher, thus
 365 indicating deposition. At Za-zounmè, the mean inventory of ^7Be on the treatments NT0M,
 366 NT3M, NT7M, SR0M, SR3M, IR0M and IR3M was lower inventory but for SR7M and CR7M
 367 was higher than the reference inventory.



368

369 Figure 6: Inventories of ^7Be in soil at Dan. Means with the same lowercase letter are not
 370 significantly different among treatments. NT0M: No tillage + 0 t/ha of mulch; NT3M: No tillage + 3 t/ha of
 371 mulch; NT7M: No tillage + 7 t/ha of mulch; SR0M: Slope Ridging + 0 t/ha; SR3M : Slope Ridging + 3 t/ha of
 372 mulch; SR7M : Slope Ridging + 7 t/ha of mulch; CR0M : Contour ridging + 0 t/ha of mulch; CR3M : Contour
 373 ridging + 3 t/ha of mulch; CR7M: Contour ridging + 7 t/ha of mulch.



374
 375 Figure 7: Inventories of ^7Be in soil at Za zounmè. Means with the same lowercase letter are not
 376 significantly different among treatments. NT0M: No tillage + 0 t/ha of mulch; NT3M: No tillage + 3 t/ha of
 377 mulch; NT7M: No tillage + 7 t/ha of mulch; SR0M: Slope Ridging + 0 t/ha; SR3M: Slope Ridging + 3 t/ha of mulch;
 378 SR7M : Slope Ridging + 7 t/ha of mulch; CR0M : Contour ridging + 0 t/ha of mulch; CR3M : Contour ridging + 3
 379 t/ha of mulch; CR7M: Contour ridging + 7 t/ha of mulch.

380 The total soil loss estimated with the ^7Be methodology had a similar trend as the soil
 381 losses measured directly, with high soil losses with the control treatment and a decrease in soil
 382 loss with the no-tillage and contour ridges treatments (Table 4). However, the ^7Be methodology
 383 resulted in an overestimation of the total soil loss for most plots. At Dan, the highest soil erosion
 384 was obtained for SR0M (10.19 t ha⁻¹) and highest soil deposition for CR7M (4.06 t ha⁻¹). The
 385 treatments NT0M; NT3M; SR0M; SR3M and CR0M showed erosion while the treatments
 386 NT7M; SR7M; IR3M and CR7M show deposition. At Za-zounmè, the treatments NT0M; NT3M;
 387 NT7M; SR0M; SR3M; CR0M and CR3M show erosion whereas deposition was obtained on
 388 SR7M and CR7M. The highest soil erosion was obtained with NT0M (-7.36 t ha⁻¹) and the
 389 highest soil deposition was observed with CR7M (3.93 t ha⁻¹). The obtained data showed that
 390 both mulch and tillage have significant impact on soil erosion. Mulch is efficient especially if
 391 great amounts (7 t ha⁻¹) are used and among three tested tillage approaches the contour ridging is
 392 most efficient. The mean soil redistribution rates for all plots under these two treatments reached

393 0.9 t/ha for plots with 7 t ha⁻¹ of mulch and 0.4 t ha⁻¹ for plots with contour ridges. This is very
 394 good result as both these conservation measures entirely prevented net soil erosion and only
 395 limited soil redistribution took place at these experimental plots resulting in minor net deposition.
 396 The relationship between the soil loss and some characteristics of the soil is shown in table 5. It
 397 was found out that soil loss is significantly ($p < 0.05$) correlated with the amount of the mulch ($r =$
 398 -0.73), soil water content ($r = -0.91$), runoff ($r = 0.63$) and soil organic matter content ($r = -0.75$) at
 399 Dan. At Za-zounmè, significant correlation was observed between soil loss and the amount of the
 400 mulch ($r = -0.82$), soil water content ($r = -0.86$), runoff ($r = 0.67$) and Field Water Holding capacity
 401 ($r = -0.63$).

