Seismic discrimination of controlled explosions and earthquakes near Mount St. Helens using P/S ratios

Ruijia Wang^{1,1}, Brandon Schmandt^{1,1}, and Eric Kiser^{2,2}

¹University of New Mexico ²University of Arizona

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Abstract

Explosions and earthquakes are effectively discriminated by P/S amplitude ratios for moderate magnitude events (M[?]4) observed at regional to teleseismic distances ([?]200 km). It is less clear if P/S ratios are effective explosion discriminants for lower magnitudes observed at shorter distances. We report new tests of P/S discrimination using a dense seismic array in a continental volcanic arc setting near Mount St. Helens, with 23 single-fired borehole explosions (ML 0.9-2.3) and 406 earthquakes (ML 1-3.3). The array provides up to 95 three-component broadband seismographs and most source-receiver distances are <120 km. Additional insight is provided by ~3,000 vertical component geophone recordings of each explosion. Potential controls on local distance P/S ratios are investigated, including: frequency range, distance, magnitude, source depth, number of seismographs, and site effects. A frequency band of about 10-18 Hz performs better than lower or narrower bands because explosion-induced S-wave amplitudes diminish relative to P for higher frequencies. Source depth and magnitude exhibited weak influences on P/S ratios. Site responses for earthquakes and explosions are correlated with each other and with shallow crustal Vp and Vs from travel-time tomography. Overall, the results indicate high potential for local distance P/S explosion discrimination in a continental volcanic arc setting, with [?]98% true positives and [?]6.3% false positives when using the array median from [?]16 stations. Performance is reduced for smaller arrays, especially those with [?]4 stations, thereby emphasizing the importance of array data for discrimination of low magnitude explosions.

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1 Seismic discrimination of controlled explosions and earthquakes

2 near Mount St. Helens using P/S ratios

- 3 Ruijia Wang^{1*}, Brandon Schmandt¹, & Eric Kiser²
- 4 1. Department of Earth and Planetary Science, University of New Mexico, Albuquerque, NM, 87131,
- 5 USA.
- 6 2. Department of Geosciences, University of Arizona, Tucson, AZ, 85721, USA.
- 7
- 8 *Corresponding author: <u>ruijia.wang@ualberta.ca</u>.
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10 Key Points:

- 11 1. Influences on local P/S ratios are analyzed with 23 shallowly buried explosions and 406 $M_L \ge 1$
- 12 earthquakes near Mount St. Helens.
- 13 2. Optimized array-median P/S ratios achieve \geq 98% true positives and \leq 6.3% false positives
- 14 when using ≥ 16 stations to classify explosions.
- 15 3. P/S ratio variations at individual stations are interpreted as site effects that correlate with
- 16 shallow crustal velocity structure.

18 Abstract

19 Explosions and earthquakes are effectively discriminated by P/S amplitude ratios for moderate 20 magnitude events (M \geq 4) observed at regional to teleseismic distances (\geq 200 km). It is less clear if P/S ratios are effective explosion discriminants for lower magnitudes observed at shorter 21 22 distances. We report new tests of P/S discrimination using a dense seismic array in a continental 23 volcanic arc setting near Mount St. Helens, with 23 single-fired borehole explosions ($M_{\rm L}$ 0.9-2.3) 24 and 406 earthquakes (M_L 1-3.3). The array provides up to 95 three-component broadband 25 seismographs and most source-receiver distances are <120 km. Additional insight is provided by 26 ~3,000 vertical component geophone recordings of each explosion. Potential controls on local distance P/S ratios are investigated, including: frequency range, distance, magnitude, source 27 28 depth, number of seismographs, and site effects. A frequency band of about 10-18 Hz performs 29 better than lower or narrower bands because explosion-induced S-wave amplitudes diminish 30 relative to P for higher frequencies. Source depth and magnitude exhibited weak influences on P/ 31 S ratios. Site responses for earthquakes and explosions are correlated with each other and with 32 shallow crustal Vp and Vs from travel-time tomography. Overall, the results indicate high 33 potential for local distance P/S explosion discrimination in a continental volcanic arc setting, 34 with \geq 98% true positives and \leq 6.3% false positives when using the array median from \geq 16 35 stations. Performance is reduced for smaller arrays, especially those with ≤ 4 stations, thereby 36 emphasizing the importance of array data for discrimination of low magnitude explosions.

37 Plain Language Summary

38 Methods to remotely classify seismic sources as either shear-slip earthquakes or shallow 39 subsurface explosions are important geophysical tools. They are used for investigations of 40 anthropogenic processes such as underground nuclear explosion tests and mining activity as well 41 as to obtain pure catalogs of tectonic and volcanic earthquakes. The ratio of compressional (P) 42 wave amplitude to shear (S) wave amplitude is effective for classifying large earthquakes and 43 explosions observed hundreds to thousands of kilometers away. Application of such methods at 44 local distances is a topic of growing interest because smaller magnitude sources are only 45 observed at close distances. We tested influences on P/S amplitude ratios and their effectiveness

- 46 for source discrimination using a data set of tectonic and volcanic earthquakes and controlled
- 47 shallow borehole explosions near Mount St. Helens. Most observations were within 120 km. We
- 48 found that use of high frequencies and array-median statistics is largely effective for source
- 49 discrimination in this setting, successfully classifying 100% of explosions while falsely
- 50 attributing about 5% of earthquakes to explosions. Variability of P/S ratios across the seismic
- 51 array has a highly similar pattern for explosions and earthquakes and that pattern appears to be
- 52 controlled by the seismic velocity structure of the shallow crust.