402 Table 4. Soil redistribution for the studied treatments estimated by ⁷Be-method

Treatments	Total soil loss (t ha ⁻¹)	
	Dan	Za-zounmè
NT0M	-8.63 ± 1.06	-7.36 ± 2.85
NT3M	-4.19 ± 1.49	-2.80 ± 1.27
NT7M	0.80 ± 3.31	-1.69 ± 2.22
SR0M	-10.19 ± 1.30	-6.13 ± 2.30
SR3M	-0.38 ± 1.65	-4.03 ± 0.90
SR7M	0.69 ± 3.35	0.23 ± 1.69
CR0M	-0.52 ± 4.60	-2.89 ± 1.91
CR3M	2.07 ± 8.93	-1.57 ± 3.22
CR7M	4.05 ± 7.28	3.93 ± 2.34

403 *NT0M: No tillage + 0 t/ha of mulch; NT3M: No tillage + 3 t/ha of mulch; NT7M: No tillage + 7 t/ha of mulch; SR0M: Slope Ridging + 0 t/ha; SR3M: Slope Ridging + 3 t/ha of mulch; SR7M:*
 404 *Slope Ridging + 7 t/ha of mulch; CR0M: Contour ridging + 0 t/ha of mulch; CR3M: Contour ridging + 3 t/ha of mulch; CR7M: Contour ridging + 7 t/ha of mulch.*

405 Table 5: Pearson correlation coefficients between soil loss rate and soil properties

Parameters	Soil loss (t/ha)	
	Dan	Za-zounmè
Mulch amount (t/ha)	-0.73*	-0.82**
Soil Moisture (%)	-0.91***	-0.86**
Runoff coefficient (%)	0.63*	0.67*
Organic matter content of the soil (g/kg)	-0.75*	-0.13ns
pF 2.5 (mm)	-0.82ns	-0.63*
pF 4.2 (mm)	-0.41ns	0.03ns

406

407

408 **4. Discussion**

409 The results of this study showed a significant integrative effect of tillage and mulching on
410 the soil water content and runoff. The impact of tillage and mulching on the water storage is
411 recognized worldwide (Roger-Estrade et al., 2010). In this study, it was found that for the same
412 mulch amount, the highest water content and conversely the lowest runoff coefficient were
413 associated with the contour ridges. For the same tillage treatment, the water content significantly
414 had increased, whereas the runoff coefficient had significantly decreased with the mulch amount.
415 Then, the integrative treatment combining contour ridging and 7 t ha⁻¹ of mulch had yielded the
416 higher water content of soil (17.7% at Dan and 12.1% at Za-zounmè) and had totally prevented
417 the runoff at both investigated sites. These results showed that the ridges oriented along the
418 contour direction act as efficient obstacle for runoff and consequently they contribute to
419 infiltrating and retaining water at the slope. The major effect of mulch cover is reducing soil
420 evaporation. Douzet et al. (2010); Mazarei & Ahangar (2013) and Houngnandan et al. (2018)
421 reported a 10-50% reduction in soil water evaporation as a result of soil mulching. The quantities
422 of mulch have greater impact on soil moisture especially in the topsoil, but they are detectable
423 also in deeper layers, although here the differences are smaller. Interesting feature is that at both
424 sites, the difference in the soil moisture between topsoil and deeper layers is greatest for NT0M
425 treatment and this treatment although in topsoil it has soil moisture lower than NT3M treatment
426 (as it is for all tillage treatments) in the deeper layers it has soil moisture considerably higher than
427 NT3M treatment. This can be explained by occurrence of great amount of continuous vertical
428 macropores which are known to develop usually under no tillage treatment. These macropores
429 significantly increase soil permeability and help to drain rainfall to deeper part of the soil profile.
430 If mulch is present on the soil surface it results in ponding and interception and thus hinders

431 quick infiltration. This could probably cause the greater contrast between soil moisture of topsoil
432 and subsoil under NT treatment without mulch and NT treatment with mulch than what is
433 between soils under CT and ST.

434 The tillage and mulching have significant effect also on soil erosion. The lowest soil
435 erosion was recorded under contour ridging (CR) at both sites. These findings are in line with the
436 results reported in the literature according to which the adequate tillage systems are key soil
437 water conservation measures (Kurothe et al., 2014; Akplo et al., 2017). Contour ridges stop the
438 runoff completely or at least reduce its velocity, giving thus water more time to infiltrate, and
439 deposit detached soil particles. It retains sediments in the field. In contour farming, ridges and
440 furrows are formed by tillage. Unfortunately, slope ridge (SR) practice is the most common
441 tillage approach used by the local farmers in Benin. The impact of mulch on soil erosion is based
442 on two particular effects. First, the crop residues covering the soil surface protect soil aggregates
443 from mechanical impact of falling rain drops and this prevents the detachment of soil particles
444 and reduces the amount of soil material mobilized by runoff. Secondly, the crop residues are an
445 obstacle for runoff, they reduce its speed and thus reduce its transporting capacity.

446 The high erosion rate observed under NT management as compared to the CR
447 management is in contrary with the results of Ouattara et al. (2018) and Ryken et al. (2018) who
448 reported that under no-tillage system the soil erosion is lower than under conventional tillage.
449 However, Akplo et al. (2017) showed that at short slopes the soil loss amount was 20-30 times
450 lower for contour ridging as compared to no-tillage in the watershed of Linsinlin in central Benin.
451 In general, the conservational effect of NT practices are associated with a transition phase of 7-8
452 years (on average) characterized by high soil erosion (Pagnani et al., 2019). Soil needs time to

453 develop continuous macropores improving its permeability. This can explain the high soil erosion
454 obtained under no-tillage in this study since as NT was introduced just two years ago.

455 The results showed that NT is effective in soil erosion controlling if associated with 7
456 t.ha⁻¹ of mulch. The positive effect of mulch on soil and water conservation is widely documented
457 (Uwizeyimana et al., 2018; Roger-Estrade et al., 2010; Kurothe et al., 2014). Soil water content
458 consistently increased with increase in surface cover across the three tillage practices. Treatments
459 that received 7 t ha⁻¹ of mulch cover had the highest soil water content. The findings of the
460 present study show that the lower runoff rates were obtained under the treatments that received 7
461 t ha⁻¹ of mulch at both studied sites. This means that 7 t ha⁻¹ of mulch cover is effective in water
462 conservation and soil erosion control under the agroclimatic conditions typical for Benin. The
463 role of crop residue cover in soil erosion control is based on reducing the erosive power of falling
464 rain drops and reducing the volume and velocity of runoff (Guto et al. 2012). However, to have
465 real benefit from mulch, a great quantity should be applied. Mupangwa et al. (2007) suggested at
466 least 4 t ha⁻¹ of mulch. Le Bissonnais et al. (2005) reported that below 20% of coverage, the
467 canopy or residues do not provide sufficient and continuous protection against raindrop impact
468 and particles detachment by runoff. While the direct measurements were incapable to identify
469 deposition points, the Be measurements indicate deposition under certain treatments (e.g.
470 CR7M). However, estimates of soil redistribution based on the ⁷Be measurements were an
471 overestimation relative to the direct soil loss measured. This can partially be related to the point
472 sampling of the ⁷Be methodology. Possible deposition or eroding areas within the experimental
473 plot can be unsampled (Ryken et al., 2018). In addition, as demonstrated in Taylor et al. (2014),
474 Be is preferentially adsorbed to the fine particle fraction of the soil and then eroded with fine

475 particle more quickly than the coarser fraction. This may result in an overestimation of erosion by
476 ^7Be method (Yang et al., 2013).

477 The SR tillage is a dominant land management in Benin. But because it has its negative
478 impacts such as soil erosion and nutrients as soil water loss, the NT should be recommended as
479 an effective land management controlling soil erosion and improving soil quality. However, the
480 feasibility of NT for smallholder farmers in Benin is constrained by biophysical, socio-
481 economical and technical challenges. First of all farmers must be properly trained on the NT
482 since it requires increased knowledge of the agroecosystems and adaptation to the agroecological
483 conditions and the managerial, agrotechnical, and economic conditions of the farming (Erenstein
484 et al., 2012). For example, the first condition would be a broad availability of appropriate
485 machinery for no tillage sowing. Hand no tillage sowing equipment is produced for example in
486 Brazil and was successfully tested at experimental fields in Zimbabwe under the IAEA funded
487 technical cooperation project RAF5075 'Enhancing Regional Capacities for Assessing Soil
488 Erosion and the Efficiency of Agricultural Soil Conservation Strategies through Fallout
489 Radionuclides' (Figure 8).