53 1. Introduction

54 Quantifying the distinctive properties of explosive seismic sources is an important capability for 55 identification and characterization of underground nuclear explosion tests and a key component of verifying compliance with nuclear test-ban treaties (Bowers and Selby, 2009). Seismic 56 identification and characterization of explosions are also important in other contexts, such as 57 58 investigations of chemical explosions that may be the subjects of judicial investigations (e.g., 59 Holzer et al., 1996; Koper et al., 2002, 2003) and volcanic explosions studied in the interest of natural hazard mitigation (e.g., Neuberg et al., 1994; Rowe et al., 1998; Johnson and Lees, 2000). 60 61 Early research on seismic discrimination of nuclear explosions and earthquakes focused on 62 events that are observable at regional to teleseismic distances (>200 km), which generally 63 requires M \geq 4 (Richards and Zavales, 1990). One useful seismic approach to discriminating nuclear explosions and earthquakes at such distances is the measurement of P/S amplitude ratios. 64 65 Abundant empirical evidence confirms that large explosions ($M \ge 4$) produce greater P/S 66 amplitude ratios compared to tectonic earthquakes, although the observed ratios are regionally heterogeneous (e.g., Taylor et al., 1989; Kim et al., 1993; Walter et al., 1995; Hartse et al., 1997; 67 68 Xie and Patton, 1999; Jenkins and Sereno, 2001; He et al., 2018; Walter et al., 2018). 69 Potential expansion of seismic discrimination techniques to local distances and lower 70 magnitudes (or explosive yields) has become a subject of increasing interest (e.g., Zeiler and 71 Velasco, 2009; O'Rourke et al., 2016; Kolaj, 2018; Pyle and Walter, 2019; Holt et al., 2019; 72 Kinter et al., 2020). At local distances and lower magnitudes, methods are usually developed to 73 discriminate chemical explosions from earthquakes and, in some cases, to differentiate single-74 fired explosions from delayed-fired explosions that are common in mining activity (Zeiler and 75 Velasco, 2009; O'Rourke et al., 2016). Single-fired chemical explosions in boreholes provide a 76 useful proxy for underground nuclear tests (Stump et al., 1999) and well-documented examples 77 are available for study on account of geophysical experiments targeting seismic source physics 78 (e.g., Pyle and Walter, 2019) or imaging of geological structures (e.g., O'Rourke et al., 2016). 79 There is mixed evidence regarding the effectiveness of P/S discrimination for ≤M3 events at 80 distances of ≤ 200 km. Some empirical investigations report that failure to discriminate between 81 earthquakes and explosions may be restricted to the shortest distances (e.g., ≤50 km in O'Rourke 82 et al., 2016). Others report sporadic failures across the local distance range, potentially on

83 account of lithologic variability of the crust causing complex source and path effects that are 84 more subdued at regional to teleseismic distances (e.g., Pyle and Walter, 2019, Kinter et al., 85 2020). Further research is needed to address questions such as: Does the complexity of crustal wave propagation make P/S ratios less diagnostic of explosive sources below a common distance 86 87 threshold? Can diminished explosion discrimination performance be overcome by larger seismic arrays or enhanced local calibration using earthquakes to constrain site and/or path effects? What 88 89 are the underlying differences in explosion sources that control discrimination capability at local 90 distances?

91 We use a data set with dense local distance recordings of earthquakes and single-fired borehole explosions near Mount St. Helens to gain further insight into the seismic source and 92 93 structural properties that control the effectiveness of the P/S ratio explosion discriminant for low 94 yields (Fig. 1). Important aspects of the data set are its diverse source-receiver paths with most 95 distances <120 km and its combination of single-fired borehole explosions and earthquakes, 96 including shallow volcanic seismicity at Mount St. Helens (e.g., Ulberg et al., 2020; Glasgow et 97 al., 2018). The source-receiver distribution was optimized for 3D structural imaging, so the 98 sources and receivers are broadly distributed within a radius of about 75 km from Mount St. 99 Helens. Compared to other data sets with one isolated test site or linear transects of receivers, the diversity of source-receiver paths helps to isolate the effects of different source types from 100 101 specific path and site influences. The inclusion of volcanic earthquakes near Mount St. Helens 102 offers an interesting comparison because volcanoes often produce more frequent shallow 103 earthquakes and more variable source mechanisms compared to other geologic settings.

104 2. Data

105 This study uses seismic recordings of earthquakes and single-fired chemical explosions in 106 shallow boreholes (Table S1). The explosions were detonated for the controlled source 107 component of the iMUSH project to image the magmatic system underlying Mount St. Helens 108 (Kiser et al., 2016, 2018; Hansen et al., 2016). Eight of the 23 boreholes were loaded with 907 kg of explosive and the other 15 were loaded with 454 kg (Fig. 1b). The explosives were buried in 109 shallow boreholes with maximum depths of ~22-28 m and explosives occupying the bottom ~5 110 111 m of the boreholes. Earthquake source information from 2014 - 2016 was provided by the Pacific 112 Northwest Seismic Network, which contributes to the USGS Comprehensive Catalog (ComCat;

113 USGS, 2020). Earthquakes within 75 km of Mount St. Helens with $M_L \ge 1$ were considered for 114 the study. Lower magnitude earthquakes are poorly recorded across most of the study area and 115 would be excluded by the requirement of P wave signal-to-noise (SNR) >2. Additionally, using 116 $M_L \ge 1$ provides a close match to the magnitude range of the explosions (M_L 0.9-2.3; calculated 117 based on waveform amplitudes instead of yield).

The primary seismic waveform data for this study are from the broadband part of the 118 119 iMUSH project (e.g., Han et al., 2018; Crosbie et al., 2019; Mann et al., 2019; Ulberg et al., 2020), which temporarily increased the density of local seismic monitoring. The iMUSH 120 121 broadband network (XD 2014-2016) was combined with permanent regional three-component 122 broadband networks (CC and UW) to create a composite network of up to 95 stations within 75 123 km of Mount St. Helens (Fig. 1a). Sampling rates vary among the networks. Based on the 124 minimum sample rate of 40 Hz we limited our analysis to frequencies ≤ 18 Hz. Network 125 information for all the broadband data is provided in Table S1. Examples of explosion and 126 earthquake record sections from the broadband array are shown in Figure 2. The example events 127 have equal local magnitudes (M_L=1.9) and they are plotted after application of bandpass filtering from 2-6 Hz. The explosion source exhibits a stronger P-wave than the earthquake, while the 128 129 earthquake exhibits a more prominent S-wave than the explosion (Fig. 2).