490
491 Figure 8: Hand sowing equipment tested at experimental fields of Chemistry and Soil Research
492 Institute, Ministry of Agriculture, Mechanization and Irrigation Development, Zimbabwe

493 5. Conclusion

494 Soil and water conservation are among keys challenges to achieve food security in sub-
495 Saharan Africa. The present study explored the efficiency of two practices of soil and water
496 conservation at plot-scale at two selected experimental sites in central Benin. The findings
497 revealed that tillage and mulching significantly influence runoff, soil water content and erosion.
498 At Dan, no-tillage with 7 t.ha⁻¹ of mulch (NT7M); contour ridging with 3 t.ha⁻¹ of mulch (CR3M)
499 and contour ridging with 7 t.ha⁻¹ of mulch (CR7M) are associated with high soil water content
500 and low runoff and soil erosion. At Za-zounmè, contour ridging with 7 t.ha⁻¹ of mulch (CR7M) is
501 associated with high water content of soil and low runoff and soil erosion. Then no-tillage with 7
502 t.ha⁻¹ of mulch (NT7M), contour ridging with 3 t.ha⁻¹ of mulch (CR3M) and contour ridging with
503 7 t.ha⁻¹ of mulch (CR7M) can be adopted for water erosion controlling and water conservation.
504 However, contour farming is most efficient on slopes between 2 and 10 %. In the long-term, it

505 should be better if farmers would adopt no-tillage practice because of its long-term sustainable
506 positive impact on the soil quality. Farmers should retain in-situ stalk of corn. Residues of
507 soybean or other residues of the previous crop should be left on the field and the seeding of the
508 next crop should be done without turning the soil by tillage. Land managers and governmental
509 agricultural decision makers should provide to farmers, the technical assistance and training them
510 in using the soil conservation agricultural practices. Because the rainfall and erosion temporal
511 dynamics and spatial distribution are very variable and the effect of the conservational practices
512 is site-specific, future research should be done specially to assess the long-term effect of contour
513 ridging and no-tillage on soil erosion in Benin.

514 **Conflicts of interest:**

515 The authors declare that they have no known competing financial interests or personal
516 relationships that could have appeared to influence the work reported in this paper.