130 A secondary source of seismic waveform data is vertical-component geophones deployed 131 during the iMUSH controlled source imaging experiment (Kiser et al., 2016, 2018; Hansen et al., 132 2016). Our analysis of source discrimination using P/S energy focuses on three-component recordings so we only present record sections from the vertical geophones to illustrate local 133 phase propagation (Fig. 3). In Figure 3, the geophone seismograms for all 23 explosions (70,944 134 135 source-receiver pairs) were sorted into 1 km distance bins and the median envelope in each 136 distance bin is plotted with trace-normalized amplitude. The high density of recordings illustrates 137 the existence of the S-wave starting at small distances and extending across the array. 138 Comparison of the 2-6 Hz envelopes in Figure 3a and 6-18 Hz envelopes in Figure 3b shows 139 diminished S-wave amplitudes relative to P for higher frequencies. Due to the short duration of 140 the geophone deployment and movement of most geophones during the experiment, there are few opportunities for comparison with earthquakes that were recorded across most of the array. 141 142 Consequently, we focus on the broadband data from 2014 - 2016 for evaluation of P/S ratio as an 143 explosion versus earthquake discriminant.

144 3. Methods

145 **3.1 P/S amplitude ratios**

146 P/S ratios were measured with an approach similar to that used by O'Rourke et al. (2016). Below 147 we focus on the subtle differences with respect to use of three-component data and phase 148 windowing for amplitude measurements. O'Rourke et al. (2016) omitted the transverse 149 components for P measurements because a 1D isotropic medium should not produce P-wave energy on the transverse component. In contrast to O'Rourke et al. (2016), we use all three 150 151 components for measurements of amplitude in P, S, and pre-event noise windows for both 152 earthquakes and explosions. P-wave energy is commonly observed on transverse components in our dataset (Fig. 2), presumably due to out-of-plane scattering. 153

154 Phase windowing at local distances presents a challenge due to the decreasing separation of P and S with decreasing distance. To maximize use of the data we scaled the window length 155 by the S-P time, so that the time window length increases with distance until reaching a fixed 156 duration. The time window starts at -5% of the S-P time before the phase arrival time (P, S or 157 Noise) and ends at 50% of the S-P time after the arrival time for shorter source-receiver 158 distances. At larger distances (i.e., beyond 40 km) a fixed value of 3 sec after the arrival time 159 160 (Fig. 4) is used for the end of the measurement window. Stations that are too close to an event 161 (i.e., produce a S-P time window less than 1 sec) are discarded because they prevent reliable 162 separation of P and S amplitudes and their arrival times are more variable. Pre-event noise time 163 windows were sampled starting at 10 sec before the origin time of each explosion or earthquake 164 source. Our goal is to ensure the maximum phase energy is captured within the windows while 165 minimizing the contamination from noise or interfering phases. Although the optimization of 166 phase-windowing is somewhat arbitrary, similar P/S ratio results were achieved in additional 167 tests with the maximum window length increased to 4, 5, and 6 sec. We focus on the 3 sec 168 window results for the remainder of the text.

The phase windows shown in Figure 4 were calculated using a local 1D P and S velocity model derived from the controlled source survey (Fig. 1b and Fig. S1; Kiser et al., 2016). Events with P-wave root-mean-square amplitude SNR>2 were retained for P/S ratio measurements (Fig. S2). For SNR calculation, we rotated the data into the LQT reference frame (Vinnik, 1977) and 173 measured P-wave SNR on the L component so that changes in P-wave incidence angle do not 174 systematically bias the SNR. A minimum SNR value is not required for S-waves because we do 175 not want to cull weak S-waves expected for explosions. Stability in the results for different phase window lengths from 3-6 sec indicates that the deviations from the predicted 1D arrival times 176 177 have little effect. This is not surprising because phase picks for the explosion sources from Ulberg et al., (2020) have small travel time residuals compared to the 3 sec window length (Fig. 178 179 4). Residual times for 1309 manually picked P phases from explosions recorded by the broadband array have a standard deviation of 0.3 sec (average 0.01 sec), much smaller than our 180 181 window width. Manual picks are unavailable for many P and S phases at individual stations because only the clearest arrivals are picked. Thus, we prefer the generic phase windowing 182 183 approach using the 1D velocity model and 3 sec phase windows for consistency and to avoid biasing amplitude measurements by under-representing weak S-waves that are important to 184 source discrimination. 185

186 After phase windowing the three-component P/S ratio (*R*) at a given station (n) was187 calculated as:

188

 $R_n = \sqrt{\dot{\iota} \dot{\iota} \dot{\iota}}$, Eq(1)

where the subscript RTZ (could also be LQT etc.) denotes the three seismogram components and 189 190 the summations reflect the total energy within phase windows (P, S or N). All vectors in Eq(1) have same numbers of elements (i.e., window length). For source discrimination tests, the array 191 192 median and scaled median absolute deviation (SMAD) of all the individual P/S ratios are used. 193 P/S ratios were measured with waveforms bandpass filtered in several frequency bands. We 194 tested narrow frequency bands of 2-4 Hz, 4-6 Hz, 6-8 Hz, 8-10 Hz, 10-12 Hz, 12-14 Hz, and 14-195 16 Hz, following O'Rourke et al., (2016). We also tested two broader frequency bands of 6-12 Hz and 10-18 Hz. In each case, a two-pole Butterworth filter was applied to the response-196 197 corrected waveforms after demeaning and detrending.

3.2 Bootstrap resampling for different array sizes

The temporary broadband array (XD), in combination with the permanent networks (UW, CC),
provides better seismic sampling than is available for many areas of interest for explosion
monitoring (Fig. 1a). Although up to 95 stations are available during the 2-year period, not all

stations/components are available the entire time and meet the SNR>2 threshold. Within our

203 preferred frequency range (10-18 Hz), the number of stations that are finally used for P/S ratio calculation for explosions ranges from 36 to 78, with an average of 66. The average number of 204 205 stations for $M_L \ge 2$ and $M_L 1-2$ earthquakes are 72 and 47, respectively. To fully evaluate the 206 potential of our preferred method and parameter set, we used bootstrap resampling test to 207 simulate results for six subset array sizes: 2, 4, 8, 16, 32, and 64. For each subset, the cumulative array was randomly resampled 1,000 times (without replacement) from the 74 common stations 208 209 that recorded all earthquakes and explosions without any prerequisite (i.e., SNR). Within each sampled set, the array-median P/S ratio for earthquakes and explosions are calculated after 210 211 applying the SNR control. In the other words, the bootstrapping approach attempts to simulate 212 scenarios with smaller arrays and an unconditioned distribution of SNR recordings.