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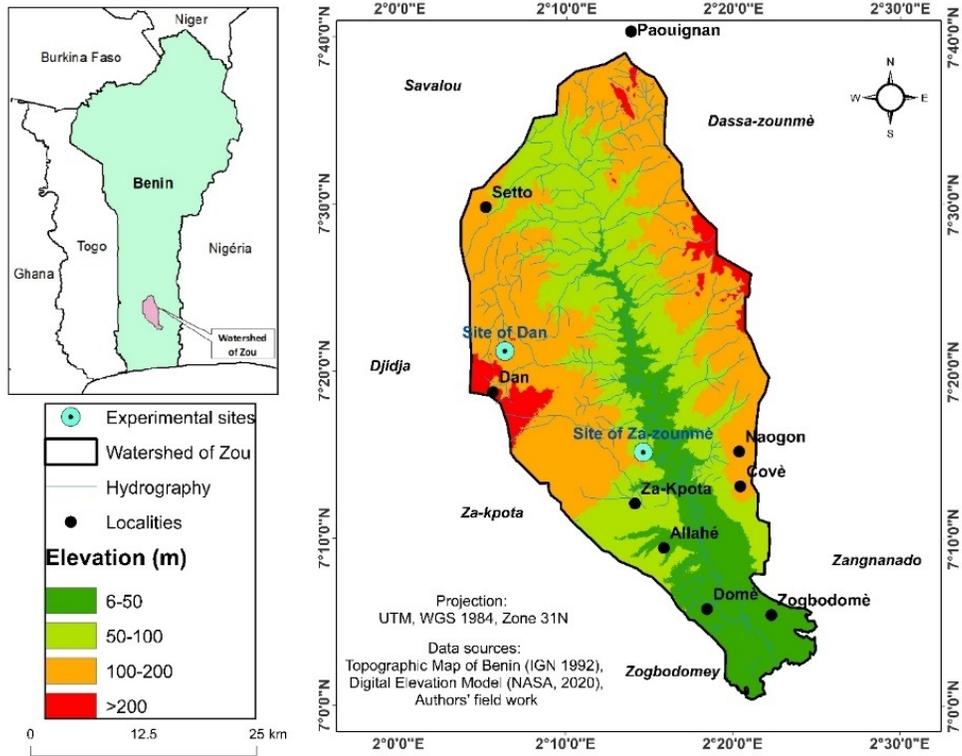
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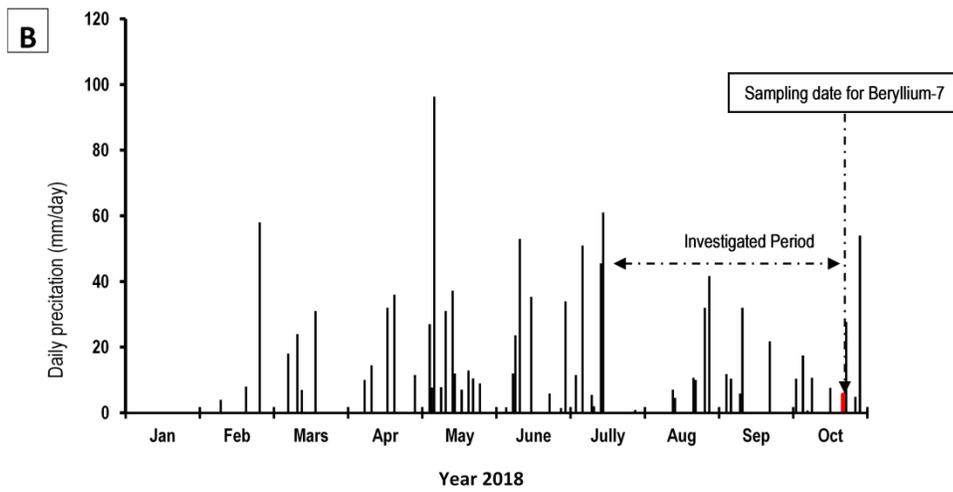
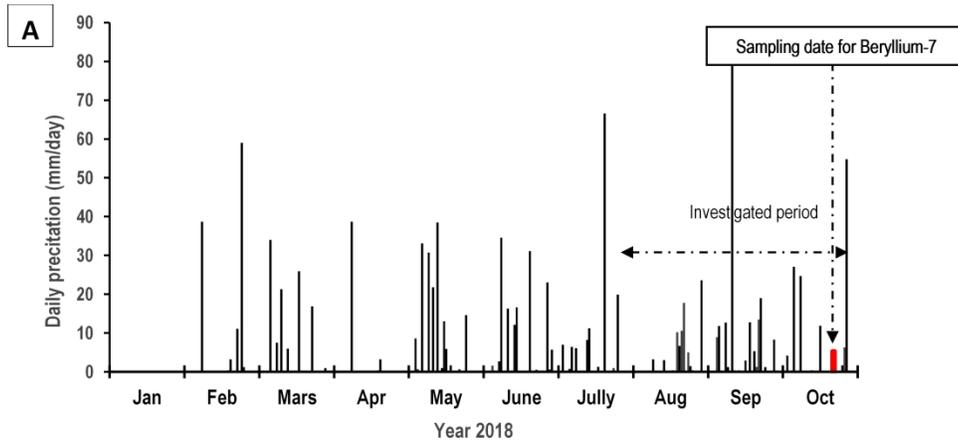
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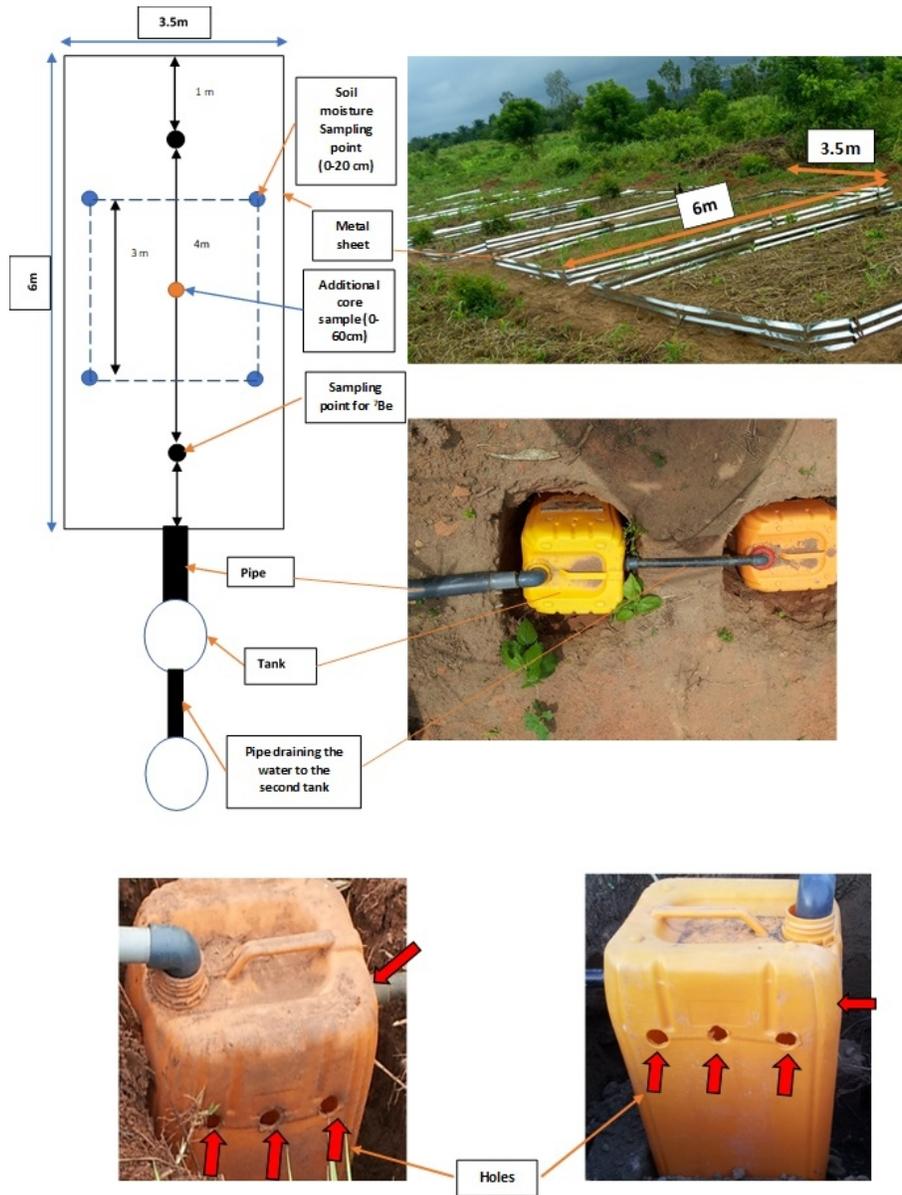
Watershed of Zou and experimental field location