213 **3.3 Site corrections for P/S ratios**

214 Site corrections are often applied to P/S ratio-based discrimination measurements to minimize 215 the effects of structural heterogeneity near individual stations (e.g., Walter et al., 1995) because 216 the fine-scale structure that influences high-frequency amplitudes is usually not well constrained 217 by tomography models. Benefiting from the large number of broadly distributed stations in the study area, we estimated station-based site corrections using P/S ratios of earthquakes. This was 218 chosen to mimic the circumstance in which P/S corrections could be estimated using only 219 220 earthquake data and then applied to subsequent events of unknown physical origin. The 221 correction is calculated as a normalization of event-averaged P/S ratio at each of the N stations: (_

$$C_{1,2,3...N} = R_{eq@station(1,2,3,..n)} / mean(R_{eq@station(1,2,3,..n)}), Eq(2)$$

Where, $R_{eq@station(1,2,3,..n)}$ is a vector that contains N values, each corresponding to an eventaveraged P/S ratio (i.e., calculated from up to 406 earthquakes) at a given station after the SNR control. For each event (explosion or earthquake) recorded at a subset of m stations, its P/S ratio is then corrected by dividing $C_{1,2,3...m}$. The outcome of site correction is discussed in section 4.5 and R_{eq} for the entire array is presented in Figure 9b.

228 4. Results

229 4.1 Optimal frequency content

230 Array median P/S ratios for explosions are greater than for earthquakes in all frequency bands 231 (Fig. 5). However, the one SMAD intervals of P/S ratios overlap for lower frequency bands and most narrow frequency bands. Distributions of P/S ratios are typically not Gaussian (i.e., long-232 233 tailed), so the SMAD and median values are preferred instead of the standard deviation. In 234 general, higher bands provide larger separation in the median P/S ratios between earthquakes and 235 explosions, while broader bands help to decrease the variance and stabilize discrimination of 236 individual events (Fig. 5). With respect to source discrimination, 10-18 Hz is the preferred frequency band for this local distance data set and it is used for all the results, except where 237 238 another frequency band is specifically mentioned. The 14-16 Hz band also performs well but for 239 individual events it is more variable and it would reduce the number of SNR>2 phase windows 240 for analysis. The 10-18 Hz array-median P/S ratios and SMAD values for earthquakes and 241 explosions are $1.72(\pm 0.34)$ and $0.46(\pm 0.19)$, respectively. P/S ratios for both earthquakes and 242 explosions increase with frequency, however the increase with frequency is greater for the explosions (Fig. 5). This result from analysis of the three-component broadband array data is 243 244 consistent with the observation from the vertical-component geophones showing that S-wave 245 amplitude diminishes relative to P for higher frequencies (Fig. 3).

246 **4.2 Distance, magnitude, and depth effects**

We focus on results from distances <120 km because most of the available source-receiver pairs are within that distance range (Fig. 4b). Median P/S ratios for earthquakes and explosions sorted into six 20 km wide distance bins show little change at distances less than ~60 km and then increasing P/S ratio with distance beyond ~60 km (Fig. 6a). The SMAD values are also larger at greater distances due to the decreased number of samples within each distance bin. Given that distance distributions of earthquakes and explosions are very similar in this study (Fig. 4b), we do not apply distance corrections to the P/S ratios.

P/S ratios for earthquakes and explosions do not vary strongly with local magnitude (Fig.
6b). The median P/S ratios in most 0.2 M_L bins overlap within one SMAD. There appears to be

an increase in P/S ratio for the largest explosion magnitude bin, but it is heavily influenced by 256 one explosion source with a particularly high P/S ratio resulting in a relatively large SMAD for 257 258 the highest magnitude bin among explosions (Fig. 5b). Earthquake P/S ratios remain low across 259 the local magnitude range. There is a slight decrease in the median earthquake P/S ratios for the 260 largest magnitudes ($M_1 > 2.5$), which is within the range of one SMAD. Given the weak distance and magnitude dependences found in the P/S ratios, we did not apply the magnitude and distance 261 262 amplitude correction (MDAC) approach that is commonly used in regional distance studies (Walter and Taylor 2001; Anderson et al., 2009). 263

264 Estimated earthquake source depths exhibit weak correlation with P/S ratios (Fig. 7). As the area near Mount St. Helens is characterized by variable surface topography (i.e., ranging 265 266 from 0 - 4 km, Fig. 1). To account for elevation in Figure 7, we add the surface elevations at 267 event epicenter locations to the source depths reported relative to sea level. The sum thus reflects 268 the distances between the hypocenters and the surface. Binning the earthquake sources into four 269 depth ranges (0-5, 5-10, 10-15, and 15-20 km) results in median P/S ratios that all overlap within 270 one SMAD. Depth uncertainties are highly variable depending on local array coverage, but 271 reported uncertainties from the Pacific Northwest Seismic Network for $M_1 \ge 1$ earthquakes near 272 Mount St. Helens are typically <1 km. In that context, results from binning within 5-km depth intervals should not be strongly biased by inaccurate depth estimates. There is a slight decrease 273 274 in median P/S ratio from 0.78 at 0-5 km to 0.41 at 15-20 km, which is comparable to the SMAD (i.e., 0.1-0.35) for any of the source depth bins. 275

4.3 Number of stations in the seismic array

277 Bootstrap resampling of the three-component seismographs simulates the potential average 278 source discrimination performance with smaller seismic arrays (see section 3.2). The cumulative 279 distribution functions (CDFs) from resampling show that greater variations are observed for explosion P/S ratios compared to earthquake P/S ratios (Fig. 8). Increasingly large seismic arrays 280 281 help reduce the overlap of earthquake and explosion P/S ratio distributions near a value of ~ 1 (Fig. 8). Separation of earthquake and explosion P/S ratios is subject to diminishing 282 283 improvement for arrays with over 16 stations. The improvement with increasing array size 284 appears modest in this context because the curves shown in Figure 8 are generated as averages 285 from 1,000 bootstrap resampling subsets (for 2, 4, 8, 16, 32 and 64 station cases). The variance

of P/S ratios is much larger for smaller arrays and its effect on discrimination performance isdiscussed further in section 5.1.

4.4 Site response effects and shallow crust structure

289 Variations in station-averaged P/S ratios from earthquakes and borehole explosions exhibit 290 similar spatial patterns, despite the generally higher P/S ratios for explosions (Fig. 9). A scatter 291 plot of the earthquake station-averages versus the explosion station-averages shows an 292 approximately linear trend, with a correlation coefficient of 0.625. If the earthquakes are subset 293 by magnitude, the M_L1-2 and M_L \geq 2 subsets yield correlations of 0.625 and 0.641 (these two 294 earthquake subsets are correlated at 0.91), respectively. These correlations indicate that 295 observations of small ($\sim M_1$ 1-3) earthquakes may provide a useful basis for determining 296 empirical P/S amplitude site corrections that are applicable to explosions. However, the 297 improvement for the purpose of source discrimination appears to be subtle in this case (Fig. 10). 298 Application of site corrections increased the difference between the median explosion and 299 earthquake P/S ratios from 1.29 to 1.41, but the SMAD values also increased slightly for 300 explosions (0.38 to 0.43) and earthquakes (0.21 to 0.23). Furthermore, we found the site correction terms are positively correlated with shallow crustal velocities. We adopt a velocity 301 302 model from a recent local travel time tomography study around Mount St. Helens (Ulberg et al., 303 2020) and evaluate the correlation of our site corrections with the model. The Vp, Vs and Vp/Vs 304 values are extracted from the tomography at 1 km depth beneath all the station (site) locations 305 (i.e., interpolated from the tomography model using each station's latitude and longitude). Overall, the cross-correlation coefficients for the site correction terms are 0.397 for Vp and 0.479 306 for Vs. Site corrections exhibit a much weaker correlation (-0.086) with Vp/Vs (Fig. 9 d-f). The 307 308 correlation coefficients remain comparable for all layers around sea level (± 2 km) and they 309 decrease at deeper depths, suggesting that the site correction is influenced by uppermost crustal 310 structure.

311 5. Discussion

312 **5.1 Effectiveness for explosion discrimination**

313 To evaluate the performance of different frequency bands and array sizes, we adopt receiver 314 operating characteristic (ROC) curves (James et al., 2013), which show the diagnostic 315 performance of binary classifiers calculated from: true positive, false positive, true negative, and 316 false negative results. In this case for explosions versus earthquakes, we treat explosions identified correctly as "true positive" and earthquakes identified as explosions as "false positive" 317 318 (vice versa for earthquakes). For each P/S ratio used as a discrimination threshold, the point 319 along the ROC curve is determined by the rate of true positives and false positives. The optimal discrimination threshold is chosen by maximizing the area under the ROC curve (AUC). Thus, 320 321 an ideal classifier would be plotted in the upper left corner corresponding to 100% true positive 322 and 0% false positives. Application to P/S ratios with the preferred frequency band of 10-18 Hz and the full data set of earthquakes and explosions shows 100% true positives and 4.93% (20 out 323 324 of 406) false positives for a P/S ratio threshold of 1.2 (Fig. 11a). Half of the events that create 325 false positives (i.e., P/S>1.2) are only recorded with <6 stations, reflecting the disadvantage of insufficient station coverage for low-magnitude sources (Fig. S5). For comparison, a lower and 326 narrower frequency band of 6-8 Hz results in 86.95% true positives and 5.67% false positives for 327 328 a P/S ratio threshold of 0.9 (Fig. 11b).

329 Discrimination performance generally improves with increasing event magnitude and 330 array size (Fig. 11c, d). Using all explosions and only $M_1 \ge 2$ earthquakes, a threshold P/S ratio of 331 1.2 results in 100% true positives and 0% false positives. The M_L 0.9-2.3 explosions produced an 332 average of 66 stations with SNR>2, while the M_L 1-2 earthquakes only produced an average of 333 47 stations with SNR>2. So, the diminished discrimination performance for M_L 1-2 earthquakes 334 is likely influenced by SNR at individual stations and the total number of stations available for 335 analysis. ROC curves for seismic arrays composed of N=4, 16, and 64 seismographs illustrate 336 the effects of array size (Fig. 11c). For N=64, the bootstrap resampling results show that a 337 maximum AUC of 1 is consistently achieved for discrimination of explosions and $M_1 \ge 2$ 338 earthquakes. For N=16, the average of the AUC maxima is 0.98. For N=4, the average of the 339 AUC maxima reduces to 0.94 (Fig. 11d). However, the ROC curves for N=4 are much more

340 variable, including a few samples with near-random performance (Fig. 11c) and some extreme 341 cases reaching the AUC maximum (Fig. 11d). Generally, larger array size is expected to better 342 mitigate source and path variations, so the requirement could be much lower in the case where 343 the explosion and earthquake sources are co-located. A separate bootstrap resampling test with 344 an earthquake epicenter nearly co-located with an explosion shows that <16 stations are sufficient for robust discrimination (Fig. S6), suggesting that the minimum number of stations 345 346 could be much lower if the earthquake epicenter and suspected explosion are closely located. In 347 this example the horizontal locations are separated by 2.4 km and the depths are separated by 348 11.1 km.

349 Comparison of the new results from near Mount St. Helens with other local distance P/S 350 ratio discrimination tests may be influenced by different local propagation effects related to 351 geological settings as well as measurement approaches. A similar scale study using data covering 352 the Bighorn mountain range and adjacent sedimentary basins in Wyoming found effective P/S 353 discrimination at ~50-200 km distance but failure at <50 km distance (O'Rourke et al., 2016). As 354 our analysis exhibits effective discrimination at such distances, below we consider two minor methodological differences between this study and O'Rourke et al. (2016) that might contribute 355 356 to the difference in performance. We acknowledge that different local propagation effects may 357 also be the cause of the difference in discrimination performance, but a thorough re-analysis of 358 their data would be required to isolate that influence.

359 The first methodological difference is that we include the transverse component for Pwave measurements (see section 3.1). Explosion recordings in this study commonly show 360 361 SNR>2 (our threshold for analysis) even for P-waves recorded on the transverse component (Fig. 362 2). If scattering of P energy onto the transverse component is important at distances <50 km, then 363 the inclusion of transverse component data may be beneficial for explosion discrimination. A 364 comparison of array-median P/S ratios with and without the transverse component shows that 365 separation of the explosion and earthquake ratios improves with inclusion of the transverse 366 component (Fig. 12). The increased separation is primarily due to increases in the explosion P/S 367 ratios, while changes in the earthquake P/S ratios are smaller. This is consistent with the possibility that out-of-plane P-wave scattering is stronger for explosions than earthquakes. In this 368 369 case, the benefit of including transverse component P-wave energy spans our entire local

distance range (Fig. 12), but given that P/S ratios tend to increase with distance for both
approaches the incremental improvement is more important at smaller distances (≤60 km).