108x83mm (220 x 220 DPI)

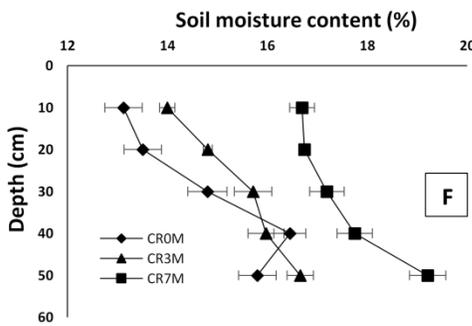
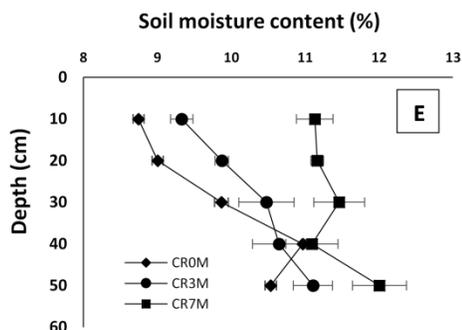
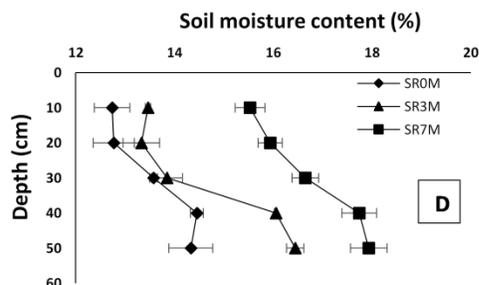
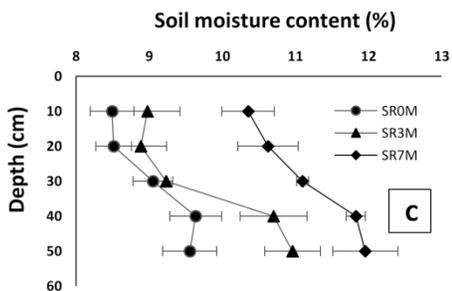
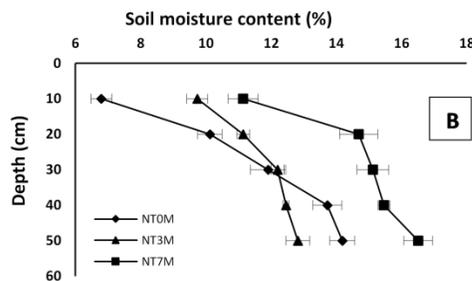
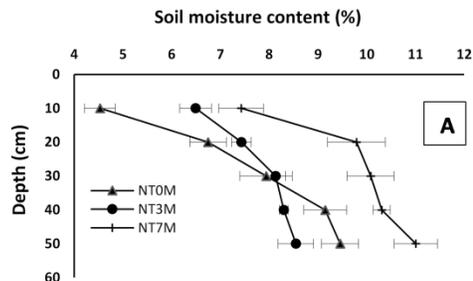


The daily precipitation recorded for the study sites

674x694mm (144 x 144 DPI)

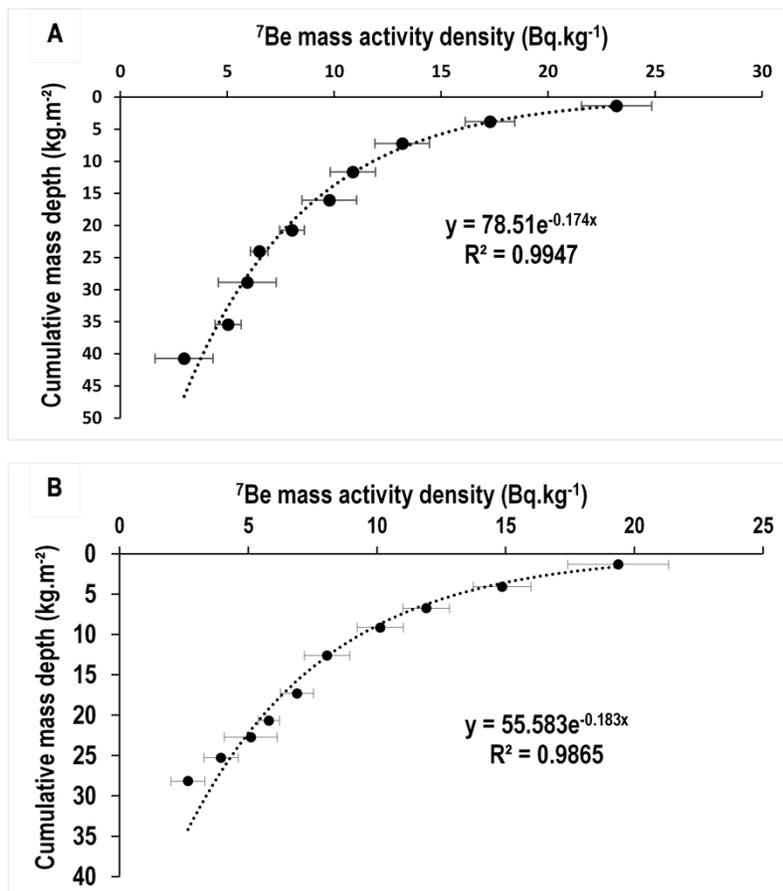


The experimental field setup
 120x154mm (150 x 150 DPI)