372 The second difference is that we did not apply the MDAC method for regional seismic discriminants (Walter and Taylor 2001; Anderson et al., 2009) to correct for distance and 373 374 magnitude effects. We chose not to use MDAC because the distance and especially magnitude trends in our raw P/S ratios are modest compared to the SMAD values for explosion and 375 376 earthquakes, respectively (Fig. 6). Additionally, MDAC was originally designed for larger 377 distances (e.g., >100 km) and O'Rourke et al. (2016) note that stations at their shortest distances 378 (~20-40 km) exhibit abnormally high MDAC corrections for explosions, further challenging 379 their discrimination. We speculate that the amplitude correction techniques developed for 380 regional distances may need to be revised for shorter local distances. Similar to the weak distance and magnitude trends found in this study, Zeiler and Velasco (2009) reported negligible 381 382 distance dependence of explosion discriminants (including P/S ratios) within the local distance 383 range. We suggest that the necessity and design of the amplitude correction techniques for 384 explosions observed at short distances (\leq 50 km) should be further investigated.

385 In a recent local to regional distance study, Pyle and Walter (2019) investigated P/S ratio 386 discrimination with six chemical explosions from the Source Physics Experiment (Snelson et al., 2013) and nearby tectonic earthquakes. Similar to O'Rourke et al. (2016) and this study, Pyle 387 388 and Walter (2019) found that P/S discrimination performance improved with increasing 389 frequency (≥ 6 Hz) and that array averaging of ~ 10 or more stations was needed to achieve clear 390 separation of explosion and earthquake P/S ratios. Four of the six explosions used in their study 391 had larger explosive yields than all the explosions in this study and the receiver spacing within 392 \sim 100 km was sparser, so relative to O'Rourke et al., (2016) there is less opportunity for 393 comparison of results at similar scales. The fact that we observe optimal performance for 394 somewhat higher frequencies in this study (e.g., 10-18 Hz) likely reflects our focus on shorter source-receiver distances of <120 km compared to distances up to ~450 km in Pyle and Walter. 395 (2019).396

397 5.2 Source effects

398 The geophone record sections show that S-waves emerge within the first few kilometers from the 399 source, acknowledging that there is not sufficient sampling available to resolve S-wave 400 emergence in detail at scales of hundreds of meters (or less) from the source (Fig. 3). Assuming

401 the S-wave is effectively generated at the source for this data set, increasing P/S ratio with

402 distance is expected if S-wave attenuation is greater than P-wave attenuation in the crust (e.g.,

403 Pyle et al., 2017). In contrast, a difference in source spectra may be needed to explain why

404 explosion P/S ratios increase with frequency more than earthquake P/S ratios (Fig. 5).

Prior studies of M≥3 chemical explosions and nuclear explosions indicate that explosion-405 406 induced crustal S-waves (Lg) exhibit lower corner frequencies than explosion-induced P-waves 407 (local Pg & regional Pn phases; Xie, 2002; Fisk, 2006, 2007). In these studies, the S-wave corner frequency is typically about half of the P-wave corner frequency. Our results with lower yield 408 409 chemical explosions are similar based on the increased separation of local distance explosion and earthquake P/S ratios at higher frequencies. The 10-18 Hz band may perform relatively well for 410 411 P/S ratio discrimination because it partially overlaps the interval between the lower S-wave corner frequency and the higher P-wave corner frequency (e.g., Fisk, 2007). Using the Mueller-412 413 Murphy model corner frequency scaling from Fisk, (2007) the explosions in this study are expected to produce local P-wave corner frequencies of ~35-45 Hz and S-wave corner 414 415 frequencies of ~17-23 Hz. The 40 Hz sampling rate for most stations limited our analysis to 416 frequencies below ~18 Hz, so only the highest frequencies in this study are near the expected S-417 wave corner. Extension of P/S ratio measurements to higher frequencies by collecting higher 418 sample-rate data may be beneficial, especially for very short distances (\leq 50 km) and low 419 magnitudes ($M_L \leq 2$).

420 The physical controls on explosion-induced S-wave spectra remain debated. If a 421 difference in source spectra explains the observed frequency dependence of P/S ratios, the 422 physical cause may be rooted in the different P- and S-wave elastic length scales of sensitivity to 423 near-source rock damage (Taylor, 2009). However, a variety of complicated and locally specific 424 effects such as spall and free-surface topographic scattering are thought to influence explosioninduced S-wave spectra (e.g., Xie and Lay, 1994; Patton and Taylor, 1995). Multiple explosion 425 426 source studies suggest that the conversion from Rayleigh to S-wave could be the dominant 427 contributor to explosion S-waves and control the distinct frequency-dependent decay of S-wave 428 amplitudes (e.g., Myers et al., 1999; Pitraka et al., 2015; Mellors et al., 2018). An alternative to explaining the frequency dependence of P/S ratios with different source spectra is that explosions 429 430 may preferentially excite shallower shear modes that attenuate more rapidly with distance (e.g.,

Baker et al., 2004, 2012). Regardless of the exact S-wave excitation mechanism, our results
show that local distance P/S ratios increase with frequency; the effects of both source diversity
and near-source structural complexity, even around an active volcano, can be suppressed using
array median P/S ratios if the array size is large enough.

435 One explosion source in this study that produced a relatively low P/S ratio resulted in clear surface evidence of shear slip at the source. The 'X4' explosion (Fig. 1b; also see Fig. S4 436 437 and Table S1) detonated in a borehole with maximum depth of ~ 22 m depth resulted in a small normal fault scarp with a length of ~15 m and vertical offset of up to ~20 cm. Consequently, it is 438 unsurprising that this explosion exhibited a relatively low P/S ratio of 1.27 (Fig. 10), which is 439 440 near the optimal binary classification cutoff of 1.2 for the 10-18 Hz data set including all 441 M_L≥1earthquakes (Fig. 11b). It is unknown if 'blind' shear failures that did not rupture the 442 surface are common for other low P/S ratio explosions.