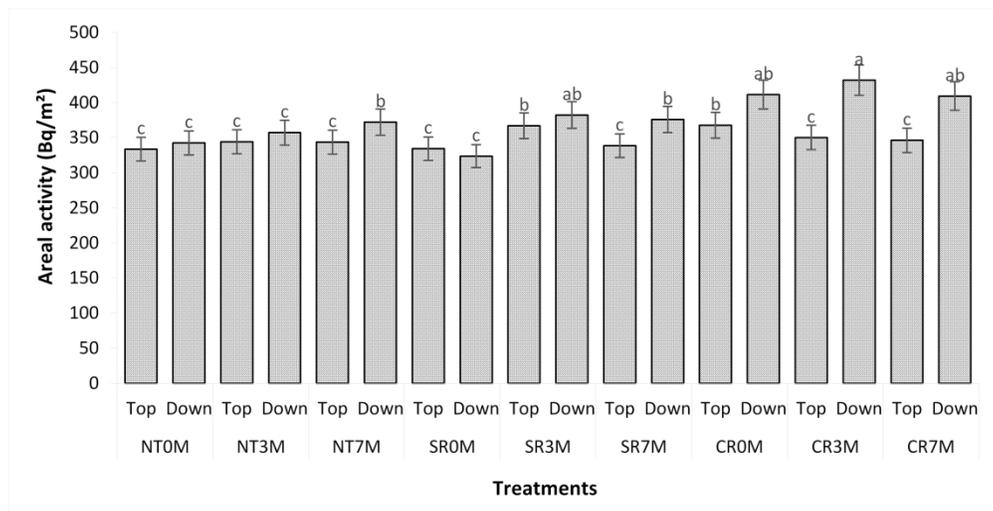
Effect of tillage and mulching on the depth distribution of soil moisture: a) no-tillage treatments at Dan; b) no-tillage treatments at Za-zounmè; c) slope ridging at Dan; slope ridging at Za-zounmè; e) contour ridging at Dan; f) contour ridging at Za-zounmè.

666x674mm (144 x 144 DPI)



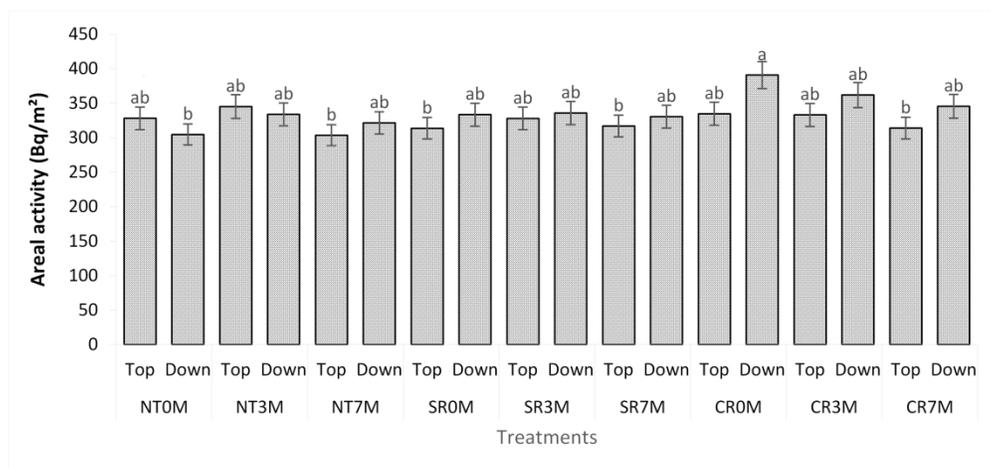
The depth distribution of ${}^7\text{Be}$ mass activity: A) at Dan and B) at Za-zounmè

666x612mm (144 x 144 DPI)



Inventories of ⁷Be in soil at Dan

670x359mm (144 x 144 DPI)



Inventories of ⁷Be in soil at Za zounmè

676x332mm (144 x 144 DPI)



Hand sowing equipment tested at experimental fields of Chemistry and Soil Research Institute, Ministry of Agriculture, Mechanization and Irrigation Development, Zimbabwe

304x228mm (87 x 87 DPI)