443 5.3 Combining local distance seismic discriminants

444 The P/S ratio results presented here show the potential for effective discrimination if a large local array is available, but in practice explosion discrimination is usually more challenging due to 445 smaller arrays and source discrimination relies on evidence from multiple types of seismic 446 447 measurements. Consequently, we discuss possibilities for combining P/S ratios with other types 448 of local distance source discriminants. Ratios of different seismic magnitude metrics such as mb 449 (body-wave magnitude) & Ms (surface-wave magnitude) have long been used as an initial or 450 'screening' step for source discrimination of M≥3 events (Stevens and Day, 1985; Selby et al., 451 2012; Ford and Walter, 2014). At local scales there is growing evidence that the difference 452 between the local (Richter) magnitude and the coda duration magnitude (M_L-M_C) can help 453 discriminate explosions, primarily because the magnitude difference is sensitive to source depth 454 (Holt et al., 2019; Voyles et al., 2020). M_L and M_C measurements are based on different parts of 455 the seismogram. M_L is controlled by the peak seismic amplitude, while M_C is controlled by the duration of later-arriving scattered energy. Very shallow sources such as borehole explosions 456 457 preferentially produce longer coda leading to negative M_L - M_C . P/S amplitude ratios, as implemented in this study, ignore the extended coda and we find weak source depth dependence 458 459 for P/S amplitude ratios (Fig. 7). Thus, the capabilities of the two discriminants may be rooted in complementary aspects of the local seismic wavefield. A simple workflow to leverage the two 460

approaches would be using M_L-M_C to screen for unusual events given that routine catalog 461 462 generation can commonly provide both parameters. Then events identified by screening could be 463 further investigated with P/S ratios. More thorough approaches to jointly classifying events 464 based on M_L-M_C and P/S ratios should also be considered. P/S ratio measurements could also be 465 automated to enhance screening capabilities once travel time relationships and site corrections are developed for an array. Additional use of more time-consuming moment tensor analysis of 466 467 low magnitude local distance events might be reserved for events flagged by M_L-M_C and P/S screening (e.g., Alvizuri and Tape, 2016). 468

469 6. Conclusions

P/S ratio discrimination of earthquakes and shallow single-fired borehole explosions at distances 470 471 less than 120 km was tested with a dense broadband seismic array near Mount St. Helens. Taking 472 advantage of the excellent coverage of both stations and sources, we evaluated the effects of 473 frequency bands, source-receiver distances, source magnitudes and focal depths. Optimal 474 separation of P/S ratios for the two sources types was found using a 10-18 Hz frequency band, 475 which achieved explosion discrimination with 100% true positives and 4.93% false positives 476 using the entire array. Randomly resampling to simulate smaller arrays shows performance of 477 \geq 98% true positives and \leq 6.3% false positives for \geq 16 stations. Performance becomes highly 478 variable using ≤ 4 stations, likely as a result of structural complexity in the volcanic arc setting. 479 Successful separation using the dense array and optimized frequency band left limited room to 480 improve the performance, consequently our site corrections derived from 406 local earthquakes had a negligible effect on discrimination statistics. Despite the limited improvements in this case, 481 we found that the site corrections correlate with Vp and Vs of the uppermost crust from a recent 482 483 tomography study. Future studies using P/S ratios may benefit from local site corrections derived 484 from small earthquake recordings or local tomography models.

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- 643





Figure 1. Study area maps with sources and receivers. A) Vertical geophone locations are plotted 646 along with single-fired explosion locations. Explosion locations loaded with 907 kg of explosive 647 648 are denoted by filled symbols and locations loaded with 454 kg are denoted by hollow symbols. 649 The symbol sizes for explosions are scaled by their M_L. Explosions labeled with stars were detonated during controlled source phase 1 (recorded by Texan 1 array; ~2370 nodes) and 650 diamonds were detonated during phase 2 (recorded by Texan 2 array; ~2220 nodes). 'X4' 651 652 denotes one explosion that is discussed in the text. Geophone locations in pink (~900 nodes) 653 recorded both sets of explosions. B) Broadband stations used in the study are plotted along with 654 the locations of $M_L \ge 1$ earthquakes that occurred between June 20, 2014 to August 31, 2018) within 75 km of Mount St. Helens. The time span corresponds the deployment of XD array 655 (blue); permanent stations are shown as CC (green) and UW (grey). 656



657

Figure 2. A) A record section is plotted for an explosion event with 616kg equivalent TNT load 658 (Y8, located at the NW of array, M_L=1.9, depth=0 km; see Table S1 for details). The event 659 660 showed relatively strong S energy among explosions. Only 18 seismograms are shown for 661 clarity. B) Record section for an equal-magnitude earthquake (2015 Feb 9, 05:45:35, depth=0.4 km) with waveforms from 19 stations. Waveforms are filtered between 2-6 Hz at plotted with a 662 663 reduced velocity of 7 km/s in both figures. The blue and red shades mark the P and S wave 664 windows, predicted using a locally optimized 1D velocity model (Kiser et al., 2016; also see Fig. 665 S1 and section 3.1). Note the relatively strong P energy around 60 km. Same events but filtered with 10-18 Hz are shown in Fig. S3. 666



667

668 Figure 3. Stacked geophone recordings of explosions. A) Median envelopes of geophone

seismograms from all 23 explosions in 1 km distance bins (70,944 source-receiver pairs).

670 Seismograms were bandpass filtered from 2-6 Hz before envelope calculation and median-

671 stacking. Median envelopes at each distance are normalized by their maximum. The cyan dashed

672 line marks the beginning of the P window and the red dashed line marks the beginning of the S

673 window. B) Same as A, except that seismograms were bandpass filtered from 6-18 Hz. The

674 higher frequency band exhibits diminished S-wave amplitudes relative to P.



Figure 4. Phase windowing and source-receiver distances. A) Phase windowing based on travel
times from a local 1D P and S velocity model (Kiser et al., 2016; also see Fig. S3&4 for
waveform examples). B) Histogram of source-receiver distances using 10 km bins up to 180 km.
Note that the number of earthquake source-receiver pairs in each distance bin is divided by 5 to
better enable comparison of the two distributions.



685 Figure 5. Median P/S ratio for explosions and earthquakes at nine different frequency bins: seven

686 2-Hz narrow bins same as O'Rourke et al., 2016 and two wide bins (filled symbols). Bold error

- 687 bars are SMAD and thin bars are 2-scaled median absolute deviation (i.e., 2*SMAD). The
- 688 median±SMAD for explosions are labeled on top.





690 Figure 6. Distance and magnitude effects (calculated at 10-18 Hz). A) P/S versus distance

averaged over 20 km with step size of 20 km for all source-station pairs of earthquakes and

692 explosions. B) P/S ratio versus magnitude with bin size of 0.2. Error bars indicate the SMAD

693 calculated from station-based ratios of all events within each magnitude bin.



694Distance to suface (km)695Figure 7. Earthquake P/S ratios versus source depth below surface (calculated at 10-18 Hz). Red696circles show array-averaged P/S ratios for individual earthquakes, with circle size scaled by M_L 697(1-3.3). The four bold (thin) bars show median SMAD (2*SMAD) within depth bins: 0-5 km, 5-69810 km, 10-15 km, and 15-20 km.



Figure 8. Effects of array size on P/S ratios (calculated at 10-18 Hz). A) Cumulative distribution
functions (CDF) for P/S ratios of earthquakes as a function of array size for 2, 4, 8, 16, 32, and
64 stations. Each event ratio is calculated from the median of P/S ratio measured at N stations
while the final CDF curves are generated from the mean of all events. B) Same as (A) except for

rot explosions rather than earthquakes.



Figure 9. Site corrections and crustal seismic structure (calculated at 10-18 Hz). A) Map of
station-averaged P/S ratios for explosions. B) Map of station-averaged P/S ratios for earthquakes.
Note that the color scale is different from A so that the similarity in spatial pattern is easier to
identify. C) Scatter of station-averaged P/S ratios for earthquakes versus explosions. D-F) Scatter
plots of site correction versus Vp, Vs, and Vp/Vs at 1 km depth from Ulberg et al., 2020. CC:
cross-correlation coefficient.



714 Figure 10. Site corrections and P/S ratios (calculated at 10-18 Hz). A) Histograms of array-

715 averaged P/S ratios for all explosions and earthquakes. B) Same as A, except the P/S site

716 correction term is applied. The median \pm SMAD of the P/S ratio distributions are labeled in

717 corresponding colors.



718

719 Figure 11. A) ROC curves for P/S ratio threshold optimization at 10-18 Hz and 6-8 Hz. B) Area 720 under curve (AUC) for searched P/S ratio thresholds (0.1 step size from 0.2 to 2.6). The 721 preferred P/S ratio cutoff is 1.2 at 10-18Hz (AUC=0.98), which leads to a true positive rate of 100% and false positive rate of 4.93%. C&D) Similar to A&B) but showing bootstrapping results 722 723 using only $M_1 \ge 2$ earthquakes. The bold lines are averaged curves from 1000 subsets and the 724 three dots mark the highest AUC. Note that a few outliers exhibit near-random performance for 725 the 4-station case (light blue near the diagonal in C) and a few others may reach AUC=1 while 726 the averages (bold curves) are below 1 for 4-station and 16-station cases (in D).





Figure 12. Effect of transverse component P-wave energy on P/S ratios. The error bars show

729 medians and SMAD values of 10-18 Hz P/S ratios in 20 km bins for all source-station pairs

730 (similar to Figure 6a but using only $M_L \ge 2$ earthquakes and all explosions).



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Supporting Information for

Seismic discrimination of controlled explosions and earthquakes near Mount St. Helens using P/S ratios

Ruijia Wang^{1*}, Brandon Schmandt¹, & Eric Kiser²

1. Department of Earth and Planetary Science, University of New Mexico, Albuquerque, NM, 87131, USA.

2. Department of Geosciences, University of Arizona, Tucson, AZ, 85721, USA.

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Figures S1 to S6

Additional Supporting Information (Files uploaded separately)

Captions for Tables S1

Introduction

This supporting information provide additional details on our velocity model (Figure S1) and data quality (Figure S2). Figure S3 presents the station coverage and magnitude information for the high P/S ratio earthquakes. A simple bootstrapping resampling analysis on a nearly colocated pair of earthquake and explosions is provided to show that fewer stations could be sufficient to discriminate explosive sources (Figure S4). Finally, complete header information for the explosions (i.e., shots), earthquakes and broadband stations are included in Table S1. All waveform data are openly available from the IRIS DMC.



Figure S1. Simplified 1D P and S velocity model for Mount St. Helens (Kiser et al., 2016). The depth is relative to sea level.



Figure S2. SNR distribution of earthquakes and shots in log scale, where a cutoff of SNR=2 is around 0.3 in log scale. Each measurement is for a single source-receiver pair from the broadband array.



Figure S3. Same as Figure 2 in the main text but with filter range of 10-18 Hz.



Figure S4. Example of phase windowing on unfiltered waveforms. (a) and (b): explosive source (X4, M_L 1.3; also see Figure 1 and Table S1) recorded at near and far source stations. (c) and (d) earthquake (2016/07/07 15:29:36 UTC, M_L 2, depth=18.2 km; also see Table S1) recorded at near and far source stations. Note in (b) & (d), the time scales are 3 times of (a) & (c) and the phase windows are bounded by 3 sec.



Figure S5. Station coverage of the high P/S ratio earthquakes that lead to false positive explosion classifications (see Figure 11 in the main text). A) Histogram showing number of valid stations used to calculate the median value. B) Event P/S vs. magnitude with number of valid stations labeled. Note that these 20 earthquakes are sparsely located around Mount. St. Helens with depth ranging from 0 to 20 km.



Figure S6. Bootstrap resampling test for a pair of co-located earthquake and explosion. A) location of the pair (magenta box); shot name "Y6". The horizontal distance between the sources is 2.4 km and the depth difference is 11.1 km. B) and C) Histograms for the P/S ratio determined from randomly selected (no repeat) ~20% of the stations recording the pair.

Table S1. Event and station information (files uploaded separately)

Sheet1-Shot: time, location, magnitude and yield for all explosions

Sheet2-earthquake: all earthquakes within 75km of Mount St. Helens requested from PNSN catalog; only $M_l \ge 1$ earthquakes are used in this study.

Sheet3-broadband array: broadband stations from net code XD, CC and UW.